DRAFT TRAFFIC STUDY FOR THE 8888 WASHINGTON BOULEVARD PROJECT

Prepared for:

THE RUNYON GROUP

FEBRUARY 2017

Submitted by:



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EXECUTIVE SUMMARY

A detailed traffic study was performed by Raju Associates, Inc. to assess the traffic impacts of the proposed 8888 Washington Boulevard Mixed-Use Project within the City of Culver City, California. The Project is located at 8888 Washington Boulevard.

The Proposed Project consists of the construction of 59,325 square feet of office use, 2,878 square feet of retail use, and 3,184 square feet of restaurant use. The Project would provide 212 parking spaces. The ground floor would contain four loading spaces and one ADA van accessible space, and the subterranean parking levels would contain 207 spaces. The existing site contains an auto repair facility with a building size of 9,992 square feet which will be demolished.

As proposed, one driveway located along Washington Boulevard would provide access to the Project site.

Current and future traffic analyses at 26 intersections within the Cities of Culver City and Los Angeles were conducted in this study. At these locations, traffic operations were studied prior to and after implementation of the Proposed Project; deficiencies and impacts, if any, identified; improvements and mitigation measures, if required, developed; their effectiveness determined and residual traffic impacts, if any, ascertained as part of this study. Access and circulation at the proposed driveway to the parking area for the Project were also evaluated. The following executive summary highlighting the key findings of this study is presented below.

- Twenty-six intersections were analyzed within the study area for this project. These
 locations are within the study area bounded by Cattaraugus Avenue on the north,
 Jefferson Boulevard/Rodeo Road on the south, Hughes Avenue/Duquesne Avenue on the
 west and La Cienega Boulevard on the east. Of the 26 intersections, 14 intersections are
 located within the City of Culver City and 12 intersections within the City of Los Angeles.
- Currently, 24 of the 26 analyzed intersection locations are operating at levels of service (LOS) D or better during the morning peak hour. During the evening peak hour, 23 of the 26 analyzed intersections are operating at LOS D or better. The remaining intersections are operating at LOS E or F.
- In the Cumulative (Future Year 2018) Base conditions, i.e., future conditions without the
 implementation of the Proposed Project, 20 of the 26 study intersections are projected to
 operate at LOS D or better during the morning peak hour. During the evening peak hour,
 19 of the 26 analyzed intersections are projected to operate at LOS D or better. The
 remaining intersections are projected to operate at LOS E or F.

- The Proposed Project consists of 59,325 square feet of office use, 2,878 square feet of retail use, and 3,184 square feet of restaurant use. The existing site contains an auto repair facility auto repair facility with a building size of 9,992 square feet which will be demolished. The Project is estimated to generate a net total of 100 trips during the morning peak hour and 124 trips during the evening peak hour.
- In the Existing (2016) plus Project conditions, both the morning and evening peak hour operating conditions would be similar to those for the Existing conditions. Under this scenario, 23 of the 26 analyzed intersection locations would continue to operate at acceptable levels of service (LOS) D or better during both the morning and evening peak hours. The remaining intersections would be operating at LOS E or F.
- The Existing (2016) plus Project traffic conditions indicate that the Proposed Project would not cause significant traffic impacts at any of the analysis locations during the weekday morning and evening peak hours.
- In the Cumulative (Future Year 2018) plus Project conditions, both the morning and evening peak hour operating conditions would be similar to those projected for the Cumulative Base conditions. Under this scenario, 20 of the 26 study intersections are projected to operate at LOS D or better during the morning peak hour. During the evening peak hour, 19 of the 26 analyzed intersections are projected to operate at LOS D or better. The remaining intersections are projected to operate at LOS E or F.
- The Cumulative (Future Year 2018) plus Project traffic conditions indicate that the Proposed Project would not cause significant traffic impacts at any of the analysis locations during both the weekday morning and evening peak hours.
- The Proposed Project would not have a significant impact on the residential streets in the local neighborhood.
- The Proposed Project would add less than 50 trips to the nearest Congestion Management Program (CMP) arterial monitoring locations and would add less than 150 trips in either direction to the nearest CMP mainline freeway monitoring locations during both the weekday morning and evening peak hours. Per CMP guidelines, no further CMP analysis is required.
- The Proposed Project shall make a contribution of \$100,000 towards transportation improvements including Intelligent Transportation System (ITS) signal system improvements and bicycle and pedestrian system improvements. The contribution will be due at the time of issuance of a Certificate of Occupancy.

Summarizing, the Proposed Project would not cause any significant impacts at any of the analyzed intersections. Therefore, no project-specific mitigation measures would be required.

I. INTRODUCTION

This report documents the assumptions, methodologies and findings of a study conducted by Raju Associates, Inc., to evaluate the potential traffic impacts of the proposed project located at 8888 Washington Boulevard within the City of Culver City, California.

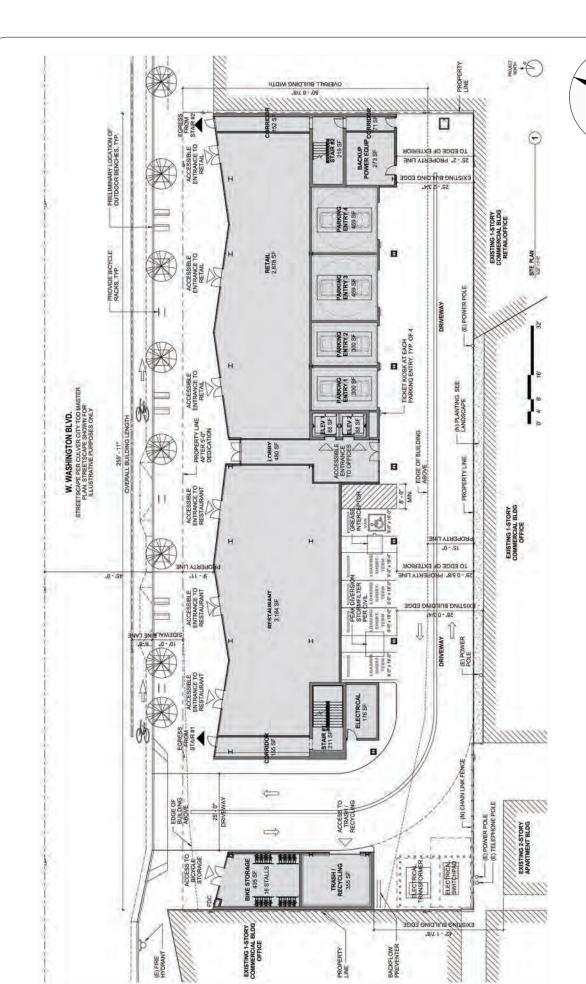
PROJECT DESCRIPTION

The Proposed Project is located on the south side of Washington Boulevard between Robertson Boulevard-Higuera Street and Landmark Street. Figure 1 illustrates the location of the Proposed Project in relation to the surrounding street system.

The Proposed Project consists of the construction of 59,325 square feet of office use, 2,878 square feet of retail use, and 3,184 square feet of restaurant use. The Project would provide 212 parking spaces. The ground floor would contain four loading spaces and one ADA van accessible space, and the subterranean parking levels would contain 207 spaces. The existing site contains an auto repair facility with a building size of 9,992 square feet which will be demolished.

As shown on Figure 2, the proposed project driveway is located along Washington Boulevard on the western boundary of the project site. The proposed project driveway would provide access to the Project site.

FIGURE 1 LOCATION OF PROJECT AND ANALYZED INERSECTIONS



SOURCE: ABRAMSON TEIGER ARCHITECTS

FIGURE 2 PROJECT SITE PLAN

STUDY SCOPE

The scope of work for this study was developed in conjunction with the Cities of Culver City and Los Angeles staff. The base assumptions, technical methodologies and geographic coverage of the study were all identified as part of the study approach. The study is directed at the analysis of potential traffic impacts on the street system produced by the Proposed Project per the City of Culver City traffic impact significance criteria. For locations within the City of Los Angeles, the City of Los Angeles traffic impact significance criteria have been used. The scenarios identified below have been evaluated in this study.

- <u>Existing (2016) Conditions</u> The analysis of existing traffic conditions is intended to provide a basis for the remainder of the study. The existing conditions analysis includes an assessment of streets, traffic volumes, and operating conditions.
- <u>Existing (2016) Plus Project Conditions</u> The net traffic expected to be generated by the Proposed Project is estimated and added to the Existing (2016) traffic volumes. The impacts of the Proposed Project on existing traffic operating conditions are then identified.
- <u>Cumulative (2018) Base Conditions</u> Future traffic conditions in the year 2018 without the Proposed Project have been developed. The objective of this analysis is to project future traffic growth and operating conditions, which could be expected to result from regional ambient growth and related projects in the vicinity of the study area by the year 2018.
- <u>Cumulative (2018) Plus Project Conditions</u> The net traffic expected to be generated by the Proposed Project is estimated and added to the Cumulative (2018) Base traffic forecasts. The impacts of the Proposed Project on future traffic operating conditions are then identified.

As part of this traffic study, a total of 22 signalized intersections and four unsignalized intersections within two jurisdictions have been analyzed. A list of these intersections is presented in Table 1 and their locations are illustrated in Figure 1. Of the 26 study locations, 14 intersections are in the City of Culver City and 12 intersections are in the City of Los Angeles. These study locations were coordinated with the affected jurisdictions as part of the scoping for the study and were analyzed for the scenarios described above.

A detailed Memorandum of Understanding (MOU) was prepared in coordination with the City of Culver City staff. The MOU includes among other details, a description of the Proposed Project, its trip generation and distribution characteristics. A copy of the MOU is attached in Appendix A of this report.

TABLE 1
LIST OF ANALYZED INTERSECTIONS

	Inte			
Int #	Northbound/Southbound	Eastbound/Westbound	Jurisdiction	Signalized?
1.	Robertson Boulevard	I-10 WB Off-Ramp/Kincardine Avenue	City of Los Angeles	Yes
2.	Robertson Boulevard	National Boulevard	City of Los Angeles	Yes
3.	National Boulevard	I-10 Eastbound On-Ramp	City of Los Angeles	Yes
4.	Bagley Avenue	Venice Boulevard	City of Los Angeles	Yes
5.	Culver Boulevard	Venice Boulevard	City of Los Angeles	Yes
6.	Robertson Boulevard	Venice Boulevard	City of Los Angeles	Yes
7.	National Boulevard	Venice Boulevard	City of Los Angeles	Yes
8.	La Cienega Boulevard	Venice Boulevard [1]	City of Los Angeles	Yes
9.	Culver Boulevard	Washington Boulevard/Irving Place	Culver City	Yes
10.	Main Street	Culver Boulevard	Culver City	Yes
11.	Culver Boulevard	Washington Boulevard	Culver City	Yes
12.	Ince Boulevard	Washington Boulevard	Culver City	Yes
13.	Robertson Boulevard/Higuera Street	Washington Boulevard	Culver City	Yes
14.	Landmark Street	Washington Boulevard	Culver City	Yes
15.	National Boulevard	Washington Boulevard	Culver City	Yes
16.	Helms Avenue	Washington Boulevard	Culver City	Yes
17.	La Cienega Avenue	Washington Boulevard	Culver City	Yes
18.	La Cienega Boulevard	Washington Boulevard	Culver City	Yes
19.	Wesley Street	National Boulevard	Culver City	Yes
20.	Hayden Avenue	National Boulevard	Culver City	Yes
21.	Jefferson Boulevard	National Boulevard	City of Los Angeles	Yes
22.	Jefferson Boulevard	Higuera Street/Rodeo Road	City of Los Angeles	Yes
23.	Robertson Boulevard	I-10 EB On-Ramp	City of Los Angeles	No
24.	Robertson Boulevard	Exposition BI/I-10 EB Off-Ramp	City of Los Angeles	No
25.	Wesley Street	Washington Boulevard	Culver City	No [2]
26.	Cattaraugus Avenue	Washington Boulevard	Culver City	No

^[1] Los Angeles County Congestion Management Program monitoring location.

^[2] The intersection will be signalized in the future.

ORGANIZATION OF REPORT

An executive summary presenting key details of the study is provided at the beginning of this report. The rest of the report is divided into seven chapters. Chapter I presents an introduction and provides details of the various elements of the study. Chapter II describes the existing circulation system, traffic volumes, and traffic conditions within the study area. Chapter III describes the development of the Proposed Project's traffic projections. The methodology to develop Future Year 2018 traffic volume forecasts without and with the Proposed Project is described and applied in Chapter IV. Chapter V presents assessment of traffic conditions with and without the project and the potential traffic impacts due to the Proposed Project. Residential street segment analysis, parking, and access/circulation evaluations are presented in Chapter VI. The results of the analysis of the Proposed Project's impacts on the CMP regional transportation system are provided in Chapter VII. A summary of the analysis and study conclusions is included in Chapter VIII. Appendices to this report include details of the technical analyses.

II. EXISTING CONDITIONS

A comprehensive data collection effort was undertaken to develop a detailed description of existing conditions within the study area. The assessment of conditions relevant to this study includes an inventory of the street system, traffic volumes on these facilities, and operating conditions at key intersections. A detailed description of these elements is presented in this chapter. The existing transit system serving the study area is also described in this chapter.

STUDY AREA

The Project site is located on south side of Washington Boulevard between Robertson Boulevard-Higuera Street and Landmark Street. The San Diego (I-405) Freeway is located approximately two miles west of the Project site and the Santa Monica (I-10) Freeway is located less than a half mile north of the Project site. The study area is bounded by Cattaraugus Avenue on the north, Jefferson Boulevard/Rodeo Road on the south, Hughes Avenue/Duquesne Avenue on the west and La Cienega Boulevard on the east.

EXISTING STREET SYSTEM

The existing street system within the study area consists of a regional highway system, primary arterials, secondary arterials, and neighborhood feeder streets/collectors and local streets. A description of the regional and local access and circulation offered by the various roadways follows.

The San Diego (I-405) and Santa Monica (I-10) Freeways provide the primary regional access to the study area. The key arterials serving the site are Venice Boulevard, National Boulevard, Washington Boulevard, Culver Boulevard, Duquesne Avenue, Robertson Boulevard, Higuera Street, Hayden Avenue, La Cienega Boulevard, Rodeo Road, Jefferson Boulevard, and Fairfax

Avenue. The remaining neighborhood streets (collector and local streets) offer local circulation possibilities. A brief description of these facilities follows.

- Santa Monica (I-10) Freeway The I-10 Freeway is an east-west freeway that transverses the Southern California region from its western terminus at Pacific Coast Highway in the City of Santa Monica into San Bernardino County and points east. In the vicinity of the study area, this freeway generally provides four lanes in the westbound direction and four lanes in the eastbound direction. There are interchanges at Robertson Boulevard, National Boulevard, La Cienega Boulevard/Venice Boulevard and Washington Boulevard/Fairfax Avenue in the vicinity of the study area. This freeway provides access to the regional interstate system.
- <u>San Diego (I-405) Freeway</u> The I-405 Freeway is a north-south freeway that transverses
 the Southern California region from its northern terminus at the I-5 Freeway in Sylmar to
 its southern terminus at the I-5 Freeway in Irvine. In the vicinity of the study area, this
 freeway provides six lanes in each direction (including one HOV lane). There are
 interchanges at Culver Boulevard and Venice Boulevard/Washington Boulevard in the
 vicinity of the study area. This freeway provides access to the regional interstate system.
- Venice Boulevard Venice Boulevard is classified as a primary arterial/major highway, within the study area, and traverses in an east-west direction across several jurisdictions. Within the study area, Venice Boulevard generally offers six travel lanes, three lanes in each direction, with left-turn lanes at key intersections and a large raised median island. On-street parking is allowed on both sides of the street throughout the study area. Venice Boulevard provides access to the I-10 (Santa Monica) Freeway.
- Washington Boulevard Washington Boulevard is classified as a primary arterial roadway within the City of Culver City and a major highway within the City of Los Angeles. It defines the northern frontage of the Project site. Washington Boulevard traverses in an east-west direction across several jurisdictions and generally offers four travel lanes, two lanes per direction, with a central left-turn lane or median. On-street parking is generally allowed along this roadway in the vicinity of the study area.
- <u>Culver Boulevard</u> Culver Boulevard is a primary arterial within the City of Culver City and a major highway within the City of Los Angeles and traverses diagonally in an east-west direction from Playa del Rey to its terminus at Venice Boulevard. Within the study area, this roadway offers four travel lanes, two lanes per direction, with a raised median and turn lanes at major or key intersections. On-street parking is allowed along this roadway throughout the study area, except at major intersections where turn lanes are provided. Culver Boulevard currently provides access to the I-405 (San Diego) Freeway to and from the north.
- <u>Jefferson Boulevard</u> Jefferson Boulevard is a primary arterial/major highway west of La Cienega Boulevard and traverses in an east-west direction across several jurisdictions. East of La Cienega Boulevard, Jefferson Boulevard is classified as a secondary highway. Within the study area, this roadway generally provides four travel lanes, two lanes in each direction with a central left-turn lane. On-street parking is generally allowed along this roadway.

- La Cienega Boulevard La Cienega Boulevard is classified as a primary arterial/major highway and traverses in a north-south direction across several jurisdictions. This roadway offers six travel lanes, three lanes per direction, with a central left-turn median. There is no stopping at any time along the roadway within the study area. This roadway provides access to the I-10 (Santa Monica) Freeway, as well as, the I-405 (San Diego) Freeway to and from the south.
- <u>Fairfax Avenue</u> Fairfax Avenue is a primary arterial/major highway that traverses in a north-south direction and offers four travel lanes, two lanes per direction, with left-turn lanes at key intersections. On-street parking is generally prohibited along this roadway within the study area. This roadway provides access to the I-10 (Santa Monica) Freeway.
- Rodeo Road Rodeo Road is classified as a major highway and runs in an east-west direction across the City of Los Angeles. Within the study area, this roadway generally provides six travel lanes during peak commute hours, three lanes in each direction, with a central left-turn median. Restricted on-street parking is generally allowed along this roadway.
- Robertson Boulevard Within the City of Los Angeles, Robertson Boulevard is classified as a secondary highway. Within Culver City, south of Venice Boulevard, Robertson Boulevard is classified as a primary arterial. This roadway runs in a north-south direction and generally provides four travels lanes, two lanes in each direction. On-street parking is allowed on both sides of the streets within the study area. Some segments of Robertson Boulevard have parking prohibitions and/or restrictions on one or both sides of the street. Robertson Boulevard provides access to the I-10 (Santa Monica) Freeway.
- <u>National Boulevard</u> National Boulevard is a secondary arterial/highway that runs in an east-west direction. It generally offers two lanes in each direction and provides connection to the I-10 (Santa Monica) Freeway north of the Project site. On-street parking is available along many stretches of this roadway, generally, except at major intersections where turn lanes are provided.
- <u>Duquesne Avenue</u> Duquesne Avenue is a secondary arterial roadway that traverses in a north-south direction. Within the study area, this roadway offers two travel lanes, one lane per direction. On-street parking is generally allowed on both sides of the street.
- <u>Hayden Avenue</u> Hayden Avenue is a secondary arterial that traverses in a north-south direction. This roadway offers two travel lanes, one lane in each direction. Between National Boulevard and Higuera Street, on-street parking is generally prohibited or restricted.
- Higuera Street Higuera Street is classified as a secondary arterial between Hayden Avenue and Jefferson Boulevard and provides four travel lanes, two lanes in each direction. Between Washington Boulevard and Hayden Avenue, Higuera Street is classified as a neighborhood feeder street and provides two travel lanes, one lane per direction. On-street parking is generally allowed along many stretches of this roadway. At the intersection of Hayden Avenue-Hayden Place/Higuera Street, a raised median barrier has been placed to prevent eastbound and westbound through traffic movements. All traffic in either direction along Higuera Street must turn onto Hayden Avenue or Hayden Place.

- <u>Hughes Avenue</u> Hughes Avenue is classified as a collector street and traverses in a north-south direction. Within the study area, this roadway provides two travel lanes, with one lane in each direction. On-street parking is generally allowed along this roadway throughout the study area. Between Venice Boulevard and Washington Boulevard, onstreet parking is prohibited.
- Wesley Street Wesley Street is a discontinuous local roadway that runs in a north–south direction. One segment of Wesley Street extends south from Washington Boulevard, terminating in a cul-de-sac. The other segment of Wesley Street connects National Boulevard to Higuera Street. This roadway provides two travel lanes, one lane per direction. On-street parking is generally allowed along this roadway within the study area.
- <u>Irving Place</u> Irving Place is a local roadway that traverses in a north-south direction.
 North of 'A' Street, the roadway provides one travel lane per direction with metered
 parking on both sides of the street. South of 'A' Street to its terminus at Lucerne Avenue,
 the roadway provides one-way northbound circulation. Parking is generally allowed on
 both sides of the street along this segment.
- <u>Braddock Drive</u> Braddock Drive is a neighborhood feeder street that runs in a northwest to southeast direction. It provides two travel lanes, one lane per direction. On-street parking is generally allowed on the south side of the street within the study area.
- <u>Landmark Street</u> Landmark Street is a local roadway that traverses in a north-south direction and adjacent to the Project site. This roadway offers two travel lanes, one lane in each direction, and it is undivided. On-street parking is allowed along this roadway.
- <u>Cattaraugus Avenue</u> Cattaraugus Avenue is classified as a local roadway within the City
 of Culver City and is classified as a collector street within the City of Los Angeles. This
 roadway traverses in a north-south direction and generally offers two travel lanes, with one
 lane per direction. On-street parking is generally allowed along this roadway.
- <u>Lucerne Avenue</u> Lucerne Avenue is a neighborhood feeder street that runs in a northwest to southeast direction. It provides two travel lanes, one lane per direction. Onstreet parking is generally allowed on the south side of the street within the study area.

The existing lane configurations of the analyzed intersections are included in Appendix B.

EXISTING TRAFFIC VOLUMES AND LEVELS OF SERVICE

The following sections present the existing intersection peak hour traffic volumes, a description of the methodology utilized to analyze the intersection traffic conditions, and the resulting level of service conditions at each of the study intersections.

Existing Traffic Volumes

Weekday morning and evening peak hour traffic counts were compiled from data collected at the analyzed intersections in February, April, September, and October 2015, and March and November 2016. Traffic counts collected in 2015 were factored upward 1% per year to reflect existing 2016 conditions. These traffic volumes reflect typical weekday operations during current year 2016 conditions. The traffic volumes in Figures 3A and 3B represent, for the purposes of this analysis, the Existing 2016 AM and PM peak hour conditions.

The raw data showing the raw traffic counts are attached in Appendix C.

<u>Level of Service Methodology</u>

Level of service (LOS) is a qualitative measure used to describe the condition of traffic flow, ranging from excellent conditions at LOS A to overloaded conditions at LOS F. LOS D is typically recognized as the minimum acceptable level of service in urban areas.

The Level of Service definitions for signalized and unsignalized intersections is provided in Table 2 and Table 3, respectively. Twenty-two of the 26 analyzed intersections are controlled by traffic signals and four analyzed intersections are unsignalized.

The Intersection Capacity Utilization (ICU) method was used to determine the intersection V/C ratio and corresponding level of service for City of Culver City study intersections. Per City of Culver City Traffic Study Criteria, a capacity of 1,600 vehicles per lane per hour is assumed, a total of 2,880 vehicles per hour for dual left-turn lanes, and a 10% reduction factor to account for the loss time of the yellow signal clearance periods was utilized in the capacity calculations.

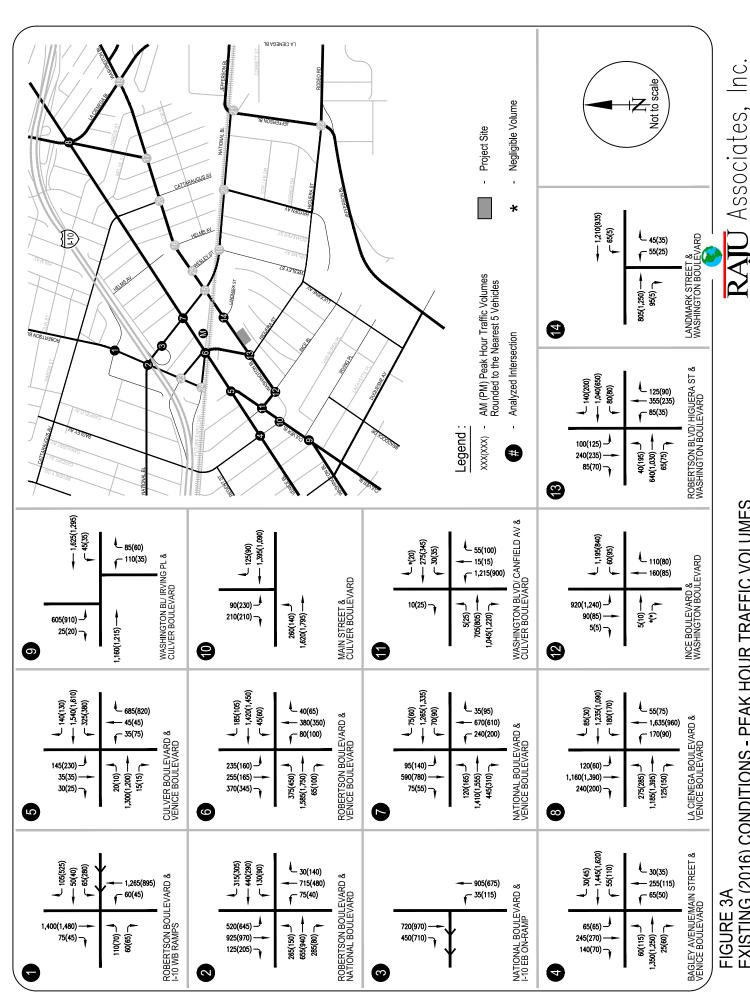
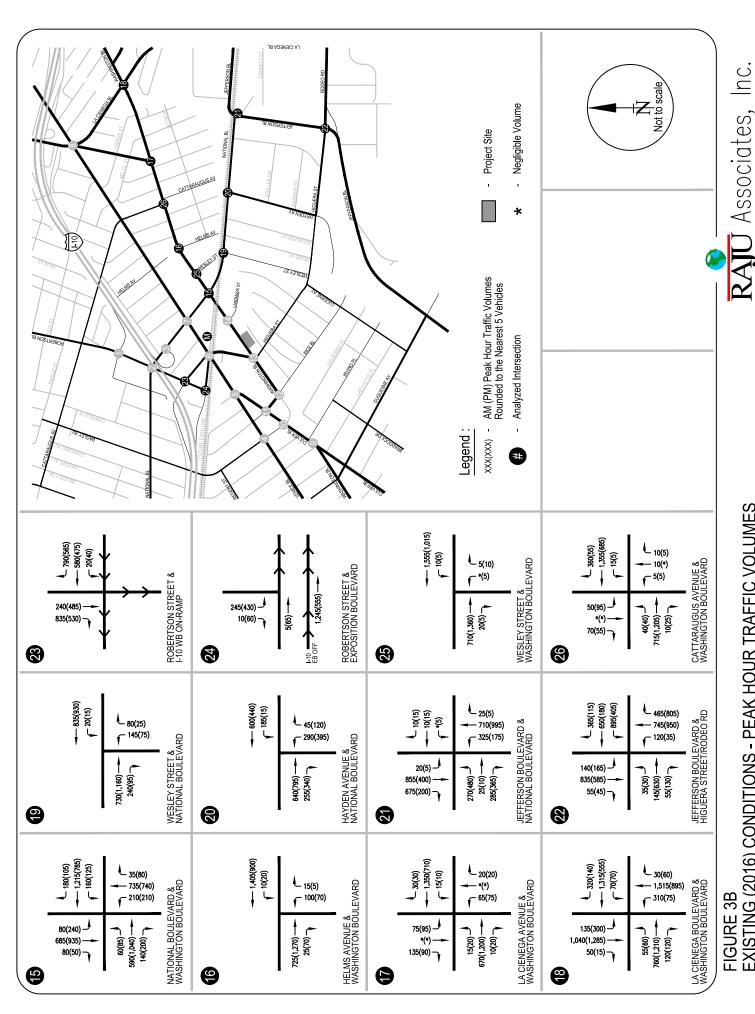


FIGURE 3A EXISTING (2016) CONDITIONS - PEAK HOUR TRAFFIC VOLUMES



EXISTING (2016) CONDITIONS - PEAK HOUR TRAFFIC VOLUMES

TABLE 2
LEVEL OF SERVICE DEFINITIONS FOR SIGNALIZED INTERSECTIONS

Level of Service	Volume/Capacity Ratio	Definition
_		EXCELLENT. No vehicle waits longer than one red
Α	0.000 - 0.600	light and no approach phase is fully used.
D	>0.000 0.700	VERY GOOD. An occasional approach phase is
В	>0.600 - 0.700	fully utilized; many drivers begin to feel somewhat
		restricted within groups of vehicles.
С	>0.700 - 0.800	GOOD. Occasionally drivers may have to wait
	>0.700 - 0.600	through more than one red light; backups may
		develop behind turning vehicles.
D	>0.800 - 0.900	FAIR. Delays may be substantial during portions
	>0.800 - 0.900	of the rush hours, but enough lower volume periods
		occur to permit clearing of developing lines,
		preventing excessive backups.
F	>0.900 - 1.000	POOR. Represents the most vehicles intersection
_	0.000 1.000	approaches can accommodate; may be long lines
		of waiting vehicles through several signal cycles.
F	> 1.000	FAILURE. Backups from nearby locations or on
		cross streets may restrict or prevent movement of
		vehicles out of the intersection approaches.
		Tremendous delays with continuously increasing
		queue lengths.

Source: Transportation Research Board, *Transportation Research Circular No. 212, Interim Materials on Highway Capacity*, 1980.

TABLE 3
LEVEL OF SERVICE DEFINITIONS FOR
STOP-CONTROLLED INTERSECTIONS

Level of Service	Average Total Delay (seconds/vehicle)
А	<u><</u> 10.0
В	> 10.0 and <u><</u> 15.0
С	> 15.0 and <u><</u> 25.0
D	> 25.0 and <u>≤</u> 35.0
E	> 35.0 and <u><</u> 50.0
F	> 50.0

Source: Transportation Research Board, *Highway Capacity Manual 2010.*

For the City of Los Angeles study locations, the "Critical Movement Analysis-Planning", (Transportation Research Board, 1980) method of intersection capacity analysis was used to determine the intersection volume to capacity (V/C) ratio and corresponding level of service at the signalized intersections. Level of service spreadsheets developed by LADOT were used to implement the CMA (Circular 212 Method) methodology.

The 10 signalized study intersections under City of Los Angeles jurisdiction are currently controlled by the City of Los Angeles' Automated Traffic Surveillance and Control (ATSAC) System and Adaptive Traffic Control System (ATCS). In accordance with LADOT procedures, a capacity increase of 10% (0.07 V/C adjustment for ATSAC and 0.03 V/C adjustment for ATCS) was applied to reflect the benefits of ATSAC/ATCS control at these intersections.

The remaining 12 signalized intersections under the jurisdiction of the City of Culver City currently operate under a signal coordination system similar to ATSAC, but have not yet been upgraded with the ATCS-type operations. Therefore, a capacity increase of 7% (0.07 V/C adjustments) was applied to reflect the benefits of ATSAC-type control at these intersections.

The Highway Capacity Manual (HCM) 2010 method of unsignalized intersection analysis was used to determine the delay (in seconds) and corresponding level of service at the stop-controlled intersections. For all-way stop controlled intersections, the intersection delay is defined as the average delay experienced by drivers at the intersection. For two-way stop-controlled locations, the intersection delay is defined as the worst case delay experienced by drivers at the intersection who must stop or yield to unimpeded major street traffic. This method uses a "gap acceptance" technique to predict driver delay and is applicable to unsignalized intersections where there is potential for difficulty for minor street or stopped traffic to cross the traffic on the major or unimpeded street. Table 3 defines the ranges of delay and corresponding levels of service for unsignalized intersections.

Existing Levels of Service

The existing traffic volumes presented in Figures 3A and 3B for AM and PM peak hours were used in conjunction with the level of service methodologies described above, and the current intersection characteristics illustrated in Appendix B, to determine the existing operating conditions at the analyzed intersections.

Table 4 summarizes the results of the intersection capacity analysis for existing conditions at each of the study intersections in the study area. The table indicates the existing V/C ratio during the morning and evening peak hours and the corresponding LOS at the study intersections. As illustrated in the table, 24 of the 26 study intersections are currently operating at LOS D or better during the morning peak hour. During the evening peak hour, 23 of the 26 study intersection are operating at LOS D or better. The remaining locations are operating at LOS E or F and includes:

- Robertson Boulevard/I-10 Westbound On-Ramp: AM Peak Hour LOS F
 PM Peak Hour LOS E
- Wesley Street/Washington Boulevard: PM Peak Hour LOS E
- Cattaraugus Avenue/Washington Boulevard: AM Peak Hour LOS F
 PM Peak Hour LOS E

Capacity calculation worksheets for Existing (2016) conditions are provided in Appendix D of the report.

TABLE 4 **EXISTING (2016) INTERSECTION LEVEL OF SERVICE ANALYSIS**

		Existing (2016) Conditions AM Peak Hour PM Peak Hour			
No.	Intersection	AM Peak V/C or Delay	Hour LOS	Hour LOS	
1.	Robertson Boulevard & I-10 WB Off-Ramp/Kincardine Avenue [1]	0.588	A	V/C or Delay 0.839	D
2.	Robertson Boulevard & National Boulevard [1]	0.892	D	0.817	D
3.	National Boulevard & I-10 Eastbound On-Ramp [1]	0.223	Α	0.452	Α
4.	Bagley Avenue & Venice Boulevard [1]	0.672	В	0.710	С
5.	Culver Boulevard & Venice Boulevard [1]	0.565	Α	0.624	В
6.	Robertson Boulevard & Venice Boulevard [1]	0.728	С	0.721	С
7.	National Boulevard & Venice Boulevard [1]	0.707	С	0.792	С
8.	La Cienega Boulevard & Venice Boulevard [1] [2]	0.813	D	0.814	D
9.	Washington Boulevard/Irving Place & Culver Boulevard [3]	0.656	В	0.648	В
10.	Main Street & Culver Boulevard [3]	0.684	В	0.602	В
11.	Washington Boulevard/Canfield Avenue & Culver Boulevard [3]	0.697	В	0.622	В
12.	Ince Boulevard & Washington Boulevard [3]	0.858	D	0.813	D
13.	Robertson Boulevard/Higuera Street & Washington Boulevard [3]	0.710	С	0.649	В
14.	Landmark Street & Washington Boulevard [3]	0.442	Α	0.444	Α
15.	National Boulevard & Washington Boulevard [3]	0.670	В	0.816	D
16.	Helms Avenue & Washington Boulevard [3]	0.540	Α	0.510	Α
17.	La Cienega Avenue/McManus Avenue & Washington Boulevard [3]	0.573	Α	0.521	Α
18.	La Cienega Boulevard & Washington Boulevard [3]	0.898	D	0.840	D
19.	Wesley Street & National Boulevard [3]	0.429	Α	0.463	Α
20.	Hayden Avenue & National Boulevard [3]	0.461	Α	0.468	Α
21.	Jefferson Boulevard & National Boulevard [1]	0.875	D	0.514	Α
22.	Jefferson Boulevard & Higuera Street/Rodeo Road [1]	0.757	С	0.727	С
23.	Robertson Boulevard & I-10 Westbound On-Ramp [1] [4]	55.2 s	F	41.8 s	E
24.	Robertson Boulevard & Exposition/I-10 Eastbound Off-Ramp [1] [4]	10.4 s	В	14.9 s	В
25.	Wesley Street & Washington Boulevard [3] [5]	22.3 s	С	49.7 s	E
26.	Cattaraugus Avenue & Washington Boulevard [3] [5]	***	F	41.9 s	E
\//C \	olume to Capacity Ratio				

V/C - Volume to Capacity Ratio

LOS - Level of Service

^[1] Study intersection is located within the City of Los Angeles.

^[2] Los Angeles County Congestion Management Program arterial monitoring location.

^[3] Study intersection is located within the City of Culver City.

^[4] All-way stop-controlled intersection. LOS based on average vehicular delay in seconds (s).

^[5] Stop-controlled on minor approach(es). LOS based on worst case approach delay in seconds (s).

*** - Oversaturated conditions per Highway Capacity Manual 2010 (HCM).

EXISTING TRANSIT SERVICE

Fourteen bus lines operated by four different transportation agencies currently serve the study area. Four bus lines are operated by the Culver City Bus (CC), eight bus lines are operated by the Los Angeles County Metropolitan Transportation Authority (MTA), one bus line is operated by the Santa Monica Big Blue Bus (SM) and one bus line is operated by the Los Angeles Department of Transportation (LADOT CE). Metro (MTA) also operates the Light Rail Line (Expo Line). These transit lines are described below:

- <u>CC Line 1</u> Line 1 is a local east/west line that provides service from Venice Beach to West Los Angeles and travels primarily along Washington Boulevard within the study area. This line runs every day, including holidays. The frequency of service during peak commute hours is approximately 10-15 minutes. The western terminus is at the intersection of Windward Avenue and Main Street in Venice. The eastern terminus is at the West Los Angeles Transit Center located at the intersection of Apple Street/Fairfax Avenue in West Los Angeles.
- <u>CC Line 4</u> Line 4 is a local north/south line that provides service from the Playa Vista area to West Los Angeles and travels primarily along Jefferson Boulevard, La Cienega Boulevard, and Fairfax Avenue within the study area. This line runs Monday through Friday at a frequency of approximately 25-40 minutes during peak commute hours. No weekend or holiday service is provided. The southern terminus is in the Playa Vista area. The northern terminus is at the West Los Angeles Transit Center located at the intersection of Apple Street/Fairfax Avenue in West Los Angeles.
- <u>Culver City Bus Line 5</u> Line 5 is a local east/west line that provides service from the west side of Culver City to Blair Hills on the east side, and travels primarily along Culver Boulevard, Washington Boulevard, Higuera Street, Hayden Avenue, and Rodeo Road within the study area. This line operates only when school is in session, Monday through Friday from 7:15-7:40 AM and from 2:45-4:05 PM. No weekend or holiday service is provided. It provides westbound/eastbound service from the intersection of Elenda Street/Braddock Drive (Culver City Schools) to the intersection of La Cienega Boulevard/Rodeo Road and eastbound only service from Venice High School (at Maplewood Road) to Culver City Schools.
- <u>Culver City Bus Line 7</u> Line 7 is a local east/west line that provides service from Marina Del Rey to Culver City and travels primarily along Washington Boulevard, Venice Boulevard, and Culver Boulevard within the study area. This line runs Monday through Friday at a frequency of approximately 30-40 minutes. Service on weekends and holidays is not provided. The western terminus is at Fisherman's Village in Marina Del Rey. The eastern terminus is at the Metro Expo Line Robertson Station in Culver City.
- Metro Line 17 Line 17 is a local east/west line that provides service from West Los Angeles to Culver City and travels primarily along Robertson Boulevard, National Boulevard, and Washington Boulevard within the study area. This line runs Monday through Friday at a frequency of approximately 30-35 minutes during peak commute hours. Service is not provided on weekends and holidays. The southern terminus is at

the Metro Expo Line Robertson Station in Culver City. The northern terminus is at the Beverly Center in West Los Angeles.

- Metro Line 33 Line 33 is a local east/west line that provides service from Santa Monica to Downtown Los Angeles and travels primarily along Venice Boulevard within the study area. This line runs every day, including holidays, at a frequency of approximately 6-15 minutes in the northbound direction and 15-20 minutes in the eastbound direction during peak commute hours. The western terminus is at the intersection of Ocean Avenue/Santa Monica Boulevard in Santa Monica. The eastern terminus is at the Patsaouras Transit Plaza (Union Station) in Downtown Los Angeles.
- Metro Line 37 Line 37 is a local east/west line that provides service from West Los Angeles to Downtown Los Angeles and travels primarily along Adams Boulevard, Washington Boulevard, and Fairfax Avenue within the study area. This line runs every day, including holidays, at a frequency of 5-8 minutes during peak commute hours. The western terminus is at the West Los Angeles Transit Center located at the intersection of Apple Street/Fairfax Avenue in West Los Angeles. The eastern terminus is at the intersection of Beaudry Avenue/1st Street in Downtown Los Angeles.
- Metro Line 38 Line 38 is a local east/west line that provides service from West Los Angeles to Downtown Los Angeles and travels primarily along Jefferson Boulevard, La Cienega Boulevard, Washington Boulevard, and Fairfax Avenue within the study area. This line runs every day, including holidays, at a frequency of approximately 12-24 minutes during peak commute hours. The western terminus is at the West Los Angeles Transit Center located at the intersection of Apple Street/Fairfax Avenue in West Los Angeles. The eastern terminus is at the intersection of Broadway/Venice Boulevard in Downtown Los Angeles.
- Metro Line 105 Line 105 is a local southeast/northwest line that provides service from West Hollywood to Vernon and travels primarily along Fairfax Avenue, La Cienega Boulevard, and Rodeo Road within the study area. This line runs every day, including holidays, at a frequency of approximately 10-20 minutes during peak commute hours. The northwestern terminus is at the intersection of San Vicente/Santa Monica Boulevard in West Hollywood. The southeastern terminus is at the intersection of Santa Fe/Vernon Avenue in Vernon.
- Metro Line 217 Line 217 is a local north/south line that provides service from West Los Angeles to Hollywood and travels primarily along Fairfax Avenue within the study area. This line runs every day, including holidays, at a frequency of approximately 12-20 minutes during peak commute hours. The southern terminus is at the Howard Hughes Center located near the intersection of Sepulveda Boulevard/Centinela Avenue in Fox Hills. The northern terminus is at Vermont/Sunset Metro Station in Hollywood.
- MTA 705 Line 705 is a northwest/southeast 'Rapid Bus' line that provides service from West Hollywood to Vernon and travels primarily along Fairfax Avenue and Rodeo Road within the study area. This line runs Monday through Friday at a frequency of approximately 10-20 minutes during peak commute hours. No service is provided on weekends or holidays. The northern terminus is at the intersection of San Vicente Boulevard/Santa Monica Boulevard in West Hollywood. The southern terminus is at the intersection of Santa Fe/Vernon Avenue in the Vernon.

- MTA 733 Line 733 is an east/west 'Rapid Bus' line that provides service from Santa Monica to Downtown Los Angeles and travels primarily along Venice Boulevard within the study area. This line runs Monday through Friday at a frequency of approximately 10-20 minutes during peak commute hours. Service is also provided on weekends and holidays. The western terminus is at the intersection of Ocean Avenue/Arizona Avenue in Santa Monica. The eastern terminus is at the Patsaouras Transit Plaza (Union Station) in Downtown Los Angeles.
- Santa Monica Big Blue Bus Line 17 Line 17 is a local north/south line that provides service from Westwood to Culver City and travels primarily along Robertson Boulevard, National Boulevard, and Washington Boulevard within the study area. This line runs every day at a frequency of 30-35 minutes during peak commute hours. No holiday service is provided. The northern terminus is at the University of California, Los Angeles (UCLA) in Westwood. The Southern terminus is at the Metro Expo Line Robertson Station in Culver City.
- <u>LADOT Commuter Express Line 437</u> Line 437 is a LADOT Commuter Express line that provides service from Downtown Los Angeles to Marina Del Rey and travels primarily along Washington Boulevard and Culver Boulevard within the study area. This line runs Monday through Friday and provides service only during peak commute hours. During the morning peak hours, it runs in the eastbound direction only, from Marina Del Rey to Downtown Los Angeles, with a frequency of approximately 22-24 minutes. During the evening peak hours, it runs in the westbound direction only, from Downtown Los Angeles to Marina Del Rey, with a frequency of approximately 30 minutes. Service is not provided during weekday off-peak hours and on weekends and holidays. The western terminus is at the intersection of Pacific Avenue/Washington Boulevard in Marina Del Rey. The eastern terminus is at the intersection of San Pedro Street/Temple Street in Downtown Los Angeles.
- Metro Expo Line Expo Line is an east/west light-rail line that provides service from Union Station to Santa Monica with a station in Culver City. This line runs every day, including holidays, at a frequency of approximately 12 minutes during peak commute hours.

These transit lines within the study area are illustrated in Figure 4. It can be observed from Figure 4 that there is a robust transit network serving the study area. Further, the Metro Expo Line Light-Rail Train (LRT) with its station located just east of the Project site at the intersection of National Boulevard/Washington Boulevard provides mass transit connections to the University of Southern California (USC), Downtown Los Angeles, West Los Angeles and Downtown Santa Monica.

FIGURE 4
EXISTING TRANSIT LINES

EXISTING BICYCLE FACILITIES

The City of Culver City Bicycle Plan and City of Los Angeles 2010 Bicycle Plan documents the existing and planned bicycle facilities within each respective jurisdiction. Class I Bikeways (Bike Path) provide an exclusive paved right-of-way separated from the street or highway. Class II Bikeways (Bike Lane) provide a striped and signed bike lane for one-way travel on a street or highway. Class III Bikeways (Bike Routes) provide for a shared use of the roadway with posted signage for bicycle use which can include Sharrow pavement markings. In the study area, bicycle facilities are provided on the following roadways:

- Along Expo Line: La Cienega Boulevard to Washington Boulevard (Bike Path)
- Ballona Creek: Jefferson Boulevard to Duquesne Avenue (Bike Path)
- Venice Boulevard: Hughes Avenue to Fairfax Avenue (Bike Lane)
- Jefferson Boulevard: La Cienega Boulevard to La Brea Avenue (Bike Lane)
- Jefferson Boulevard: National Boulevard to Duquesne Avenue (Bike Lane)
- Duquesne Avenue: south of Jefferson Boulevard (Bike Lane)
- Jefferson Boulevard: National Boulevard to La Cienega Boulevard(Bike Route/Sharrows)
- Wesley Street: Higuera Street to National Boulevard (Bike Route/Sharrows)
- Lucerne Avenue: Higuera Street to Duquesne Avenue (Bike Route/Sharrows)
- Higuera Street: Lucerne Avenue to Wesley Street (Bike Route/Sharrows)
- Irving Place: Lucerne Avenue to Culver Boulevard (Bike Route/Sharrows)
- Van Buren Place: A Street to Lucerne Avenue (Bike Route/Sharrows)
- A Street: Irving Place to Van Buren Place (Bike Route/Sharrows)
- Along Expo Line/National Boulevard: La Cienega Boulevard to Washington Boulevard (Bike Path)
- North side of Washington Boulevard between Wesley Street and National Boulevard (Bike Lane). Bike lanes will be installed on the south side of Washington Boulevard between Wesley Street and National Boulevard with the development of 8770 Washington Boulevard project.
- South side of Washington Boulevard between Landmark Street and Expo bridge.
- Bike lanes will be installed on both sides of National Boulevard between Venice Boulevard and Washington Boulevard with the Ivy Station project.

The City of Culver City is preparing a feasibility study to provide a bicycle trail between the Expo Line Station and Downtown Culver City, also known as the Expo-to-Downtown Bicycle Connector. This bikeway would potentially include a two-way protected bike lane with bicycle signalization. This bike trail would be located along the north side of Washington Boulevard between Wesley Street and Robertson Boulevard; and along the south side of Washington Boulevard between Robertson Boulevard and Ince Boulevard. An additional alignment is planned along the west side of Robertson Boulevard between Venice Boulevard and Washington Boulevard. Details on the "Expo to Downtown Bicycle Connector Facility" are attached in Appendix F.

III. PROJECT TRAFFIC PROJECTIONS

In order to properly evaluate the potential impact of the Proposed Project on the local street system, estimates of the Project traffic volumes were developed. The traffic generated by the Proposed Project was estimated and assigned separately to the street system. The addition of Project traffic and existing traffic volumes represents the Existing (2016) plus Project scenario. Traffic projections for future scenarios are described in the next chapter.

PROJECT TRAFFIC VOLUMES

The development of traffic generation estimates for the Proposed Project involves the use of a three-step process: trip generation, trip distribution and traffic assignment.

Project Trip Generation

Implementation of the Proposed Project consists of 59,325 square feet of office use, 2,878 square feet of retail use, and 3,184 square feet of restaurant (high-turnover) use. The existing site contains an auto repair facility with a building size of 9,992 square feet which will be demolished.

Utilizing the ITE's *Trip Generation Manual*, 9th Edition trip rates, the Proposed Project's trip generation was determined. Table 5 presents details of the Proposed Project's trip generation including type of use, size, applicable rate and trip generation estimates. Other calculations within the tables also provide for trip generation reductions from transit trips, internal capture, pass-by trips and existing use trip credit.

From Table 5, it can be observed that the Proposed Project's trip generation would result in a net total of approximately 1,146 daily trips of which 100 trips would occur during the morning peak hour and 124 trips during the evening peak hour.

TABLE 5 ESTIMATED PROJECT TRIP GENERATION

				AM Peak Hour		PM Peak Hour			
		Size	Daily	IN	OUT	TOTAL	IN	OUT	TOTAL
Proposed Project									
Office		59,325 s.f.	883	111	15	126	25	120	145
	Transit	Trip Use (25%)	(221)	(28)	(4)	(32)	(6)	(30)	(36)
*Inte	rnal Capture (1	0%) Trip Credit	(66)	(8)	(1)	(9)	(2)	(9)	(11)
Retail		2,878 s.f.	677	11	7	18	27	29	56
Inte	rnal Capture (1	0%) Trip Credit	(68)	(1)	(1)	(2)	(3)	(3)	(6)
**	Pass-By Trip R	Reduction (25%)	(152)	(3)	(1)	(4)	(6)	(7)	(13)
High-Turnover Restaurant		3,184 s.f.	405	19	15	34	19	12	31
3	rnal Canture (1	0%) Trip Credit	(41)	(2)	(1)	(3)	(2)	(1)	(3)
		Reduction (25%)	(91)	(4)	(4)	(8)	(4)	(3)	(7)
	400 Z)p	(20,70)	(0.)	(.)	(. ,	(0)	(.)	(0)	(,,
Existing Uses (to be removed)									
Auto Repair Shop		9,992 s.f.	200	15	7	22	17	19	36
Pass-By Trip Reduc		Reduction (10%)	(20)	(2)	0	(2)	(2)	(2)	(4)
Due			4.446	00	18	100	22	04	124
Project Net Trip Generation Total		1,146	82	18	100	33	91	124	
Trip Generation Rates [1]									
Office (ITE Land Use 710) Trips		Trips per 1,000 s.f.	[2]	88%	12%	[2]	17%	83%	[2]
Retail/Shopping Center (ITE Land	l Use 820)	Trips per 1,000 s.f.	[3]	62%	38%	[3]	48%	52%	[3]
High-Turnover Restaurant (ITE La	and Use 932)	Trips per 1,000 s.f.	127.15	55%	45%	10.81	60%	40%	9.85
Automobile Care Center (ITE Land Use 942) Trips per 1,000		Trips per 1,000 s.f.	20.00 [4]	66%	34%	2.25	48%	52%	[5]

^{*} Internal capture trips determined after reduction of transit trips.

Daily: Ln(T) = 0.76 Ln(X) + 3.68 Where:

AM Peak Hour: Ln(T) = 0.80 Ln(X) + 1.57 Ln = Natural logarithm

PM Peak Hour: T = 1.12 (X) + 78.45 T = Two-way volume of traffic (total trip-ends)

X = Area in 1,000 square feet gross floor area

[3] Trip generation for retail/shopping center was calculated using the following equations:

Where:

Daily: Ln(T) = 0.65 Ln(X) + 5.83 Ln = Natural logarithm

AM Peak Hour: Ln(T) = 0.61 Ln(X) + 2.24 T = Two-way volume of traffic (total trip-ends) PM Peak Hour: Ln(T) = 0.67 Ln(X) + 3.31 X = 1,000 square feet gross leasable area

[4] ITE does not provide a daily trip generation rate for this use. Therefore, the daily trip rate for this use from Brief Guide of Vehicular Traffic Generation Rates for the San Diego Region, SANDAG, April 2002 was utilized.

[5] PM trip generation for automobile care center was calculated using the following equation:

Mhara.

PM Peak Hour: T = 2.41 (X) + 11.79 T = Two-way volume of traffic (total trip-ends)

X = 1,000 square feet occupied gross leasable area

^{**} Pass-by trips determined after reduction of internal capture trip credit.

^[1] Trip generation rates from *Trip Generation Manual*, 9th Edition, ITE 2012, unless otherwise noted.

^[2] Trip generation for office was calculated using the following equations:

Project Trip Distribution

The geographic distribution for Project trips was assumed to be the following:

To and From the North: 20%
To and From the South: 15%
To and From the East: 35%
To and From the West: 30%

Intersection level trip distribution percentages are shown in Figure 5. Based on these distribution assumptions, location and points of access of the project driveways, and trip generation estimates from the Proposed Project, traffic estimates of project-only trips were developed. These project-only trips are presented in Figures 6A and 6B.

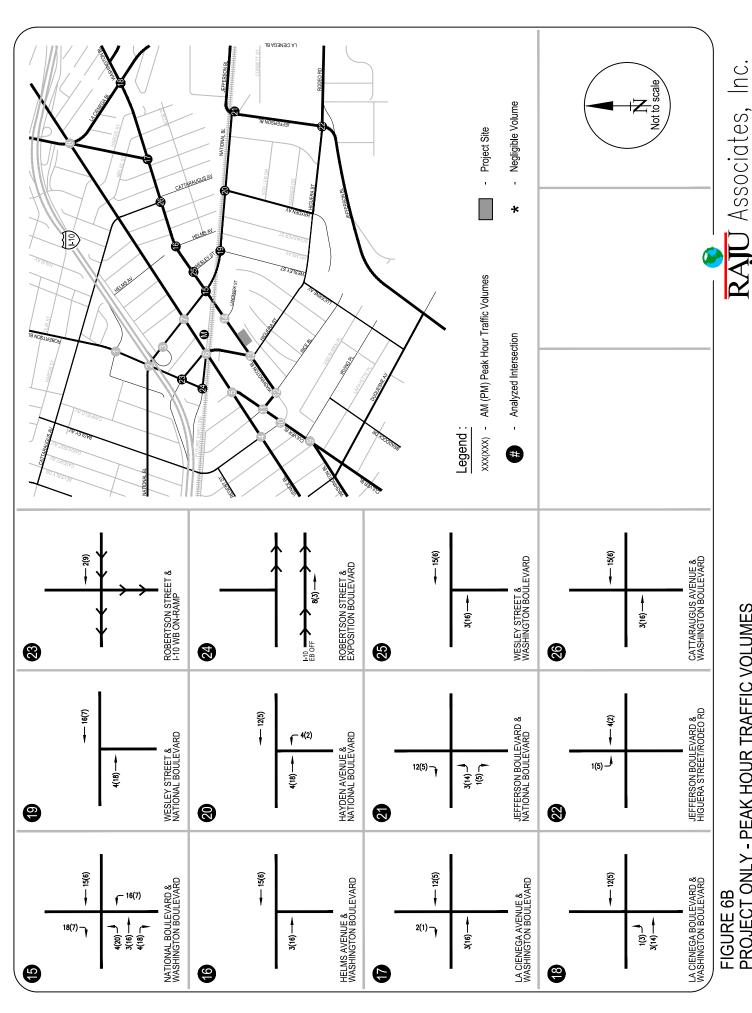
EXISTING (2016) PLUS PROJECT TRAFFIC VOLUMES

Utilizing the project-only traffic estimates developed for both AM and PM peak hours, traffic forecasts for the Existing (2016) plus Project conditions were developed. The existing (2016) traffic volumes were combined with the project-only traffic volumes to obtain the Existing with Project traffic volume forecasts. The Existing (2016) plus Project traffic volumes during both AM and PM peak hours are presented in Figures 7A and 7B.

FIGURE 5 PROJECT TRIP DISTRIBUTION

FIGURE 6A PROJECT ONLY - PEAK HOUR TRAFFIC VOLUMES

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PROJECT ONLY - PEAK HOUR TRAFFIC VOLUMES

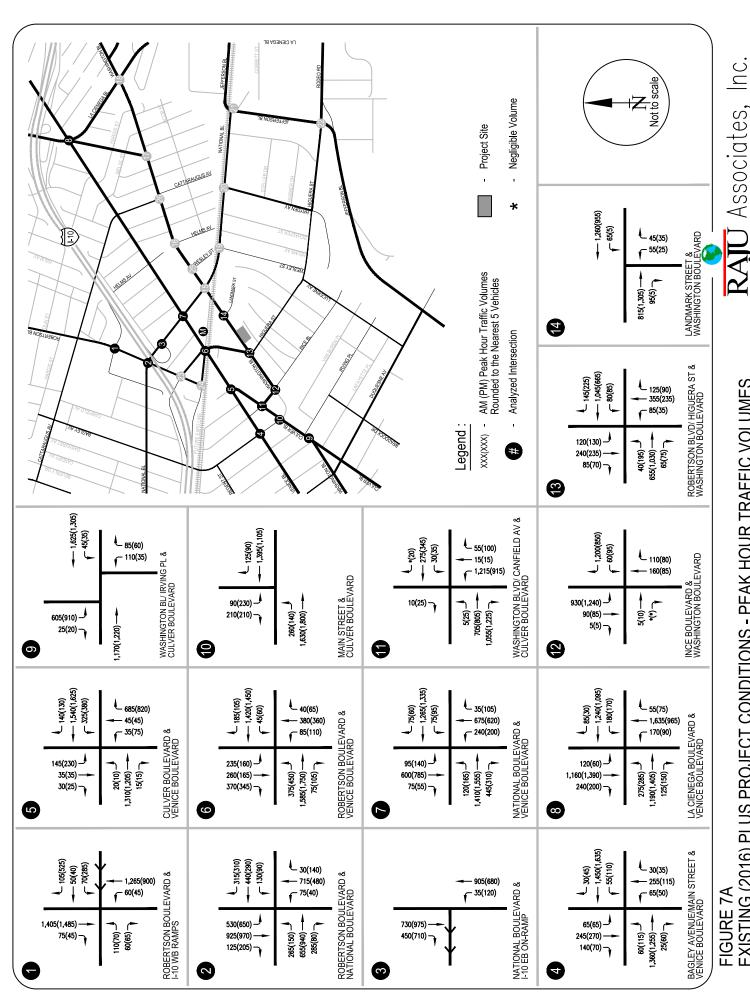
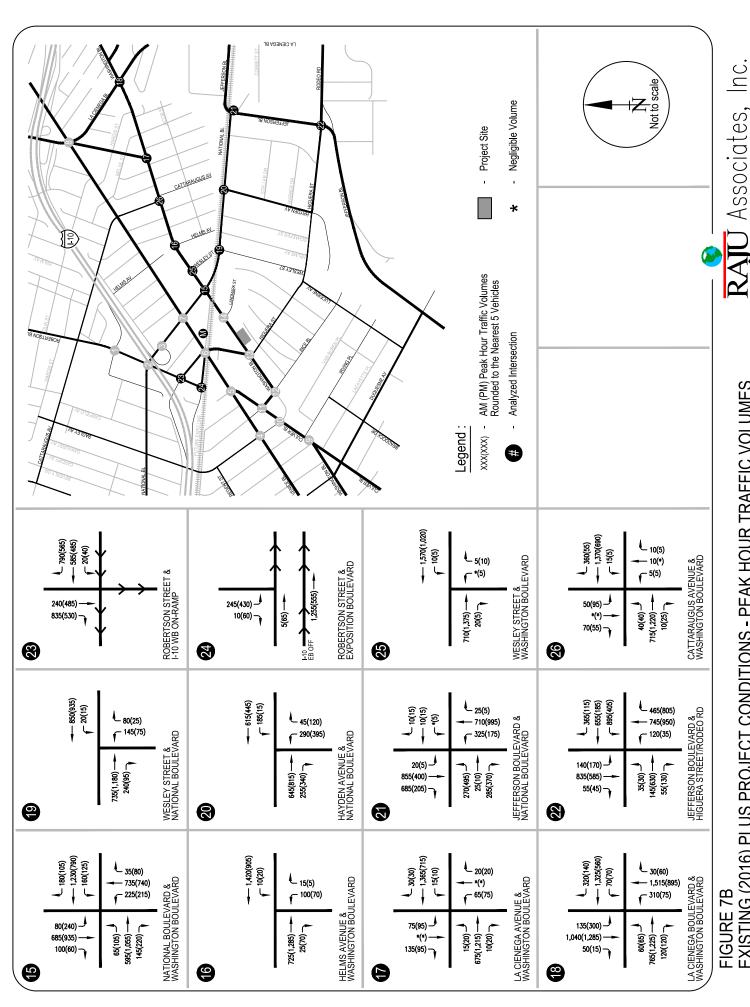


FIGURE 7A EXISTING (2016) PLUS PROJECT CONDITIONS - PEAK HOUR TRAFFIC VOLUMES



EXISTING (2016) PLUS PROJECT CONDITIONS - PEAK HOUR TRAFFIC VOLUMES

IV. FUTURE YEAR 2018 TRAFFIC PROJECTIONS

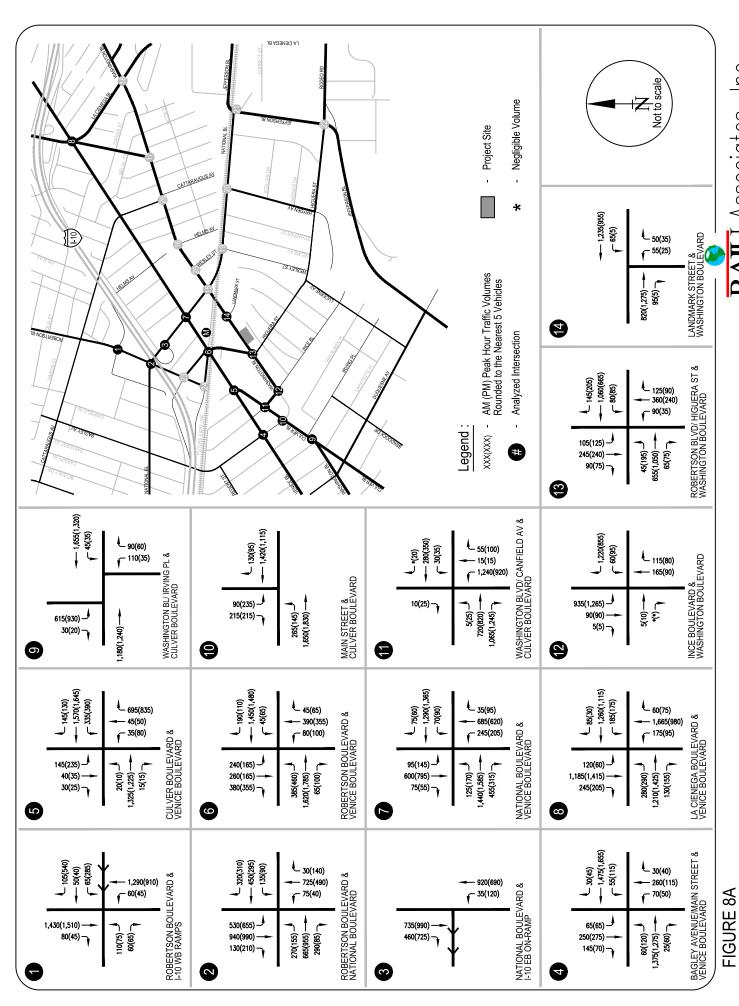
In order to properly evaluate the potential impact of the Proposed Project on the local street system, estimates of the Future Year 2018 traffic volumes both with and without the Project were developed. The Future Year 2018 without the Project was first developed including estimates for background growth in area-wide trip making and trips generated by future developments (related projects) in the vicinity of the study area. The Future (2018) without Project traffic represents the cumulative base conditions. Next, the traffic generated by the Proposed Project was estimated and assigned separately to the street system. The addition of Project traffic and the cumulative base traffic volumes provides traffic volume estimates for the Future Cumulative (2018) plus Project scenario. Each of these future traffic scenarios is described further in this chapter.

CUMULATIVE (2018) BASE TRAFFIC PROJECTIONS

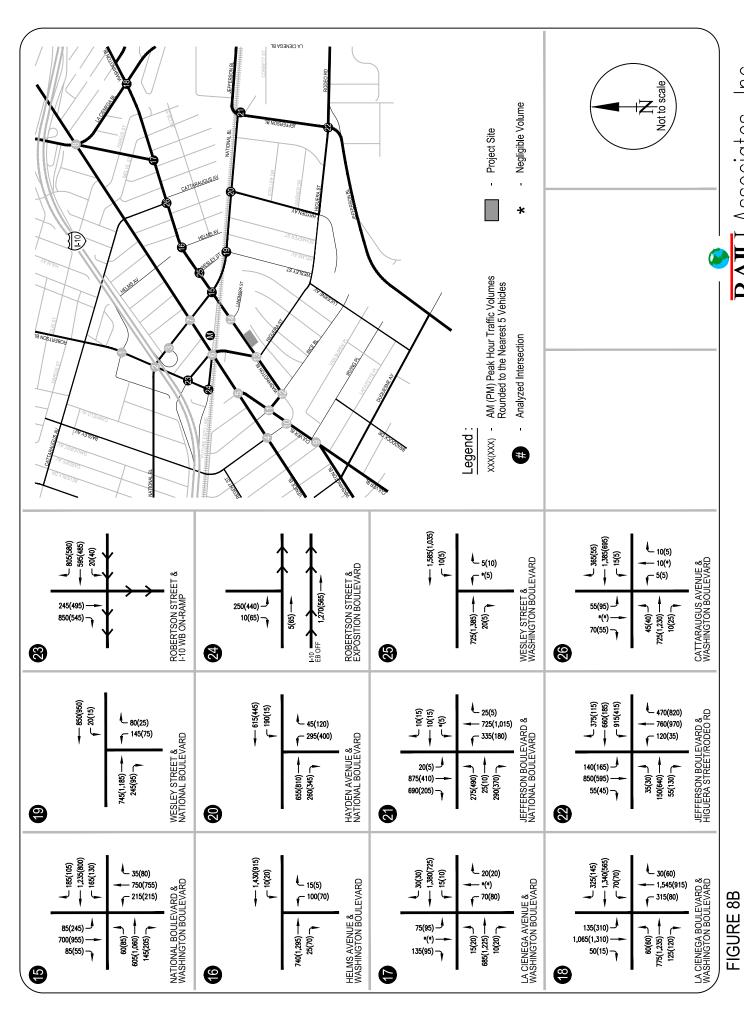
The Cumulative (2018) Base traffic projections reflect growth in traffic from two primary sources: Firstly, the background or ambient growth to reflect the effects of overall area-wide regional growth both within and outside the study area; and secondly, from traffic generated by specific related (cumulative) projects located within, or in the vicinity of, the study area. Each of these components is described below.

Area-wide Ambient Traffic Growth

The traffic in the vicinity of the study area was estimated to increase at a rate of about 1.0% per year per the Memorandum of Understanding. Future increases in background traffic volumes due to regional growth and development are expected to continue at this rate. With the assumed completion date of 2018, the Existing 2016 traffic volumes were adjusted upward by a factor of 2% to reflect this area-wide regional growth. The resulting Existing plus Ambient Growth (2018) traffic volumes are illustrated in Figures 8A and 8B.



EXISTING WITH AMBIENT GROWTH (2018) CONDITIONS - PEAK HOUR TRAFFIC VOLUMES m RAJU Associates, Inc.



EXISTING WITH AMBIENT GROWTH (2018) CONDITIONS - PEAK HOUR TRAFFIC VOLUMES m RAJU Associates, Inc.

Related Projects Traffic Generation and Assignment

As indicated, the second potential source of traffic growth in the study area is that expected from other future development projects in the vicinity. These related or "cumulative" projects are those developments that are planned and expected to be in place within the same timeframe as the Proposed Project. Data describing related projects in the area was solicited from the City of Culver City and the City of Los Angeles. Thirty-three (33) related projects were identified within the study area and are listed in Table 6. The locations of these projects are shown in Figure 9.

The trip generation estimates for the related projects were based on different sources including trip generation rates contained in the ITE's *Trip Generation Manual*, 9th Edition, trip generation estimates provided by the recently completed traffic studies for projects in Culver City, and trip generation estimates for the related projects within the City of Los Angeles provided by the City of Los Angeles Department of Transportation. The trip generation estimates for the related projects are shown in Table 6. As summarized in Table 6, the related projects are expected to generate approximately 3,621 trips during the morning peak hour and 4,197 trips during the evening peak hour. The geographic distribution and the traffic assignment of the related projects were performed and the results are shown in Figures 10A and 10B.

Cumulative (2018) Base Traffic Volumes

The related projects' traffic estimates were added to the Existing plus Ambient Growth traffic to obtain the Cumulative (2018) Base traffic volumes. Figures 11A and 11B provides the Cumulative (2018) Base traffic volumes at each of the analysis intersections during both AM and PM peak hours. These volumes represent Future (2018) Cumulative Base (without project) conditions.

CUMULATIVE (2018) PLUS PROJECT TRAFFIC VOLUMES

Utilizing the project-only traffic estimates developed for both AM and PM peak hours, traffic forecasts for the Future Year 2018 plus Project conditions were developed. The Cumulative (2018) Base traffic forecasts were combined with the project-only traffic volumes to obtain the Future with Project traffic volume forecasts. The Future Year 2018 Cumulative plus Project traffic volumes during both AM and PM peak hours are presented in Figures 12A and 12B.

TABLE 6 ESTIMATED WEEKDAY TRIP GENERATION OF RELATED PROJECTS

Map No.	Project Name	Location	Description	Daily	IN A	M Peak Ho	ur TOTAL	IN PI	I Peak Ho	TOTAL
	Culver City [1]	Location	Besonption	Dully		001	TOTAL			TOTAL
1	Residential Project	3440 Caroline Avenue	Two (2) new detached residential condominium	6	0	0	0	1	0	1
2	Mixed-Use Project	9355 Culver Boulevard	dwelling units (net addition of one unit) Three story mixed use building consisting of a ground level salon, mezzanine, and office totaling 2,947 s.f., and four residential units on the third floor.	89	4	2	6	3	5	8
3	The Wende Museum	10808 Culver Boulevard	Tenant improvements to convert existing 12,596 s.f. armory building into a museum	57	4	1	5	0	8	8
4	Chapel/Dormitory Project	10775 Deshire Place	4,740 s.f. addition to existing dormitory and replace existing chapel with a 1,660 s.f. chapel.	82	2	4	6	4	3	7
5	Residential Project	4109-4111 Duquesne Avenue	Addition of two (2) residential dwelling units to existing duplex	12	0	1	1	1	0	1
6	Residential Project	4139-4145 Duquesne Avenue	Seven unit condominiums with 15 subterranean parking spaces.	41	1	2	3	3	1	4
7	Residential Project Retail/Restaurant Project	4058 Madison Avenue 8511 Warner Drive	New four unit condominium, 7,422 s.f. total.	41	1	2	3	3	1	4
8	Retail/Restaurant Project	8511 Warner Drive	Five level parking structure with retail/restaurant. 51,520 s.f. of retail/restaurant uses. Parking Structure -307,522 s.f.	3,112	93	70	163	109	103	212
9	Mixed-Use Project [2]	8770 Washington Boulevard	TOD Mixed Use with 31,240 s.f. of retail and restaurant uses and 115 residential units (5 story)	2,914	69	85	154	150	125	275
10	Platform Project [3]	8810-8850 Washington Boulevard & 3920 Landmark Street	New commercial development (38,732 s.f. office, 41,745 s.f. of retail and restaurant)	2,357	71	20	91	100	100	200
11	Mixed-Use Project	8777 Washington Boulevard	Construct 4,500 s.f. of retail and 128,000 s.f. of office use. Demolish existing 12,485 s.f. of retail use and 4,731 s.f. of restaurant use.	30	123	-3	120	-23	92	69
12	Triangle Site - Washington/National TOD [4]	Corner of Washington Boulevard/National Boulevard	Transit oriented development to include 200 d.u, mid- rise apartments, 148-room hotel, 201,000 s.f. office, 24,000 s.f. specialty retail, 10,000 s.f. of high-turnover restaurant & 10,000 s.f. quality restaurant.	4,124	173	83	256	127	174	301
13	The Culver Studios [5]	9336 Washington Boulevard	Net increase of 138,997 s.f. of office and support facilities.	1,564	149	20	169	45	114	159
14	Office & Retail Project	10000 Washington Boulevard	Renovation of existing 9-story office building. Convert ground floor lobby space to office, retail and restaurant space. New construction includes a new stand-alone 3,115 sq. ft. one-story restaurant building and a second floor within the atrium to add 5,500 sq. ft. of office space.	3,612	136	81	217	102	112	214
15	Sony Pictures	10202 Washington Boulevard	New 8-story, 218,450 s.f. office building, a new 4- story, 51,716 s.f. Production Services support building, and expansion of an existing parking structure. Total demolition of 57,642 s.f. Net New square feet is 212.524 s.f.	2,328	308	42	350	54	262	316
16	Sony Pictures	10202 Washington Boulevard	New 22,929 s.f. 4- story office building (net new 9,875 s.f.).	109	13	2	15	3	12	15
17	Union 76	10638 Culver Boulevard	Gas station and convenience store; 2,676 G.S.F.	651	21	20	41	9	45	54
18	Willows School Comprehensive Plan	809 Higuera & 8476 Warner	Phase II & III - increase student enrollment by 100, from 475 to 575	276	50	40	90	3	15	18
19	Culver Center Shopping Center - New restaurant	10799 Washington Blvd	New 2,000 sq. ft. restaurant at existing commercial shopping center	254	12	10	22	12	8	20
20	Parcel B [5]	9300 Culver Blvd	118,000 G.S.F. of office, retail, and restaurant space.	3,702	124	31	155	167	188	355
21	Three unit condominium/ townhome Redevelopment	4241 Duquesne Avenue	New three detached condominium/ townhomes, resulting in two net new residential dwelling units	17	0	1	1	1	1	2
22	Office Building	9919 Jefferson Blvd	New 3-story, 62,558 sq. ft., office and research and development (laboratory) building, as well as a five (5) level parking structure containing 398 parking spaces, and associated site improvements	919	115	16	131	25	124	149
23	Lorcan O'Herlihy Architects	3434 Wesley St	New TOD Mixed Use project with 15 dwelling units, and 14,237sq. ft. of office/gallery on a vacant lot.	278	16	9	25	16	20	36
City of 24	Los Angeles [6] Apartment [7]	3822 S. Dunn Drive	7-story, 86-Unit Apartment building over ground floor	543	8	34	42	33	17	50
25	Wrapper Office Building Project	5790 W. Jefferson Boulevard	Construct new 10-story 150,761 s.f. office building	1,794	234	32	266	42	205	247
26	Jefferson & La Cienega Mixed Use Project [8]	3221 S. La Cienega Boulevard	Converting existing ABC Lot to a Mixed-Use: 1,218- Unit Apartment, 200,000 s.f. Office, 50,000 s.f. Grocery Store, 30,000 s.f. Retail & 20,000 s.f. Restaurant project.	10,136	319	419	738	467	382	849
27	Mixed-use Apartment & Retail	3425 Motor Avenue	115-unit apartment and 975 s.f. retail. Existing 15 apartment units, 2 single family dwellings and 3,300 s.f. office to be demolished.	999	12	43	55	58	35	93
28	Restaurant & Retail [7]	10612 National Blvd	1,726 s.f. Coffee Shop (Coffee Bean) including 250 s.f. Outdoor Seating. Existing vacant lot.	636	46	38	84	19	12	31
29	Mixed-Use: Apartment & Restaurant [7]	3644 S. Overland Avenue	New Mixed-Use: 92-Unit Apartment & 1,573 sf Restaurant use (110 spaces).	750	17	42	59	38	22	60
30	Venice Fairfax Residential Project	5930 W. Sawyer Street	Construct 60 single-family homes	656	13	39	52	42	24	66
31	Coffee Shop with Drive Through [7]	9829 W. Venice Boulevard	Coffee Bean & Tea Leaf Coffee Shop with Single- Lane Drive Through to replace existing Rally's with Dual-Lane Drive Through.	145	13	12	25	3	2	5
32	Mixed-use Apartment & Retail	9901 Washington Boulevard	131-unit apartment & 12,000 s.f. retail. Existing 16,900 s.f. retail to be removed.	507	8	50	58	42	12	54
33	Mixed-use Apartment, office, retail, and restaurant	10601 Washington Boulevard	126-unit apartment, 23,000 s.f. office, 9,000 s.f. retail, 9,000 s.f. restaurant. Existing 10,000 s.f. office to be removed.	3,595	106	112	218	170	144	314
			RELATED PROJECTS TRIP GENERATION TOTAL	46,336	2,261	1,360	3,621	1,829	2,368	4,197

^{*} Trip generation estimates are based on trip generation rates included in Trip Generation Manual, 9th Edition, ITE 2012, unless noted otherwise.

^[1] Source: Culver City Planning Division Active Projects List - January 29, 2016.

^[2] Trip generation from Traffic Impact Analysis Report, Proposed Mixed-Use Development (115-Unit Residential and 31,240 Square Foot Retail) Located at 8770 Washington Boulevard in Culver City, California Hirsch/Green Transportation Consulting, Inc., July 2010.

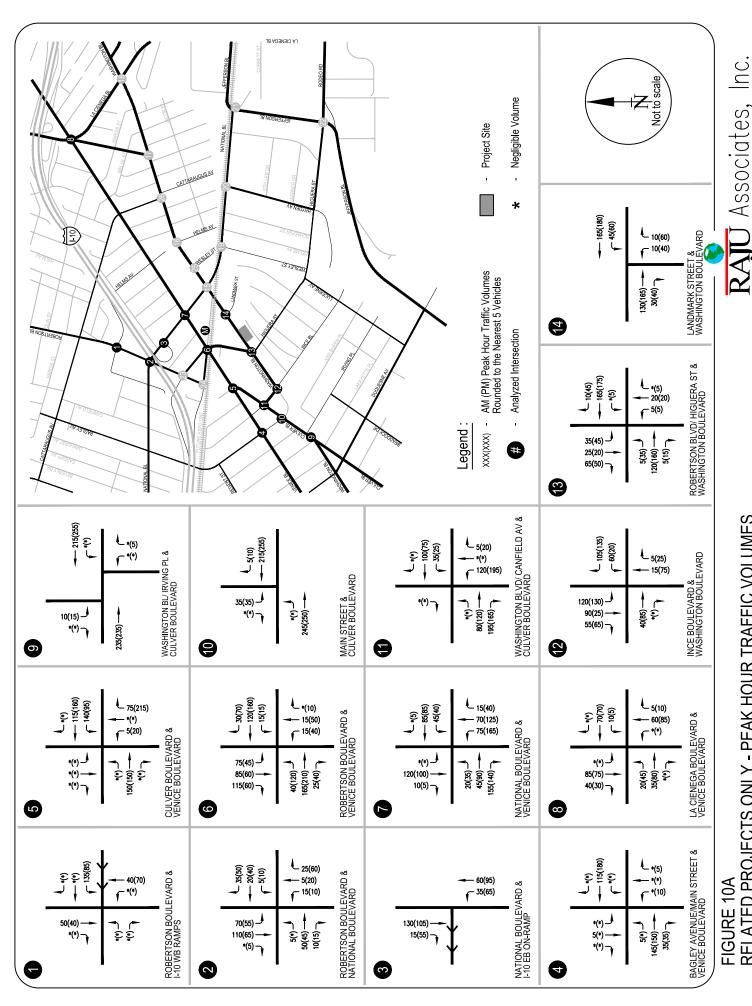
^[3] Trip generation from Traffic Study for the Platform at Culver Station Project, Raju Associates Inc., July 2011.

^[4] Trip generation estimates provided by the City of Culver City.

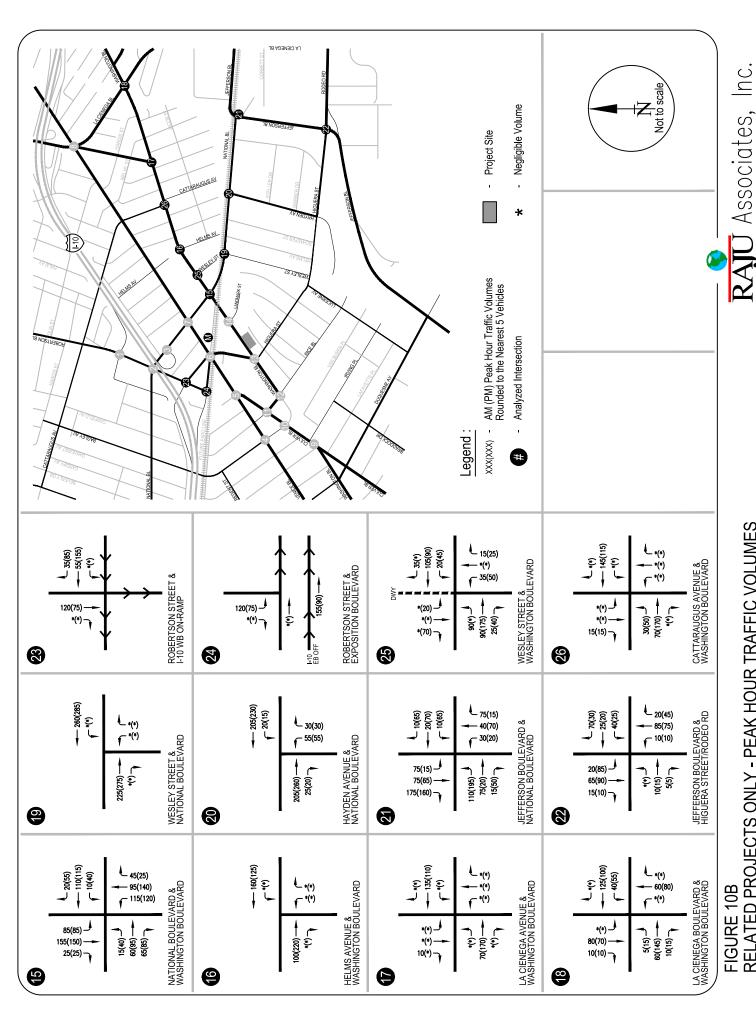
^[5] Trip generation from Culver Studios Modified Comprehensive Plan Update #6, Transportation Analysis Report Fehr & Peers, September 2015.

^[6] Source: Los Angeles Department of Transportation.
[7] Trip generation totals provided by LADOT, February 2011. Directional distribution based on *Trip Generation Manual*, \$th Edition, ITE 2012.
[8] Trip generation from *Traffic Study for the Jefferson & La Cienega Mixed-Use Development*, Gibson Consulting, Inc., June 2015.

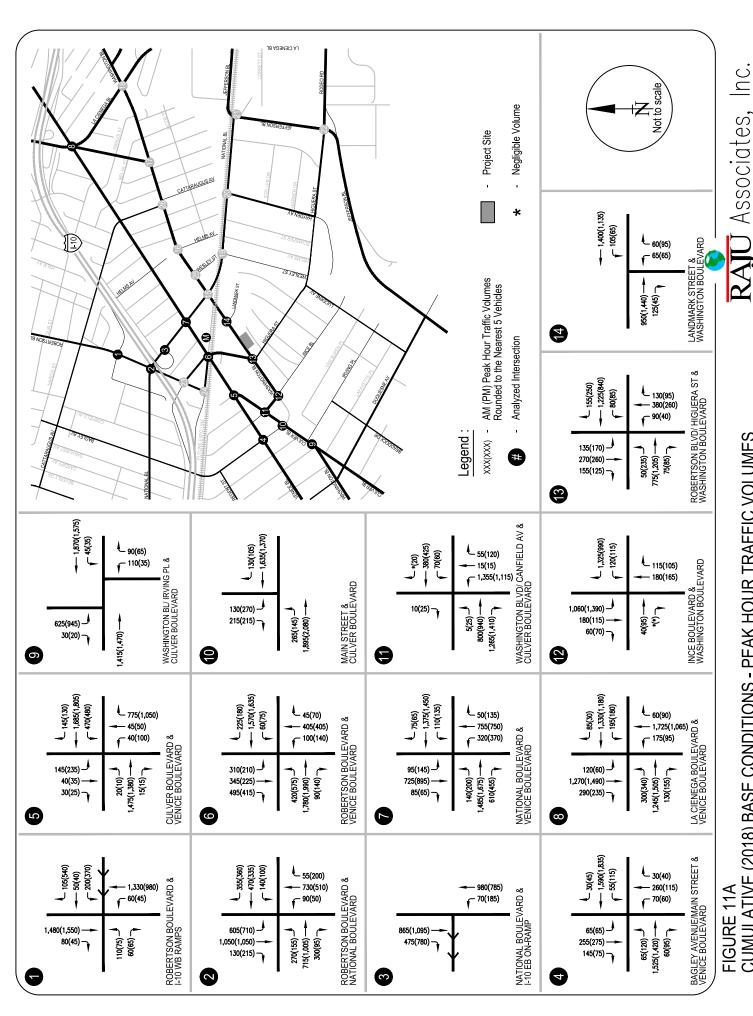
FIGURE 9 LOCATION OF RELATED PROJECTS



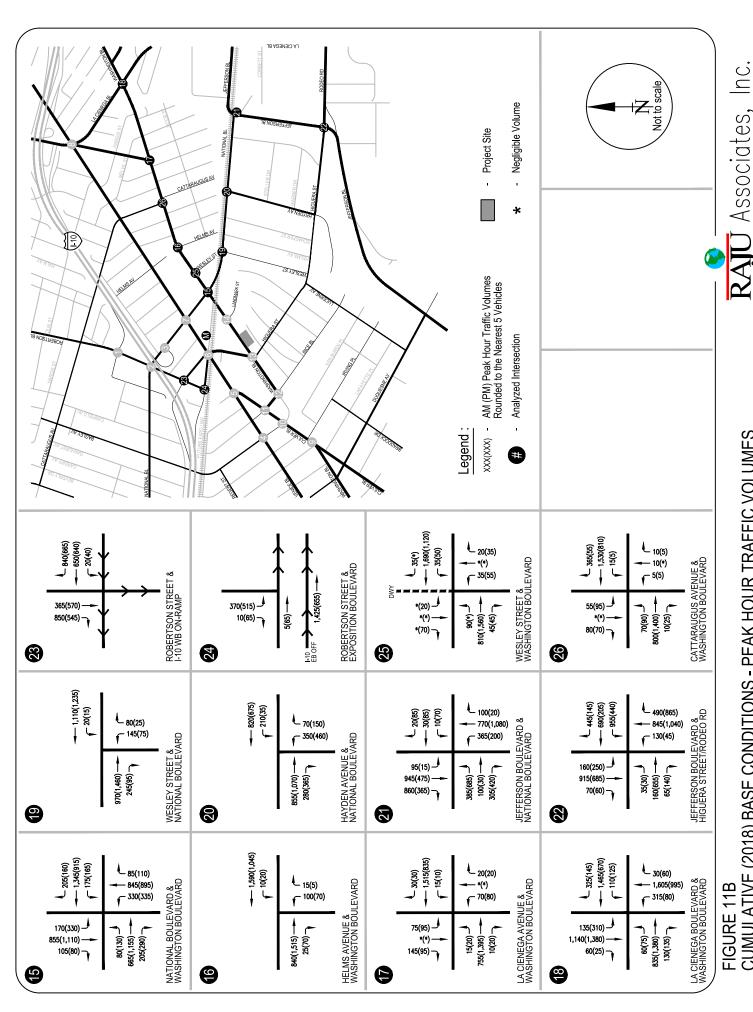
RELATED PROJECTS ONLY - PEAK HOUR TRAFFIC VOLUMES



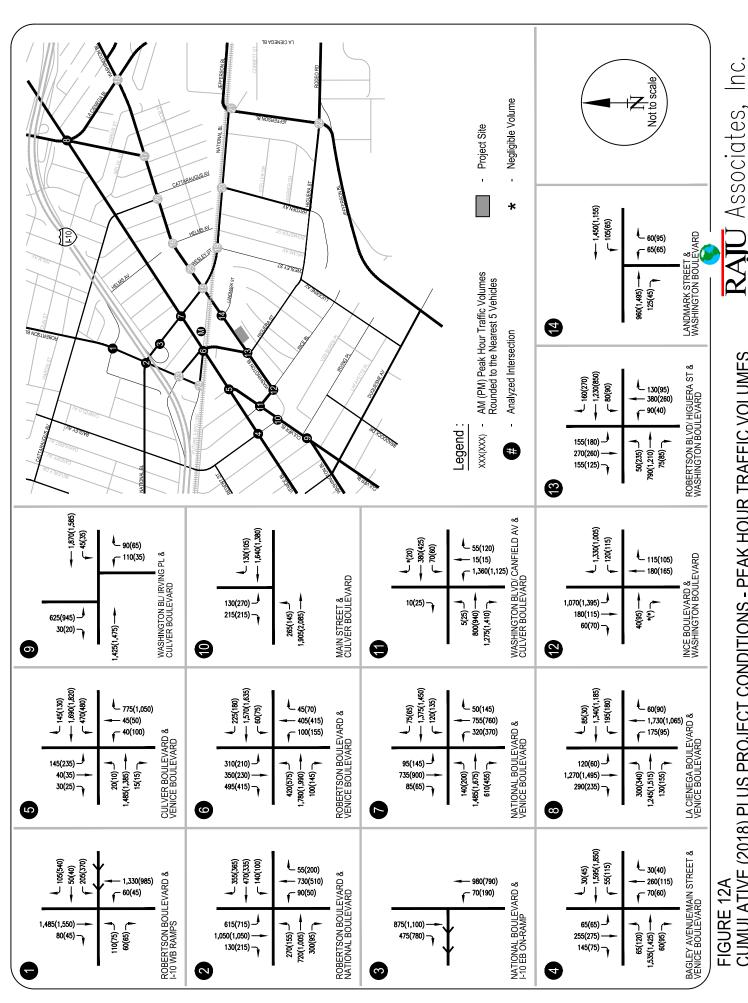
RELATED PROJECTS ONLY - PEAK HOUR TRAFFIC VOLUMES



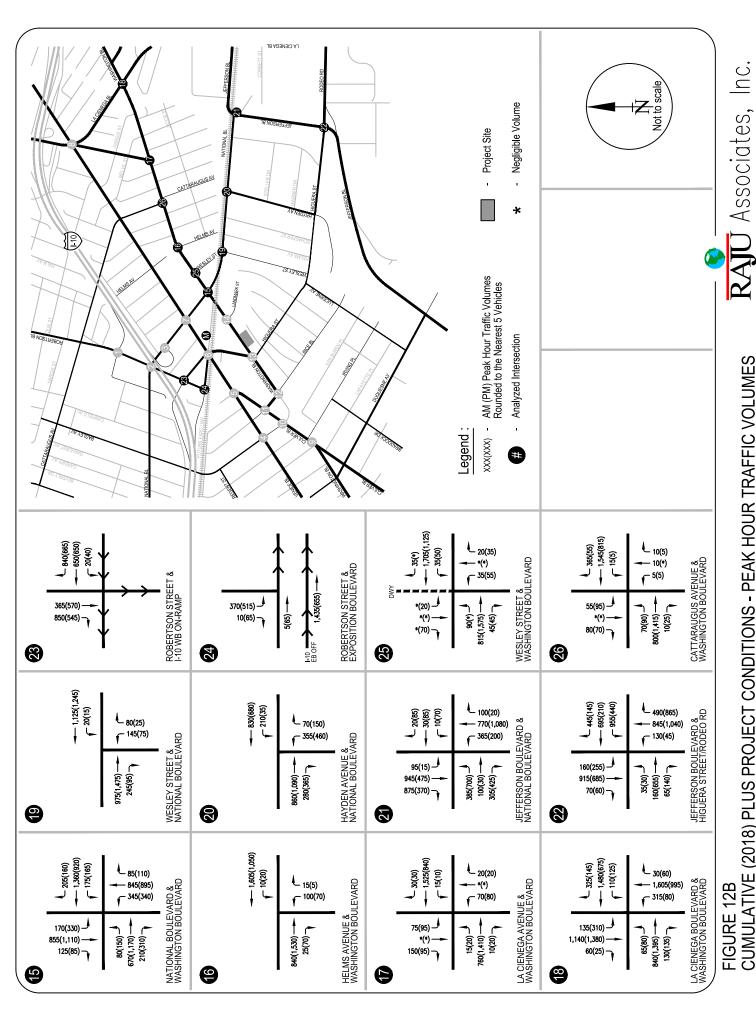
CUMULATIVE (2018) BASE CONDITIONS - PEAK HOUR TRAFFIC VOLUMES



CUMULATIVE (2018) BASE CONDITIONS - PEAK HOUR TRAFFIC VOLUMES



CUMULATIVE (2018) PLUS PROJECT CONDITIONS - PEAK HOUR TRAFFIC VOLUMES **FIGURE 12A**



CUMULATIVE (2018) PLUS PROJECT CONDITIONS - PEAK HOUR TRAFFIC VOLUMES

V. TRAFFIC CONDITIONS & IMPACT ANALYSIS

The Existing (2016) and Future Year (2018) Cumulative conditions without and with the Project were analyzed utilizing the methodologies and assumptions per the City of Culver City traffic study guidelines. The results were then used to assess the potential impact of the proposed project on the local street system.

The traffic impact analysis compares the volume to capacity (V/C) ratios at each study location under the cumulative base and cumulative plus project conditions to determine the incremental difference in V/C ratios caused by the proposed project. This provides the information needed to assess the potential impact of the project using significance criteria established by the Cities of Culver City and Los Angeles.

SIGNIFICANT TRAFFIC IMPACT CRITERIA

City of Culver City Significant Impact Criteria

For intersections under the City of Culver City jurisdiction, the City of Culver City has established threshold criteria¹ for determining the significance of impacts of a project at a specific location. According to the criteria provided by the City of Culver City, a project impact is considered significant if the following conditions are met:

Interse	ction Condition	Project-Related Increase
With P	roject Traffic	in V/C Ratio
LOS	V/C Ratio	
С	0.701 - 0.800	equal to or greater than 0.050
D	0.801 - 0.900	equal to or greater than 0.040
E, F	> 0.900	equal to or greater than 0.020

-

¹ Traffic Study Criteria for the Review of Proposed Development Projects within the City of Culver City, July 2012, City of Culver City Public Works Department/Engineering Division & Community Development Department/Planning Division.

Using these criteria, for example, a project would not have a significant impact at an intersection if it is operating at LOS D after the addition of project traffic and the incremental change in the V/C ratio is less than 0.040. However, if the intersection is operating at LOS F after the addition of project traffic and the incremental change in the V/C ratio is 0.020 or greater, the project would be considered to have a significant impact.

City of Los Angeles Significant Impact Criteria

Intersections under the jurisdiction of the City of Los Angeles are evaluated using threshold criteria² established by the City of Los Angeles to determine if a project has a significant traffic impact. According to the criteria provided by the City of Los Angeles, a project impact is considered significant if the following conditions are met:

	ction Condition Project Traffic	Project-Related Increase in V/C Ratio
LOS	V/C Ratio	
C	$\overline{0.701 - 0.800}$	equal to or greater than 0.040
D	0.801 - 0.900	equal to or greater than 0.020
E, F	> 0.900	equal to or greater than 0.010

EXISTING (2016) PLUS PROJECT TRAFFIC CONDITIONS

The Existing (2016) plus Project peak hour traffic volumes were analyzed at each of the study intersections to determine the V/C ratio and corresponding level of service. Table 7 presents the results of the Existing (2016) plus Project traffic analysis. As illustrated in the table, 23 of the 26 study intersections are currently operating at LOS D or better during both the morning and evening peak hours. The remaining locations are operating at LOS E or F and includes:

- La Cienega Boulevard/Washington Boulevard: AM Peak Hour LOS E
- Robertson Boulevard/I-10 Westbound On-Ramp: AM Peak Hour LOS F
 PM Peak Hour LOS E
- Wesley Street/Washington Boulevard: PM Peak Hour LOS F
- Cattaraugus Avenue/Washington Boulevard: AM Peak Hour LOS F

PM Peak Hour - LOS E

Capacity calculation worksheets for Existing (2016) plus Project conditions are attached in Appendix D of the report.

² Transportation Impact Study Guidelines, December 2016, City of Los Angeles Department of Transportation.

TABLE 7 SUMMARY OF INTERSECTION LEVEL OF SERVICE ANALYSIS

			Peak	Existing (2016) Conditions	016) ₁ S	Existing (2016) Plus Project Conditions	116) Plus nditions	Project Increase	Significant Project	Cumulative (2018) Base Conditions	(2018) ditions	Cumulative (2018) Plus Project Conditions	2018) Plus nditions	Project Increase	Significant Project
Š.	Intersection	Jurisdiction	Hour	V/C or Delay	SOT	V/C or Delay LOS	SOT	in V/C		V/C or Delay	COS	V/C or Delay	SOT	in V/C	Impact
-	Robertson Boulevard & I-10 WB Off-Ramp/Kincardine Avenue	Los Angeles	AM PM	0.588	∢ □	0.593	∢ □	0.005	22	0.708	O 0	0.712	00	0.004	22
2.	Robertson Boulevard & National Boulevard	Los Angeles	AM PM	0.892	۵ ۵	0.896	٥٥	0.004	22	0.968 0.915	шш	0.971	шш	0.003	9 9 2 2
6.	National Boulevard & I-10 Eastbound On-Ramp	Los Angeles	AM PM	0.223	۷ ۷	0.224	∢ ∢	0.001	22	0.262 0.543	4 4	0.263 0.546	∢ ∢	0.001	2 2 2
4.	Bagley Avenue & Venice Boulevard	Los Angeles	AM PM	0.672 0.710	m O	0.672	ш О	0.000	22	0.722 0.781	υυ	0.723	υo	0.001	2 2 2
5.	Culver Boulevard & Venice Boulevard	Los Angeles	AM PM	0.565	ВЪ	0.568	e B	0.003	0 0 2 Z	0.645 0.762	шU	0.648	ш О	0.003	2 2 2
9.	Robertson Boulevard & Venice Boulevard	Los Angeles	AM PM	0.728	υυ	0.729	υυ	0.001	0 0 2 Z	0.872 0.861	۵۵	0.873	۵۵	0.001	2 2 2
7.	National Boulevard & Venice Boulevard	Los Angeles	AM PM	0.707	υo	0.716	υυ	0.009	0 0 2 0	0.866	Он	0.875	ОH	0.009	22
ω̈	La Cienega Boulevard & Venice Boulevard [1]	Los Angeles	AM PM	0.813	٥٥	0.814	٥٥	0.001	0 0 2 2	0.864	۵ ۵	0.867	۵۵	0.003	9 g
6	Washington Boulevard/Irving Place & Culver Boulevard	Culver City	AM PM	0.656	ВВ	0.657	ш ш	0.001	0 N	0.716	υυ	0.716	00	0.000	22
10.	Main Street & Culver Boulevard	Culver City	A M	0.684	B B	0.684	ш ш	0.000	0 0 Z Z	0.786 0.716	υυ	0.787	00	0.001	0 0 2 2
7.	Washington Boulevard/Canfield Avenue & Culver Boulevard	Culver City	AM PM	0.697	а а	0.698	B B	0.001	0 N	0.801 0.755	٥٥	0.802	٥٥	0.001	22
12.	Ince Boulevard & Washington Boulevard	Culver City	AM PM	0.858	۵ ۵	0.862	۵۵	0.004	0 N	1.014	шш	1.017	шш	0.003	22
13.	Robertson Boulevard/Higuera Street & Washington Boulevard	Culver City	AM PM	0.710	OB	0.725 0.658	Om	0.015	0 N	0.816 0.785	٥٥	0.831	۵۵	0.015	22
4.	Landmark Street & Washington Boulevard	Culver City	AM PM	0.442	۷ ۷	0.458	4 4	0.016	0 N	0.507 0.574	4 4	0.522 0.592	∢ ∢	0.015	22
15.	National Boulevard & Washington Boulevard	Culver City	A M	0.670	B O	0.689	в O	0.019	0 V	0.982	П	0.833	ОШ	0.016	22
16.	Helms Avenue & Washington Boulevard	Culver City	AM PM	0.540	۷ ۷	0.544	∢ ∢	0.004	0 N	0.600	4 4	0.605	B 4	0.005	22
17.	La Cienega Avenue/McManus Avenue & Washington Boulevard	Culver City	AM M	0.573	4 4	0.578 0.526	∢ ∢	0.005	N O N	0.628 0.585	B A	0.633	В В	0.005	8 8 8

TABLE 7 (Continued)
SUMMARY OF INTERSECTION LEVEL OF SERVICE ANALYSIS

			Peak	Existing (2016)	016) ns	Existing (2016) Plus Project Conditions	16) Plus	Project Increase	Significant Project	Cumulative (2018)	(2018) itions	Cumulative (2018) Plus Project Conditions	2018) Plus	Project Increase	Significant Project
No.	Intersection	Jurisdiction	1 1	V/C or Delay	SOT	V/C or Delay LOS	SOT	in V/C	Impact	V/C or Delay	FOS	V/C or Delay LOS	SOT	in V/C	Impact
18.	La Cienega Boulevard & Washington Boulevard	Culver City	A M	0.898	۵۵	0.901	шО	0.003	9 9 2 8	0.975	шш	0.979 0.957	шш	0.004	0 0 2 Z
19.	Wesley Street & National Boulevard	Culver City	A M	0.429	4 4	0.434	4 4	0.005	22	0.520	44	0.525	∢ ∢	0.005	8 g
20.	Hayden Avenue & National Boulevard	Culver City	AM M	0.461	4 4	0.464	44	0.003	22	0.576 0.596	44	0.578	∀ Ø	0.002	8 g
21.	Jefferson Boulevard & National Boulevard	Los Angeles	A M	0.875 0.514	DΑ	0.876	0 4	0.001	22	1.060	шΟ	1.061 0.738	шΟ	0.001	8 g
22.	Jefferson Boulevard & Higuera Street/Rodeo Road	Los Angeles	AM PM	0.757 0.727	υυ	0.760	υυ	0.003	22	0.824	۵۵	0.826 0.845	۵۵	0.002	8 g
23.	Robertson Boulevard & I-10 Westbound On-Ramp [2]	Los Angeles	A M	55.2 s 41.8 s	шШ	55.2 s 41.9 s	ш	0.002	22	54.4 s 44.7 s	шШ	54.4 s 44.8 s	шШ	0.002	8 8 8
			A M	0.601	4 4	0.603	<u>4</u> 4	1 1		0.709	<u>4</u> 4	0.711	<u>4</u> 4		
24.	Robertson Boulevard & Exposition/I-10 Westbound On-Ramp [2]	Los Angeles	A M	10.4 s 14.9 s	а а	10.4 s 14.9 s	ш ш	0.000	22	13.3 s 20.2 s	ш О	13.3 s 20.2 s	ωО	0.000	0 0 2 2
			A M	0.209	<u>4</u> 4	0.209	<u> </u>	1 1		0.313	<u>4</u> 4	0.313 0.487	<u>4</u> 4		
25.	Wesley Street & Washington Boulevard [3] [5]	Culver City	A M	22.3 s 49.7 s	ОШ	22.5 s 51.4 s	ΟL	0.006	22						
			AM PM	0.754	<u>4</u> 4	0.760	<u>4</u> 4	1 1	1 1	0.658	ш ш	0.663	ωω	0.005	8 g
26.	Cattaraugus Avenue & Washington Boulevard [3]	Culver City	A M	*** 41.9 s	шШ	*** 43.4 s	ш	0.007	22	* * * * *	шш	* * *	шш	0.007	0 N
			AM	0.961 0.763	[4]	0.968	[4]	1 1	1 1	1.072 0.878	[4]	1.079 0.885	<u>4</u> 4	1 1	1 1

V/C - Volume to Capacity Ratio, LOS - Level of Service

Los Angeles County Congestion Management Program monitoring location.
 All-way stop-controlled intersection. LOS based on average vehicular delay in seconds (s).
 Stop-controlled on minor approach(es). LOS based on worst case approach delay in seconds (s).
 ViC ratio was calculated, based on signalized LOS methodology, to determine project impacts.
 The intersection will be signalized in the future.
 The intersection will be signalized in the future.

CUMULATIVE (2018) BASE TRAFFIC CONDITIONS

The Cumulative (2018) Base without proposed project peak hour traffic volumes were analyzed at each of the study intersections to determine the V/C ratio and corresponding level of service. Table 7 presents the results of the Year 2018 Cumulative Base (without project) traffic analysis. As indicated in the table, 20 of the 26 analyzed intersections are projected to operate at LOS D or better during the morning peak hour. During the evening peak hour, 19 of the 26 analyzed intersections are projected to operate at LOS D or better. Eight of the 26 intersections are projected to be operating at LOS E or F during the morning and/or evening peak hours and include the following:

- Robertson Boulevard/National Boulevard: AM and PM Peak Hour LOS E
- National Boulevard/Venice Boulevard: PM Peak Hour LOS F
- Ince Boulevard/Washington Boulevard: AM and PM Peak Hour LOS F
- National Boulevard/Washington Boulevard: PM Peak Hour LOS E
- La Cienega Boulevard/Washington Boulevard: AM and PM Peak Hour LOS E
- Jefferson Boulevard/National Boulevard: AM Peak Hour LOS F
- Robertson Boulevard/I-10 Westbound On-Ramp: AM Peak Hour LOS F

PM Peak Hour – LOS E

Cattaraugus Avenue/Washington Boulevard: AM and PM Peak Hour – LOS F

A traffic signal at the Wesley Street and Washington Boulevard intersection will be installed as part of the 8770 Washington project. Capacity calculation worksheets for Cumulative (2018) Base conditions are attached in Appendix D of the report.

CUMULATIVE (2018) PLUS PROJECT TRAFFIC CONDITIONS

The Cumulative (2018) Plus Project peak hour traffic volumes were analyzed to determine the V/C ratio and corresponding level of service at each of the analyzed intersections. The results of this analysis are also summarized on Table 7. As in indicated in Table 7, both the morning and evening peak hour operating conditions would be similar to those projected for the Cumulative Base conditions. Twenty of the 26 analyzed intersections are projected to operate at LOS D or better during the morning peak hour. During the evening peak hour, 19 of the 26 analyzed intersections are projected to operate at LOS D or better.

Eight of the 26 intersections are projected to be operating at LOS E or F during the morning and/or evening peak hours and include the following:

- Robertson Boulevard/National Boulevard: AM and PM Peak Hour LOS E
- National Boulevard/Venice Boulevard: PM Peak Hour LOS F
- Ince Boulevard/Washington Boulevard: AM and PM Peak Hour LOS F
- National Boulevard/Washington Boulevard: PM Peak Hour LOS E
- La Cienega Boulevard/Washington Boulevard: AM and PM Peak Hour LOS E
- Jefferson Boulevard/National Boulevard: AM Peak Hour LOS F
- Robertson Boulevard/I-10 Westbound On-Ramp: AM Peak Hour LOS F
 PM Peak Hour LOS E
- Cattaraugus Avenue/Washington Boulevard: AM and PM Peak Hour LOS F

Capacity calculation worksheets for Cumulative (2018) plus Project conditions are attached in Appendix D of the report.

PROJECT IMPACTS

Using the specified significant impact criteria, the traffic impacts at the analysis locations were determined. Table 7 identifies the individual impacts during both AM and PM peak hours at each of the analysis locations. It can be observed that the Proposed Project does not cause significant impacts at any of the analyzed intersections under both existing and future conditions. Therefore, no project-specific mitigation measures would be required.

VI. STREET SEGMENT AND PARKING/ACCESS ANALYSIS

This chapter provides an analysis of roadway segments in the vicinity of the Project. This analysis is targeted towards assessment of potential neighborhood traffic intrusion impacts as a result of the Proposed Project. Additionally, parking evaluation on site and other access/circulation issues are addressed in this chapter. The parking evaluation consists of examining the proposed parking supply for the Project in relation to the parking requirements for the various uses proposed by the Project. The access and egress evaluation consists of a review of vehicular access and egress driveways to ascertain that adequate provisions are provided by the Project.

RESIDENTIAL STREET SEGMENT TRAFFIC IMPACT ANALYSIS

Working closely with the City of Culver City staff, six roadway segment locations were identified for analysis and assessment of conditions with the Project. These street segments include:

- Higuera Street between Washington Boulevard and Lucerne Avenue
- Higuera Street between Wesley Street and Hayden Avenue
- Wesley Street between National Boulevard and Higuera Street
- Helms Avenue Street between National Boulevard and Higuera Street
- Schaefer Street between National Boulevard and Higuera Street
- Lucerne Avenue between Ince Boulevard and Higuera Street

Existing Street Segment Traffic Volumes

Daily traffic counts were conducted in October 2015 using machine counters. These traffic counts were factored upward 1% per year to reflect existing 2016 conditions. The segment count data for the analyzed segments are included in Appendix C.

Existing daily traffic volumes are summarized in Table 8. As indicated in the table, the existing daily traffic volumes on the analyzed street segments are as follows:

- 1. Higuera Street between Washington Boulevard and Lucerne Avenue 8,157 ADT
- 2. Higuera Street between Wesley Street and Hayden Avenue 7,642 ADT
- 3. Wesley Street between National Boulevard and Higuera Street 951 ADT
- 4. Helms Avenue Street between National Boulevard and Higuera Street 754 ADT
- 5. Schaefer Street between National Boulevard and Higuera Street 726 ADT
- 6. Lucerne Avenue between Ince Boulevard and Higuera Street 5,335 ADT

<u>Cumulative (2018) Base - Street Segment Traffic Volumes</u>

Future daily traffic volumes were projected for the residential streets in a manner similar to that used for the intersections described earlier. Firstly, with the assumed completion date of 2018, the existing 2016 traffic volumes were adjusted upward by a factor of 2% (1% per year compounded annually) to reflect this area-wide regional growth. Secondly, from traffic generated by specific cumulative projects located within, or in the vicinity of, the study area were added to the existing plus ambient growth traffic to obtain the Cumulative (2018) Base traffic volumes. The resulting Cumulative (2018) Base street segment daily and peak hour traffic volumes are summarized in Table 8.

Cumulative (2018) plus Project - Street Segment Traffic Volumes

Based on the distribution assumptions (included in Figure 5) and the daily trip generation estimates (approximately 1,146 daily trips) for the Proposed Project, daily traffic estimates of project-only trips were developed. It was determined that the Project would add 23 daily trips to Higuera Street between Washington Boulevard and Lucerne Avenue, and Lucerne Avenue between Ince Boulevard and Higuera Street. The Cumulative (2018) plus Project daily traffic volumes resulting from the addition of trips generated by the Proposed Project are shown in Table 8.

TABLE 8
RESIDENTIAL STREET TRAFFIC ANALYSIS

Street Segment Period Period				•	-	
	Existing (2016) Conditions	Cumulative (2018) Base Conditions	Project Traffic	Cumulative (2018) Plus Project	Project % Increase	Significant Impact
Higuera Street ADT	8,157	9,203	23	9,226	0.2%	No
between Washington Boulevard and Lucerne Avenue	797	871	7	873	0.2%	8
MA	704	783	7	785	0.3%	N _o
Higuera Street ADT	7,642	8,599	0	8,599	%0.0	N _O
esley Avenue and Hayden Avenue	9//	847	0	847	%0:0	8
MA	761	834	0	834	%0:0	N _o
Wesley Street ADT	951	966	0	966	%0.0	No
between National Boulevard and Higuera Street	85	88	0	88	%0.0	8
MA	131	136	0	136	%0:0	N _o
Helms Avenue ADT	754	769	0	692	%0.0	N _O
between National Boulevard and Higuera Street	91	93	0	93	%0.0	8 8
MA	74	75	0	75	%0:0	8 N
Schaefer Street ADT	726	741	0	741	%0.0	No
between National Boulevard and Higuera Street	92	94	0	94	%0.0	<u>8</u>
MA	44	45	0	45	%0:0	8
Lucerne Avenue Avenue	5,335	5,547	23	5,570	0.4%	S N
between Ince Boulevard and Higuera Street	603	619	7	621	0.3%	8
Md	539	559	7	561	0.4%	S N

Street Segment Significant Impact Criteria

As outlined in the City of Culver City Traffic Study Criteria, the following specific threshold criteria for project impacts to any street segment detailed below were used in this study:

Projected Avenue Daily Traffic (ADT) with Project	Project-Related Increase in Average Daily (ADT) Volume
999 Less	120 or more
1,000 to 1,999	12% or more of final ADT
2,000 to 2,999	10% or more of final ADT
3,000 or more	8% or more of final ADT

Assessment of Significant Impacts

As shown in Table 8, the Proposed Project would increase the traffic on Higuera Street roadway segment between Washington Boulevard and Lucerne Avenue by 0.2% on a daily basis and by 0.2% and 0.3% during the morning and evening peak hours, respectively. On Lucerne Avenue between Ince Boulevard and Higuera Street, the Proposed Project would increase traffic by 0.4% on a daily basis and by 0.3% during the morning peak hour and 0.4% during the evening peak hour. On the other four analyzed segments, the proposed project is not expected to increase traffic on those segments.

The potential impacts of the Proposed Project traffic on the adjacent neighborhood residential streets were assessed using the City of Culver City criteria specified earlier in the chapter. The results of the analysis, which are summarized in Table 8, indicate that the Proposed Project would not have a significant impact on the residential streets in the local neighborhood.

PARKING EVALUATION

The Proposed Project consists 59,325 square feet of office use, 2,878 square feet of retail use, and 3,184 square feet of restaurant use. The Project would provide 212 parking spaces. The ground floor would contain four loading spaces and one ADA van accessible space, and the subterranean parking levels would contain 207 spaces. The Project site plan is shown in Figure 2.

The following are the parking requirements contained within Section 17.320.020 Number of Parking Spaces Required established by the Culver City Municipal Zoning Code:

- Offices, Administrative, Corporate, Professional, Creative 1 space per 350 G.S.F.
- Retail and personal service uses, general 1 space per 350 G.S.F.
- Restaurant, general (table service) greater than 1,500 G.S.F. 1 space per 100 G.S.F.

Based on these requirements, the required parking for this project would be 211 spaces as shown on the following calculations:

Office: 59,325 G.S.F. x 1 space/350 G.S.F. = 170 spaces

Retail: 2,878 G.S.F x 1 space/350 G.S.F = 9 spaces

Restaurant: 3,184 G.S.F x 1 space/100 G.S.F = 32 spaces

The Project would provide a total 212 parking spaces. Therefore, there would be adequate parking for the Proposed Project.

ACCESS AND CIRCULATION

The proposed project driveway is located along Washington Boulevard along the western boundary of the project site. The proposed project driveway would provide access to the site and the subterranean parking facility. Access to the subterranean parking facility would be via four parking elevators. The existing three driveways along Washington Boulevard to the site would be removed.

In the proposed subterranean parking facility, the four parking elevators would transport vehicles to any of the three levels of parking. This automated parking system operates with the driver driving the vehicle onto the vehicle elevator. The elevator system would automatically move the vehicles by lift which then transfers it to a waiting cart on one of the multi- levels. The carts then travel horizontally and place the vehicle in its appropriate parking space. Upon retrieval of the vehicle, the elevator system will lift the car from its parking space and deliver the car to the exit area. The vehicle will be delivered in the exit area so that the front of the vehicle is oriented towards the exit of the parking elevator.

A preliminary Parking Operations Plan for the automated parking facility proposed for the Project on-site, has been prepared. Per the parking facility's automated system specifications, the retrieval rate at the proposed facility would range between 65 seconds per vehicle to 150 seconds per vehicle. The retrieval rate is the speed of the system and does not include the time associated with loading, unloading, etc. that would comprise of the overall processing rate.

The processing rate is dependent primarily upon the vertical and horizontal distance a vehicle has to be transported to and from its parking space, whether the space is a tandem space or not, etc. The (non-tandem) spaces closest to the elevator shaft take the least amount of time to process while those spaces farthest from the elevator shaft take the most amount of time to process. This fact is demonstrated in Figure 13 (also provided in the Parking Operations Plan). Based on the exhibits in the Parking Operations Plan, a processing rate of 90 seconds per vehicle is available in the automated parking structure for approximately 50 spaces per level (total of 150 spaces).

Queueing Analysis

A queueing analysis of trips inbound to the Project Site during the morning peak hour when maximum number of inbound vehicular traffic is anticipated, was conducted to assess the potential of vehicles queueing in the driveway aisle within the Project Site beyond the access driveway and spilling over on to the external street system (Washington Boulevard).

This gueuing analysis is based on a number of factors including but not limited to the following:

- Arrival Volumes Magnitude of arriving vehicles and peaking characteristics of the morning peak hour inbound traffic when maximum number of these vehicles are anticipated to arrive on site
- Processing rate of these vehicles on site
- Length of available storage of vehicles on site, and
- Available temporary parking spaces for loading/unloading and temporary storage of vehicles

Details of the associated calculations and analysis are enclosed in Appendix E of this report.

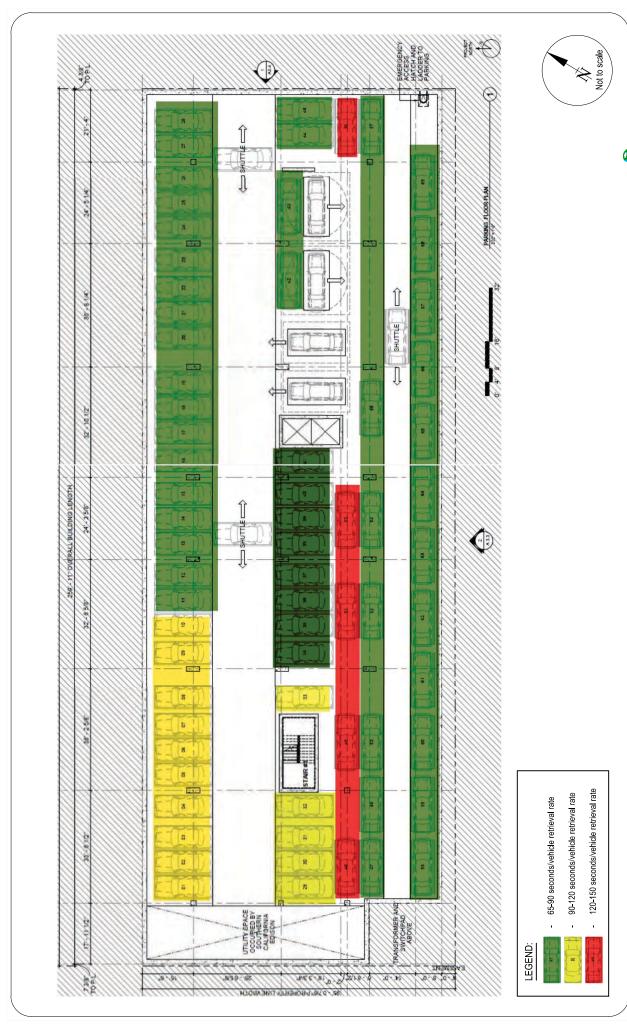


FIGURE 13 DISTRIBUTION OF PARKING SPACES BASED ON SERVICE RATE

RAJU Associates, Inc.

Based on the queueing analysis, it can be observed that during the peak times of the morning peak hour, a maximum total of 42 vehicles would arrive within a peak 15-minute period. Based on a processing rate of the system (including all-day valet services) of 90 seconds per vehicle, a total of 40 vehicles within the same time period can be processed by the system with all four operating vehicular elevators. A maximum queue of 2 vehicles would remain on site. The maximum available storage on-site, based on the Site Plan, is 10 vehicles in the queue plus four (4) short-term loading spaces and one (1) ADA parking space. Therefore, there would not be any queueing vehicles that would extend beyond the site on to the external roadway system (Washington Boulevard) assuming the maximum peaking characteristics of the arriving vehicles in the morning peak hour. Consequently, the traffic flow along Washington Boulevard would not be affected by inbound vehicles extending out of the Project driveway.

Per City of Culver City's request, a queueing analysis with three of the four parking elevators being available during the morning peak conditions was conducted. With the estimated processed rate of the system (with 3 of the 4 elevators available) with all day valet services at 90 seconds per vehicle, a total of 30 vehicles (3600 / 4 (in 15-minutes) / 90 seconds per vehicle * 3 elevators) can be processed by the system within the same peak 15-minute interval. Using a maximum arrival of a total of 42 vehicles within the peak 15-minute period, a maximum queue of 12 vehicles is anticipated. Again, the maximum available storage on-site, based on the Site Plan, is 10 vehicles in the storage lane on site plus four (4) short-term loading spaces and one (1) ADA parking space for a total of 14 to 15 vehicles that can be stored on site. Therefore, there would still not be any queueing vehicles that would extend beyond the site on to the external roadway system (Washington Boulevard) assuming the maximum peaking characteristics of the arriving vehicles in the morning peak hour and 3 of the 4 parking elevators available during that same time period. Consequently, the traffic flow along Washington Boulevard would not be affected by inbound vehicles extending out of the Project driveway even with 3 of the 4 parking elevators available during the peak time period in the AM peak hour.

VII. REGIONAL/CMP ANALYSIS

This section presents the Congestion Management Program (CMP) transportation impact analysis. This analysis was conducted in accordance with the procedures outlined in the *2010 Congestion Management Program for Los Angeles County* (Los Angeles County Metropolitan Transportation Authority, 2010). The CMP requires that when a traffic impact report is prepared for a project, traffic impact analyses be conducted for select regional facilities based on the quantity of project traffic expected to use these facilities.

CMP TRAFFIC IMPACT ANALYSIS

The CMP guidelines for determining the study area for analysis of CMP arterial monitoring intersections and for freeway monitoring locations are as follows:

- All CMP arterial monitoring intersections where the proposed project will add 50 or more trips during either the AM or PM weekday peak hours of adjacent street traffic.
- All CMP mainline freeway monitoring locations where the proposed project will add 150 or more trips, in either direction, during either the AM or PM weekday peak hours.

The CMP arterial monitoring intersections within a three-mile from the Project site includes the following:

- La Cienega Boulevard/Venice Boulevard (Study Int. 8) City of Los Angeles jurisdiction
- La Cienega Boulevard/Jefferson Boulevard City of Los Angeles jurisdiction
- Centinela Avenue/Venice Boulevard City of Los Angeles jurisdiction
- La Cienega Boulevard/Stocker Street County of Los Angeles jurisdiction
- La Cienega Boulevard/Wilshire Boulevard City of Beverly Hills jurisdiction
- Santa Monica Boulevard/Wilshire Boulevard City of Beverley Hills jurisdiction
- Overland Avenue/Venice Boulevard City of Culver City jurisdiction

Based on the incremental Project trip generation estimates presented in Chapter III, the Proposed Project is not expected to add 50 or more new trips per hour to any of these locations. Therefore, no further analysis of these CMP monitoring intersections would be required. However, one of the CMP arterial monitoring intersections listed above, La Cienega Boulevard/Venice Boulevard, has

been included in the traffic analysis and it was determined that the Project would not have a significant intersection traffic impact at this location.

The CMP mainline freeway monitoring locations within a three-mile radius from the Project site includes the following:

- Santa Monica (I-10) Freeway east of Overland Avenue
- Santa Monica (I-10) Freeway east of La Brea Avenue
- San Diego Freeway (I-405) north of Venice Boulevard

Based on the incremental Project trip generation estimates, the Proposed Project will not add 150 or more new trips per hour to these locations in either direction. Therefore, no further analysis of CMP freeway monitoring stations is required.

VIII. CALTRANS FREEWAY IMPACT SCREENING ANALYSIS

This freeway screening procedure has been prepared in accordance with the screening criteria described in the first amendment (dated on December 15, 2015) to Section 3 of the "Agreement Between City of Los Angeles and Caltrans District 7 On Freeway Impact Analysis Procedures", dated October 2013. The amended Section 3.1 of the Agreement specifies the following:

- "3.1 City will require Project applicants to work with Caltrans and prepare a Freeway Impact Analysis, utilizing Caltrans' "Guide for the Preparation of Traffic Impact Studies" ("TIS Guide"), for land use proposals that meet any of the following criteria:
- The project's peak hour trips would result in a 1-percent or more increase to the freeway mainline capacity of a freeway segment operating at level-of-service (LOS) E or F (based on an assumed capacity of 2,000 vehicles per hour per lane); or
- The project's peak hour trips would result in a 2-percent or more increase to the freeway mainline capacity of a freeway segment operating at LOS D (based on an assumed capacity of 2,000 vehicles per hour per lane); or
- The project's peak hour trips would result in a 1-percent or more increase to the capacity
 of a freeway off-ramp operating at LOS E or F (based on an assumed ramp capacity of
 850 vehicles per hour per lane); or
- The project's peak hour trips would result in a 2-percent or more increase to the capacity
 of a freeway off-ramp operating at LOS D (based on an assumed ramp capacity of 850
 vehicles per hour per lane)."

The purpose of this analysis is to apply the above screening criteria to determine whether a Freeway Impact Analysis would be required for the Proposed Project. The methodologies used to conduct the screening analysis for the project, and the results of the screening, are described below.

INITIAL STEPS

- Project trip generation estimates were prepared in accordance with the latest version of LADOT's Traffic Study Policies and Procedures. The project trip generation estimates as accepted by LADOT is shown in Table 5.
- The resulting overall trip distribution for the freeway mainline, on-ramps and off-ramps is shown in Figure 5. As indicated in Figure 5, it was determined that 10% of project trips may utilize the I-10 freeway to/from the west, 5% may utilize the I-10 Freeway to/from the east.
- Based on this distribution, two freeway mainline segments were determined to be utilized by the Project and were selected for screening. They include:
 - I-10 Freeway east of National Boulevard
 - o I-10 Freeway west Robertson Boulevard
- Also based on the trip distribution, two freeway off-ramps were selected for screening:
 - o I-10 Westbound Off-Ramp at National Boulevard
 - o I-10 Eastbound Off-Ramp at Robertson Boulevard

FREEWAY MAINLINE SEGMENT SCREENING

- The freeway mainline segment screening analysis is shown in Table 9.
- The number of lanes and capacity for each freeway segment was determined. A capacity of 2,000 vehicles per hour per lane was assumed.
- The worst-case LOS screening threshold was used to determine the trigger (i.e. the number of trips) for each freeway segment for exceeding the threshold:
 - Threshold=≥1% of segment capacity if worst-case LOS is E or F
 - Where the assumed capacity = 2,000 vphpl multiplied by the number of lanes on the freeway mainline. In other words, the threshold is 20 vphpl at LOS E or F, multiplied by the number of lanes on the freeway mainline.
- The project-added trips to each freeway mainline segment were compared to the trigger threshold. As shown in Table 9, the screening analysis determined that the screening threshold criteria would not be triggered at any of the two freeway mainline segments. Furthermore, since the project traffic did not trigger the screening thresholds at the mainline segments most likely to be used by project traffic, there is no need to look at segments farther away. Therefore, a Freeway Impact Analysis is not required.

TABLE 9
CALTRANS FREEWAY IMPACT SCREENING ANALYSIS - FREEWAY MAINLINE

	Peak	Projec	t Trips	,	Mainline		Criteria for nalysis [b]	Freeway Impact Analysis
Location	Hour	WB	EB	WB	EB	WB	EB	Required?
I-10 Freeway,	AM	4	1	8,000	10,000	80	100	NO
east of National Boulevard	PM	2	5	8,000	10,000	80	100	NO
I-10 Freeway,	AM	2	8	8,000	10,000	80	100	NO
west of Robertson Boulevard	PM	9	3	8,000	10,000	80	100	NO

WB = westboud, EB = eastbound

[[]a] The freeway capacity is 2,000 vehicles per hour per lane.

[[]b] A 1% or more increase to the freeway mainline capacity for a freeway segment operating at LOS E or F would require a freeway impact analysis.

FREEWAY RAMP SCREENING

- The freeway ramp screening analysis is shown in Table 10.
- For each ramp, the LOS screening threshold was used to determine the trigger (i.e. the number of trips) for each freeway off-ramp for exceeding the threshold:
 - Threshold=≥2% of assumed ramp capacity if approach LOS is D
 - o Threshold=≥1% of assumed ramp capacity if approach LOS is E or F

Where the assumed ramp capacity = 850 vphpl multiplied by the number of approach lanes on the ramp approach to the intersection. In other words, the threshold is 17 vphpl at LOS D and 8.5 vphpl at LOS E or F, multiplied by the number of lanes on the ramp approach to the intersection.

- The project-added trips to each off-ramp were compared to the appropriate threshold. As shown in Table 10, the screening analysis determined that the screening threshold criteria would not be triggered at any of the two freeway off-ramps. Furthermore, since the project traffic did not trigger the screening thresholds at the ramps most likely to be used by project traffic, there is no need to look at ramps further away. Therefore, a Freeway Ramp Impact Analysis is not required.
- Although no further analyses of freeway ramps are needed, the project study analyzed
 the two ramp intersections, I-10 Westbound Off-Ramp at National Boulevard and I-10
 Eastbound Off-Ramp at Robertson Boulevard, and the project impacts were evaluated at
 these locations as discussed in the main body of the report. None of the analyzed ramp
 intersections would be significantly impacted by the proposed project.

TABLE 10
CALTRANS FREEWAY IMPACT SCREENING ANALYSIS - FREEWAY OFF-RAMP

Location	Peak Hour	Project Trips	Freeway Off- Ramp Capacity [a]	Caltrans 1% Criteria for Impact Analysis [b]	Caltrans 2% Criteria for Impact Analysis [c]	Off-Ramp Impact Analysis Required?
I-10 Freeway Westbound	AM	4	1,700	17	34	NO
Off-Ramp at National Boulevard	PM	2	1,700	17	34	NO
I-10 Freeway Eastbound	AM	8	1,700	17	34	NO
Off-Ramp at Robertson Boulevard	PM	3	1,700	17	34	NO

[[]a] The freeway off-ramp capacity is 850 vehicles per hour per lane.

[[]b] A 1% or more increase to the capacity of a freeway off-ramp operating at LOS E or F would require a freeway impact analysis.

[[]c] A 2% or more increase to the capacity of a freeway off-ramp operating at LOS D would require a freeway impact analysis.

IX. SUMMARY OF CONCLUSIONS

This study was undertaken to assess existing traffic conditions with and without the Proposed Project, estimate future conditions with and without the Proposed Project, analyze potential traffic impacts of the Proposed Project, assess required improvements and identify/recommend project mitigation to alleviate the significant traffic impacts on the transportation system, if needed. Raju Associates, Inc. performed this detailed study and the following summarizes the results of the analysis:

- Twenty-six intersections were analyzed within the study area for this project. These locations are within the study area bounded by Cattaraugus Avenue on the north, Jefferson Boulevard/Rodeo Road on the south, Hughes Avenue/Duquesne Avenue on the west and La Cienega Boulevard on the east. Of the 26 intersections, 14 intersections are located within the City of Culver City and 12 intersections within the City of Los Angeles.
- Currently, 24 of the 26 analyzed intersection locations are operating at levels of service (LOS) D or better during the morning peak hour. During the evening peak hour, 23 of the 26 analyzed intersections are operating at LOS D or better. The remaining intersections are operating at LOS E or F.
- In the Cumulative (Future Year 2018) Base conditions, i.e., future conditions without the implementation of the Proposed Project, 20 of the 26 study intersections are projected to operate at LOS D or better during the morning peak hour. During the evening peak hour, 19 of the 26 analyzed intersections are projected to operate at LOS D or better. The remaining intersections are projected to operate at LOS E or F.
- The Proposed Project consists of 59,325 square feet of office use, 2,878 square feet of retail use, and 3,184 square feet of restaurant use. The existing site contains an auto repair facility auto repair facility with a building size of 9,992 square feet which will be demolished. The Project is estimated to generate a net total of 100 trips during the morning peak hour and 124 trips during the evening peak hour.
- In the Existing (2016) plus Project conditions, both the morning and evening peak hour operating conditions would be similar to those for the Existing conditions. Under this scenario, 23 of the 26 analyzed intersection locations would continue to operate at acceptable levels of service (LOS) D or better during both the morning and evening peak hours. The remaining intersections would be operating at LOS E or F.
- The Existing (2016) plus Project traffic conditions indicate that the Proposed Project would not cause significant traffic impacts at any of the analysis locations during the weekday morning and evening peak hours.

- In the Cumulative (Future Year 2018) plus Project conditions, both the morning and evening peak hour operating conditions would be similar to those projected for the Cumulative Base conditions. Under this scenario, 20 of the 26 study intersections are projected to operate at LOS D or better during the morning peak hour. During the evening peak hour, 19 of the 26 analyzed intersections are projected to operate at LOS D or better. The remaining intersections are projected to operate at LOS E or F.
- The Cumulative (Future Year 2018) plus Project traffic conditions indicate that the Proposed Project would not cause significant traffic impacts at any of the analysis locations during both the weekday morning and evening peak hours.
- The Proposed Project would not have a significant impact on the residential streets in the local neighborhood.
- The Proposed Project would add less than 50 trips to the nearest Congestion Management Program (CMP) arterial monitoring locations and would add less than 150 trips in either direction to the nearest CMP mainline freeway monitoring locations during both the weekday morning and evening peak hours. Per CMP guidelines, no further CMP analysis is required.
- The screening analysis determined that the screening threshold criteria would not be triggered at any of the two freeway mainline segments and two freeway off-ramps. Furthermore, since the project traffic did not trigger the screening thresholds at the mainline segments and off-ramps most likely to be used by project traffic, there is no need to look at segments or ramps farther away. Therefore, a Freeway Impact Analysis and Freeway Ramp Impact Analysis is not required.
- The Proposed Project shall make a contribution of \$100,000 towards transportation improvements including Intelligent Transportation System (ITS) signal system improvements and bicycle and pedestrian system improvements. The contribution will be due at the time of issuance of a Certificate of Occupancy.

Summarizing, the Proposed Project would not cause any significant impacts at any of the analyzed intersections. Therefore, no project-specific mitigation measures would be required.

APPENDIX A

Memorandum of Understanding

DRAFT

Attachment A Memorandum Of Understanding For Traffic Study

Culve Proje	er City requirements a ct Name:	and fees for the prepar 8888 Washington Bo	ration of a traffic study oulevard Project	grees to all of the City of for the following project:
Proje	ct Address:	8888 Washington Bo	oulevard Culver City,	CA
Proje	ct Description:	59,325	GFA Office /	GFA Industria Residential Units GFA Othe
		<u>2,878</u>	GFA Retail /	Residential Units
		3,184 GFA	Restaurant /	GFA Othe
* Gro	ss Floor Area (GFA)	shall be as defined in t	the most recent ITE p	ublication.
Direc [Attac	tional Distribution:	N: <u>20 </u> % directional distribution	S: <u>15%</u> % E: ˌ	e: One (1.0) % Per Yea 35 % W: 30 % ersections and driveways.
Trip (Generation Rate(s):	ITE Latest Edition / 0	Other: Please see Att	achment B.
Lanu	USE.	ITE Codo #	ITE Codo #:	
		ITE Code #:	In / Out	Total In / Total Ou
^ N / T	ring	<u>In / Out</u>	In / Out	Total In / Total Ou
AM T			/	<u>82</u> / <u>18</u>
PM T Use a	rips: additional pages if neo		//	
 1) 2) 3) 	Obtain a list of relate other affected jurisdic Prepare a draft list of Please see Attachm	ctions; f "related projects spec nent C.	ity of Culver City Pla	nning Division and from al
Inters	sections To Be Studie	d: 26 intersections,	please also see Atta	ichment D.
	Intersection:		/ Jurisdiction	
1	Robertson Boulevard	I & I₋10 WR Off₋Ramn	/ City of Los	Angeles/Caltrans
2.	Robertson Boulevard	1 & National Boulevard	/ City of Los	Angeles
3.	National Boulevard 8	l-10 EB On-Ramp	/ City of Los	Angeles/Caltrans
4.	Bagley Avenue & Ve			Angeles/Caltrans
5.	Culver Boulevard & \			Angeles/Caltrans
6.	Robertson Boulevard			Angeles/Caltrans
7.	National Boulevard 8			Angeles/Caltrans
8.		d & Venice Boulevard		Angeles/Caltrans
9.		Washington BI-Irving P		
10.	Main Street & Culver		/ Culver City	
11.		shington Bl & Culver E		
12.	Ince Boulevard & Wa		/ Culver (•
13.		I-Higuera St & Washin		-
14.		Vashington Boulevard	/ <u>Culver (</u>	-
15.		Washington Boulevard		•
16.	Helms Avenue & Wa	-	/ <u>Galver (</u> / <u>Culver (</u>	-
17.		& Washington Bouleva		-

City of Culver City Traffic Study Criteria Page 2

18.	La Cienega Boulevard & Washington Boulevard	/ Culver City
19.	Wesley Street & National Boulevard	/ Culver City
20.	Hayden Avenue & National Boulevard	/ Culver City
21.	Jefferson Boulevard & National Boulevard	/ City of Los Angeles
22.	Jefferson Boulevard & Higuera Street-Rodeo Road	/ City of Los Angeles
23.	Robertson Boulevard & I-10 WB On-Ramp	/ City of Los Angeles/Caltrans
24.	Robertson Boulevard & Exposition Bl./I-10 EB Off-ram	p / City of Los Angeles/Caltrans
25.	Wesley Street & Washington Boulevard	/ Culver City
26.	Cattaraugus Avenue & Washington Boulevard	/ Culver City

Use additional pages if necessary. Additionally, indicate any intersections that are subject to capacity analysis credit for advanced traffic signal control synchronization. Indicate any non-signalized intersections to be studied.

Residential Streets To Be Studied

No.	Street Segment:	/ <u>Jurisdiction:</u>
1.	Higuera Street between Washington Bl and Lucerne Avenue	/ Culver City
2.	Higuera Street between Wesley Street and Hayden Avenue	/ Culver City
3.	Wesley Street between National Boulevard and Higuera St	/ Culver City
4.	Helms Avenue between National Boulevard and Higuera St /	Culver City
5.	Schaefer Street between National Boulevard and Higuera St	/ Culver City
6.	Lucerne Avenue between Ince Boulevard and Higuera St	/ Culver City
Use	additional pages if necessary. Additionally, all intersection ar	nd street segment traffic count

Use additional pages if necessary. Additionally, all intersection and street segment traffic count data shall be submitted both in written format and in an electronic format acceptable to the City.

<u>Indi</u>	cate trip credits to be requested (Amount subject to City approval):	Yes	No
1.	Existing Uses:	Χ	
2.	Pass-By Trips:	X	
3.	Internal Trip Capture:	X	
4.	Transit Oriented Developments (TOD):	X	
5.	Transportation Demand Management (TDM):		Χ

Proposed Traffic Mitigation

Any proposed traffic mitigation measure shall be listed and accompanied by a drawing of the existing and proposed improvements [including city boundary lines and existing / proposed property lines] and plans shall be of a minimum scale of one inch (1") equal to forty feet (40'-0").

Post-Occupancy Traffic Counts

By signing below, the Property Owner / Developer / Applicant hereby agrees to pay for and submit to the City a post-occupancy traffic count analysis of the development to the satisfaction of the City. The analysis shall determine the amount of actual traffic generated by the development compared to the ITE trip generation rates. The analysis shall include traffic counts of all onsite driveways to be taken upon reaching eighty five percent (85.0%) occupancy of the total building gross floor area or within one (1) year of the issuance of the first Temporary Certificate of Occupancy (TCO), as determined by the City. The data shall be used to confirm the findings in the approved traffic study, and shall not result in any additional traffic mitigation measures and/or conditions of approval on the subject project.

City of Culver City Traffic Study Criteria Page 3

<u>Congestion Management Plan (CMP)</u>
This project shall also be subject to all City imposed CMP developer fees if the Planning Commission approval date is on or after the effective date of any City Council imposed CMP developer fees or as may be otherwise imposed by the City.

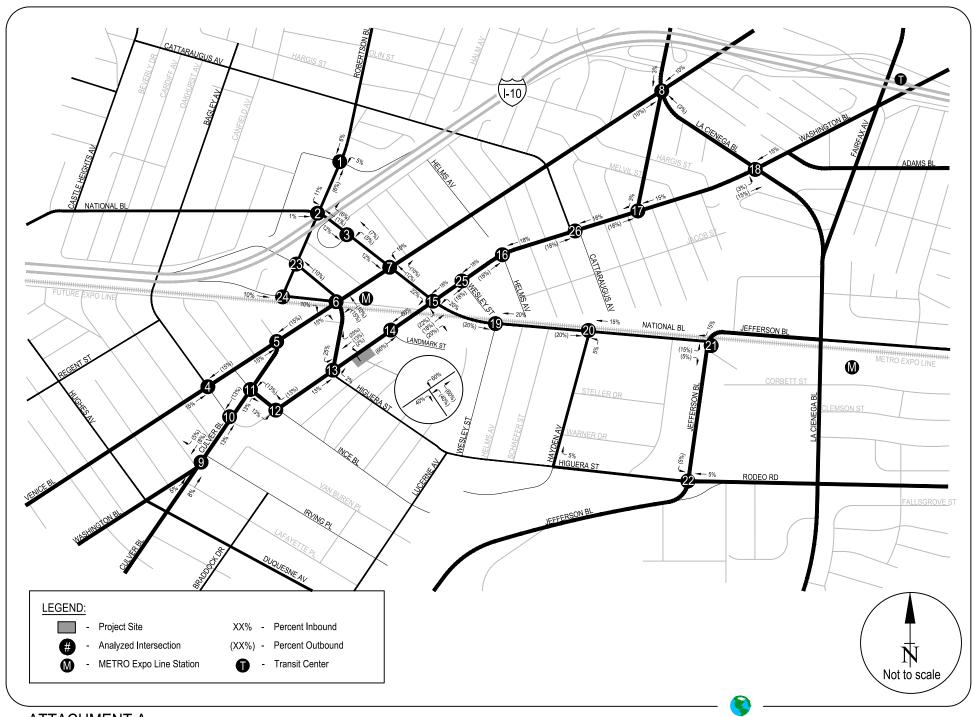
<u>Signatures</u>		
	Property Owner / Applicant:	Developer / Applicant:
Name [Signed]: Name [Printed]: Company: Address: City / State / Zip: Office: Fax: Cell: E-Mail:	Mr. Joseph Miller The Runyon Group 9900 Culver BI, Suite 1A Culver City, CA, 90232 (310) 275-0483 () () joseph@runyongroup.com Traffic Consultant:	
Name: Company: Address: City / State / Zip: Office: Fax: Cell: E-Mail:	Srinath Raju, P.E. Raju Associates, Inc. 505 E. Colorado BI, Suite 202 Pasadena, CA, 91101 (626) 792-2700 (626) 792-2772 (310) 569-7559 srinath.raju@rajuassociates.com	
Los Angeles, the uni	ncorporated areas of Los Angeles ans], then this MOU shall also	affic study are located within the City of County and/or impact any other public be approved by the reviewing staff
	City of Los Angeles:	County of Los Angeles:
Name [Signed]: Name [Printed]: Company: Address: City / State / Zip: Office: Fax: Cell: E-Mail:		

City of Culver City Traffic Study Criteria Page 4

	Other Public A	gency:		Other Public Ag	ency:
Name [Signed]: Name [Printed]: Company: Address: City / State / Zip: Office: Fax: Cell: E-Mail:					
Approved by:					/
Property Owner – App	plicant	Date	Developer	– Applicant	Date
Sinatul			1		
	/ 1/24/2	2017			,
Traffic Consultant		Date			
Eity of Cyliver City) , 2/2	2/20/7 Date			

Note: This MOU shall become valid as of the date of the City's signature and shall expire one (1) year thereafter. If the "administrative draft" of the traffic study has not been filed with the City by the expiration date, this MOU shall expire and a new MOU filing, review and approval process shall be required.

BK-JM/abn



ATTACHMENT A PROJECT TRIP DISTRIBUTION

RAJU Associates, Inc.

ATTACHMENT B ESTIMATED PROJECT TRIP GENERATION

			А	M Peak Ho	our	Р	M Peak Ho	our
	Size	Daily	IN	OUT	TOTAL	IN	OUT	TOTAL
Proposed Project								
Office	59,325 s.f.	883	111	15	126	25	120	145
	ransit Trip Use (25%)	(221)	(28)	(4)	(32)	(6)	(30)	(36)
*Internal Cap	ture (10%) Trip Credit	(66)	(8)	(1)	(9)	(2)	(9)	(11)
Retail	2,878 s.f.	677	11	7	18	27	29	56
Internal Cap	ture (10%) Trip Credit	(68)	(1)	(1)	(2)	(3)	(3)	(6)
**Pass-By	Trip Reduction (25%)	(152)	(3)	(1)	(4)	(6)	(7)	(13)
High-Turnover Restaurant	3.184 s.f.	405	19	15	34	19	12	31
•	ture (10%) Trip Credit	(41)	(2)	(1)	(3)	(2)	(1)	(3)
	Trip Reduction (25%)	(91)	(4)	(4)	(8)	(4)	(3)	(7)
,	, ,		, ,			, ,	, ,	
Existing Uses (to be removed)								
Auto Repair Shop	9,992 s.f.	200	15	7	22	17	19	36
Pass-By	Trip Reduction (10%)	(20)	(2)	0	(2)	(2)	(2)	(4)
Due lead Nat	Trin Ormanation Tatal	4.440	82	18	400	33	91	124
Project Net	Trip Generation Total	1,146	82	18	100	33	91	124
Trip Generation Rates [1]								
Office (ITE Land Use 710) Trips per 1,000 s.f.		[2]	88%	12%	[2]	17%	83%	[2]
Retail/Shopping Center (ITE Land Use 820) Trips per 1,000 s.f.		[3]	62%	38%	[3]	48%	52%	[3]
High-Turnover Restaurant (ITE Land Use	, , , ,	127.15	55%	45%	10.81	60%	40%	9.85
Automobile Care Center (ITE Land Use 9	42) Trips per 1,000 s.f.	20.00 [4]	66%	34%	2.25	48%	52%	[5]

^{*} Internal capture trips determined after reduction of transit trips.

[2] Trip generation for office was calculated using the following equations:

Daily: Ln(T) = 0.76 Ln(X) + 3.68 Where:

AM Peak Hour: Ln(T) = 0.80 Ln(X) + 1.57 Ln = Natural logarithm

PM Peak Hour: T = 1.12 (X) + 78.45 T = Two-way volume of traffic (total trip-ends) <math>X = Area in 1,000 square feet gross floor area

[3] Trip generation for retail/shopping center was calculated using the following equations:

Where:

Daily: Ln(T) = 0.65 Ln(X) + 5.83 Ln = Natural logarithm

AM Peak Hour: Ln(T) = 0.61 Ln(X) + 2.24 T = Two-way volume of traffic (total trip-ends) PM Peak Hour: Ln(T) = 0.67 Ln(X) + 3.31 X = 1,000 square feet gross leasable area

[4] ITE does not provide a daily trip generation rate for this use. Therefore, the daily trip rate for this use from Brief Guide of Vehicular Traffic Generation Rates for the San Diego Region, SANDAG, April 2002 was utilized.

[5] PM trip generation for automobile care center was calculated using the following equation:

Mhara.

PM Peak Hour: T = 2.41 (X) + 11.79 T = Two-way volume of traffic (total trip-ends)

X = 1,000 square feet occupied gross leasable area

^{**} Pass-by trips determined after reduction of internal capture trip credit.

^[1] Trip generation rates from Trip Generation Manual, 9th Edition, ITE 2012, unless otherwise noted.

ATTACHMENT C ESTIMATED WEEKDAY TRIP GENERATION OF RELATED PROJECTS

Map No.	Project Name	Location	Description	Daily	IN A	M Peak Ho	ur TOTAL	PN IN	/I Peak Ho	our TOTAL
	Culver City [1]	Location	Description	Daily	IIN	001	TOTAL	IIN	001	TOTAL
1	Residential Project	3440 Caroline Avenue	Two (2) new detached residential condominium dwelling units (net addition of one unit)	6	0	0	0	1	0	1
2	Mixed-Use Project	9355 Culver Boulevard	Three story mixed use building consisting of a ground level salon, mezzanine, and office totaling 2,947 s.f., and four residential units on the third floor.		4	2	6	3	5	8
3	The Wende Museum	10808 Culver Boulevard	Tenant improvements to convert existing 12,596 s.f. armory building into a museum	57	4	1	5	0	8	8
4	Chapel/Dormitory Project	10775 Deshire Place	4,740 s.f. addition to existing dormitory and replace existing chapel with a 1,660 s.f. chapel.	82	2	4	6	4	3	7
5	Residential Project	4109-4111 Duquesne Avenue	Addition of two (2) residential dwelling units to existing duplex	12	0	1	1	1	0	1
6	Residential Project	4139-4145 Duquesne Avenue	Seven unit condominiums with 15 subterranean parking spaces.	41	1	2	3	3	1	4
7	Residential Project	4058 Madison Avenue	New four unit condominium, 7,422 s.f. total.	41	1	2	3	3	1	4
8	Retail/Restaurant Project	8511 Warner Drive	Five level parking structure with retail/restaurant. 51,520 s.f. of retail/restaurant uses. Parking Structure -307,522 s.f.	3,112	93	70	163	109	103	212
9	Mixed-Use Project [2]	8770 Washington Boulevard	TOD Mixed Use with 31,240 s.f. of retail and restaurant uses and 115 residential units (5 story)	2,914	69	85	154	150	125	275
10	Platform Project [3]	8810-8850 Washington Boulevard & 3920 Landmark Street	New commercial development (38,732 s.f. office, 41,745 s.f. of retail and restaurant)	2,357	71	20	91	100	100	200
11	Mixed-Use Project	8777 Washington Boulevard	Construct 4,500 s.f. of retail and 128,000 s.f. of office use. Demolish existing 12,485 s.f. of retail use and 4,731 s.f. of restaurant use.	30	123	-3	120	-23	92	69
12	Triangle Site - Washington/National TOD [4]	Corner of Washington Boulevard/National Boulevard	Transit oriented development to include 200 d.u, mid- rise apartments, 148-room hotel, 201,000 s.f. office, 24,000 s.f. specialty retail, 10,000 s.f. of high-turnover restaurant & 10,000 s.f. quality restaurant.	4,124	173	83	256	127	174	301
13	The Culver Studios [5]	9336 Washington Boulevard	Net increase of 138,997 s.f. of office and support facilities.	1,564	149	20	169	45	114	159
14	Office & Retail Project	10000 Washington Boulevard	Renovation of existing 9-story office building. Convert ground floor lobby space to office, retail and restaurant space. New construction includes a new stand-alone 3,115 sq. ft. one-story restaurant building and a second floor within the atrium to add 5,500 sq. ft. of office space.	3,612	136	81	217	102	112	214
15	Sony Pictures	10202 Washington Boulevard	New 8-story, 218,450 s.f. office building, a new 4- story, 51,716 s.f. Production Services support building, and expansion of an existing parking structure. Total demolition of 57,642 s.f. Net New square feet is 212.524 s.f.	2,328	308	42	350	54	262	316
16	Sony Pictures	10202 Washington Boulevard	New 22,929 s.f. 4- story office building (net new 9,875 s.f.).	109	13	2	15	3	12	15
17	Union 76	10638 Culver Boulevard	Gas station and convenience store; 2,676 G.S.F.	651	21	20	41	9	45	54
18	Willows School Comprehensive Plan	809 Higuera & 8476 Warner	Phase II & III - increase student enrollment by 100, from 475 to 575	276	50	40	90	3	15	18
19	Culver Center Shopping Center - New restaurant	10799 Washington Blvd	New 2,000 sq. ft. restaurant at existing commercial shopping center	254	12	10	22	12	8	20
20	Parcel B [5]	9300 Culver Blvd	118,000 G.S.F. of office, retail, and restaurant space.	3,702	124	31	155	167	188	355
21	Three unit condominium/ townhome Redevelopment	4241 Duquesne Avenue	New three detached condominium/ townhomes, resulting in two net new residential dwelling units	17	0	1	1	1	1	2
22	Office Building	9919 Jefferson Blvd	New 3-story, 62,558 sq. ft., office and research and development (laboratory) building, as well as a five (5) level parking structure containing 398 parking spaces, and associated site improvements	919	115	16	131	25	124	149
23	Lorcan O'Herlihy Architects	3434 Wesley St	New TOD Mixed Use project with 15 dwelling units, and 14,237sq. ft. of office/gallery on a vacant lot.	278	16	9	25	16	20	36
City of 24	Los Angeles [6] Apartment [7]	3822 S. Dunn Drive	7-story, 86-Unit Apartment building over ground floor	543	8	34	42	33	17	50
25	Wrapper Office Building Project	5790 W. Jefferson Boulevard	Construct new 10-story 150,761 s.f. office building	1,794	234	32	266	42	205	247
26	Jefferson & La Cienega Mixed Use Project [8]	3221 S. La Cienega Boulevard	Converting existing ABC Lot to a Mixed-Use: 1,218- Unit Apartment, 200,000 s.f. Office, 50,000 s.f. Grocery Store, 30,000 s.f. Retail & 20,000 s.f.	10,136	319	419	738	467	382	849
27	Mixed-use Apartment & Retail	3425 Motor Avenue	Restaurant project. 115-unit apartment and 975 s.f. retail. Existing 15 apartment units, 2 single family dwellings and 3,300 s.f. office to be demolished.	999	12	43	55	58	35	93
28	Restaurant & Retail [7]	10612 National Blvd	1,726 s.f. Coffee Shop (Coffee Bean) including 250 s.f. Outdoor Seating. Existing vacant lot.	636	46	38	84	19	12	31
29	Mixed-Use: Apartment & Restaurant [7]	3644 S. Overland Avenue	New Mixed-Use: 92-Unit Apartment & 1,573 sf Restaurant use (110 spaces).	750	17	42	59	38	22	60
30	Venice Fairfax Residential Project	5930 W. Sawyer Street	Construct 60 single-family homes	656	13	39	52	42	24	66
31	Coffee Shop with Drive Through [7]	9829 W. Venice Boulevard	Coffee Bean & Tea Leaf Coffee Shop with Single- Lane Drive Through to replace existing Rally's with Dual-Lane Drive Through.	145	13	12	25	3	2	5
32	Mixed-use Apartment & Retail	9901 Washington Boulevard	131-unit apartment & 12,000 s.f. retail. Existing 16,900 s.f. retail to be removed.	507	8	50	58	42	12	54
33	Mixed-use Apartment, office, retail, and restaurant	10601 Washington Boulevard	126-unit apartment, 23,000 s.f. office, 9,000 s.f. retail, 9,000 s.f. restaurant. Existing 10,000 s.f. office to be removed.	3,595	106	112	218	170	144	314
			RELATED PROJECTS TRIP GENERATION TOTAL	46,336	2,261	1,360	3,621	1,829	2,368	4,197

^{*} Trip generation estimates are based on trip generation rates included in Trip Generation Manual, 9th Edition, ITE 2012, unless noted otherwise.

^[1] Source: Culver City Planning Division Active Projects List - January 29, 2016.

^[2] Trip generation from Traffic Impact Analysis Report, Proposed Mixed-Use Development (115-Unit Residential and 31,240 Square Foot Retail) Located at 8770 Washington Boulevard in Culver City, California Hirsch/Green Transportation Consulting, Inc., July 2010.

^[3] Trip generation from Traffic Study for the Platform at Culver Station Project, Raju Associates Inc., July 2011.

^[4] Trip generation estimates provided by the City of Culver City.

^[5] Trip generation from Culver Studios Modified Comprehensive Plan Update #6, Transportation Analysis Report Fehr & Peers, September 2015.

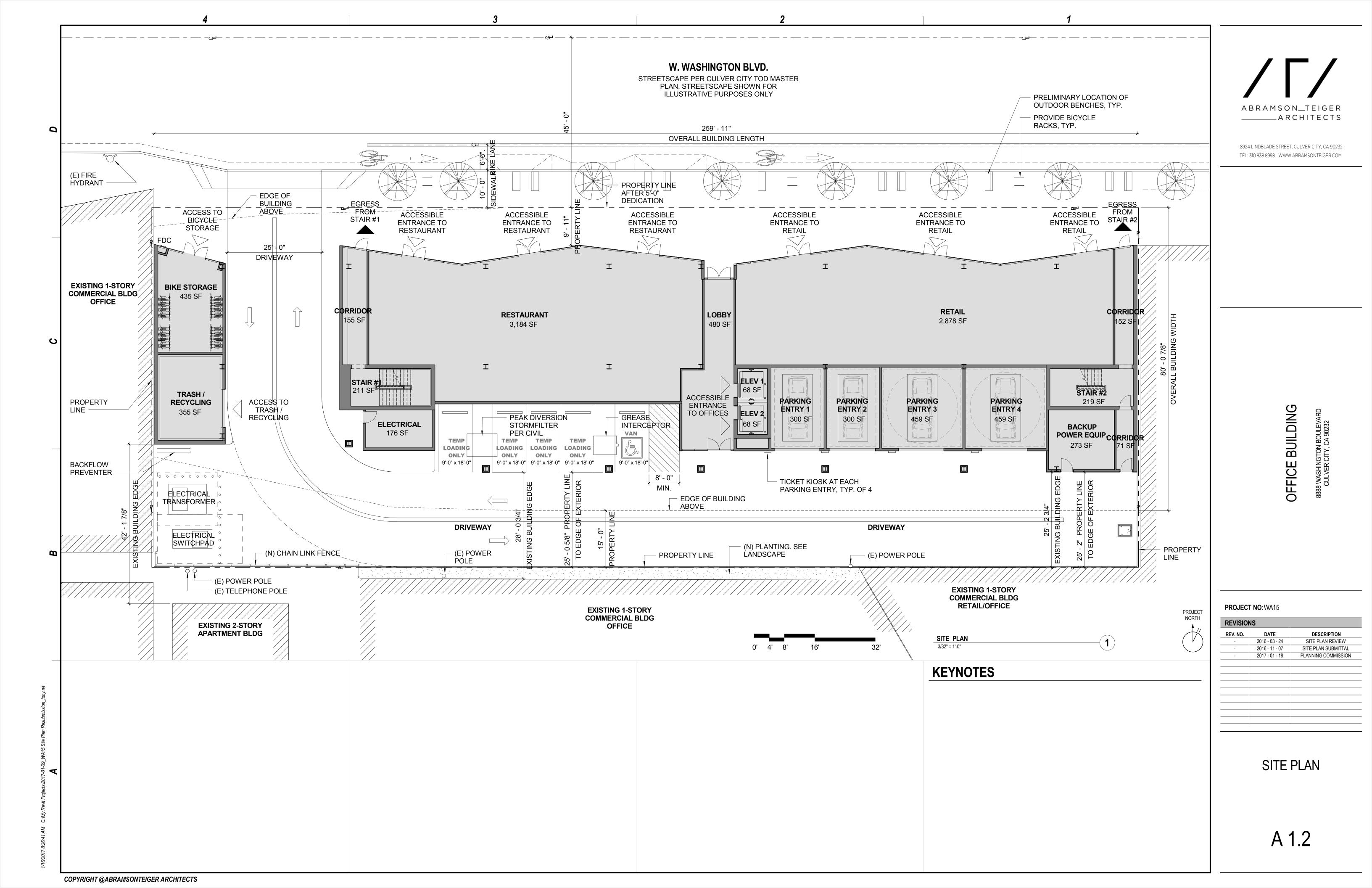
^[6] Source: Los Angeles Department of Transportation.
[7] Trip generation totals provided by LADOT, February 2011. Directional distribution based on *Trip Generation Manual*, \$th Edition, ITE 2012.
[8] Trip generation from *Traffic Study for the Jefferson & La Cienega Mixed-Use Development*, Gibson Consulting, Inc., June 2015.

ATTACHMENT D LIST OF STUDY INTERSECTIONS

	Inter	section			Signal System
#	Northbound/Southbound	Eastbound/Westbound	Jurisdiction	Signalized?	Control
1.	Robertson Boulevard	I-10 WB Off-Ramp/Kincardine Avenue	City of Los Angeles	Yes	ATSAC/ATCS
2.	Robertson Boulevard	National Boulevard	City of Los Angeles	Yes	ATSAC/ATCS
3.	National Boulevard	I-10 Eastbound On-Ramp	City of Los Angeles	Yes	ATSAC/ATCS
4.	Bagley Avenue	Venice Boulevard	City of Los Angeles	Yes	ATSAC/ATCS
5.	Culver Boulevard	Venice Boulevard	City of Los Angeles	Yes	ATSAC/ATCS
6.	Robertson Boulevard	Venice Boulevard	City of Los Angeles	Yes	ATSAC/ATCS
7.	National Boulevard	Venice Boulevard	City of Los Angeles	Yes	ATSAC/ATCS
8.	La Cienega Boulevard	Venice Boulevard [1]	City of Los Angeles	Yes	ATSAC/ATCS
9.	Culver Boulevard	Washington Boulevard/Irving Place	Culver City	Yes	ATSAC*
10.	Main Street	Culver Boulevard	Culver City	Yes	ATSAC*
11.	Culver Boulevard	Washington Boulevard	Culver City	Yes	ATSAC*
12.	Ince Boulevard	Washington Boulevard	Culver City	Yes	ATSAC*
13.	Robertson Boulevard/Higuera Street	Washington Boulevard	Culver City	Yes	ATSAC*
14.	Landmark Street	Washington Boulevard	Culver City	Yes	ATSAC*
15.	National Boulevard	Washington Boulevard	Culver City	Yes	ATSAC*
16.	Helms Avenue	Washington Boulevard	Culver City	Yes	ATSAC*
17.	La Cienega Avenue	Washington Boulevard	Culver City	Yes	ATSAC*
18.	La Cienega Boulevard	Washington Boulevard	Culver City	Yes	ATSAC*
19.	Wesley Street	National Boulevard	Culver City	Yes	ATSAC*
20.	Hayden Avenue	National Boulevard	Culver City	Yes	ATSAC*
21.	Jefferson Boulevard	National Boulevard	City of Los Angeles	Yes	ATSAC/ATCS
22.	Jefferson Boulevard	Higuera Street/Rodeo Road	City of Los Angeles	Yes	ATSAC/ATCS
23.	Robertson Boulevard	I-10 EB On-Ramp	City of Los Angeles	No	n/a
24.	Robertson Boulevard	Exposition Bl./I-10 EB Off-Ramp	City of Los Angeles	No	n/a
25.	Wesley Street	Washington Boulevard	Culver City	No (Yes in future)	Future ATSAC*
26.	Cattaraugus Avenue	Washington Boulevard	Culver City	No	n/a

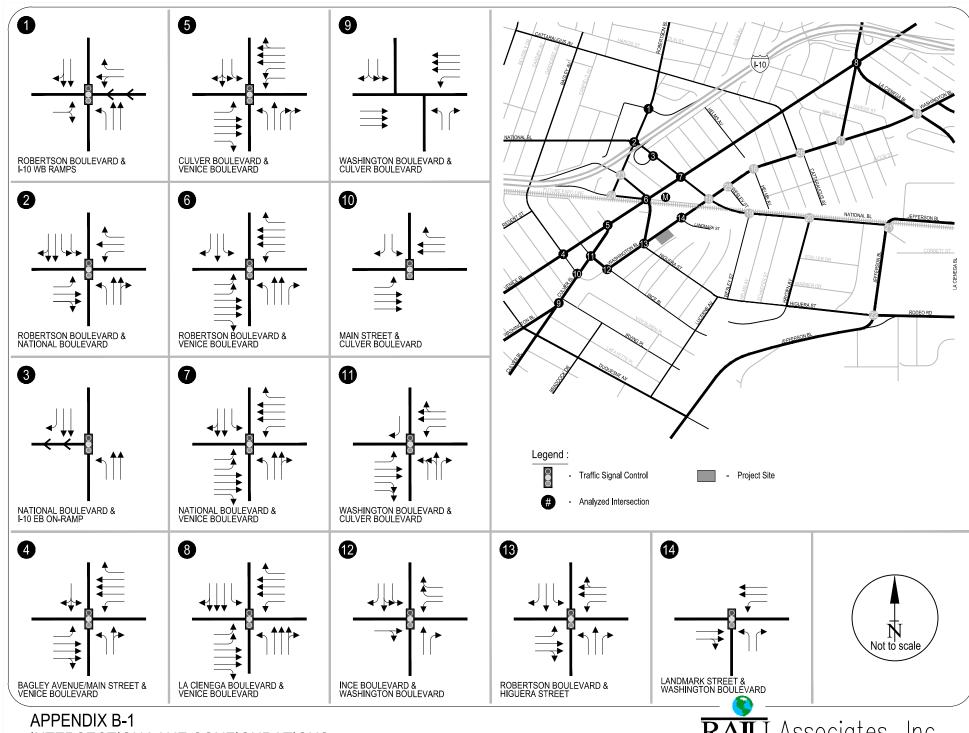
^{*} Traffic signals in Culver City have advanced traffic signal synchronization equivalent to ATSAC.

^[1] Los Angeles County Congestion Management Program monitoring location.



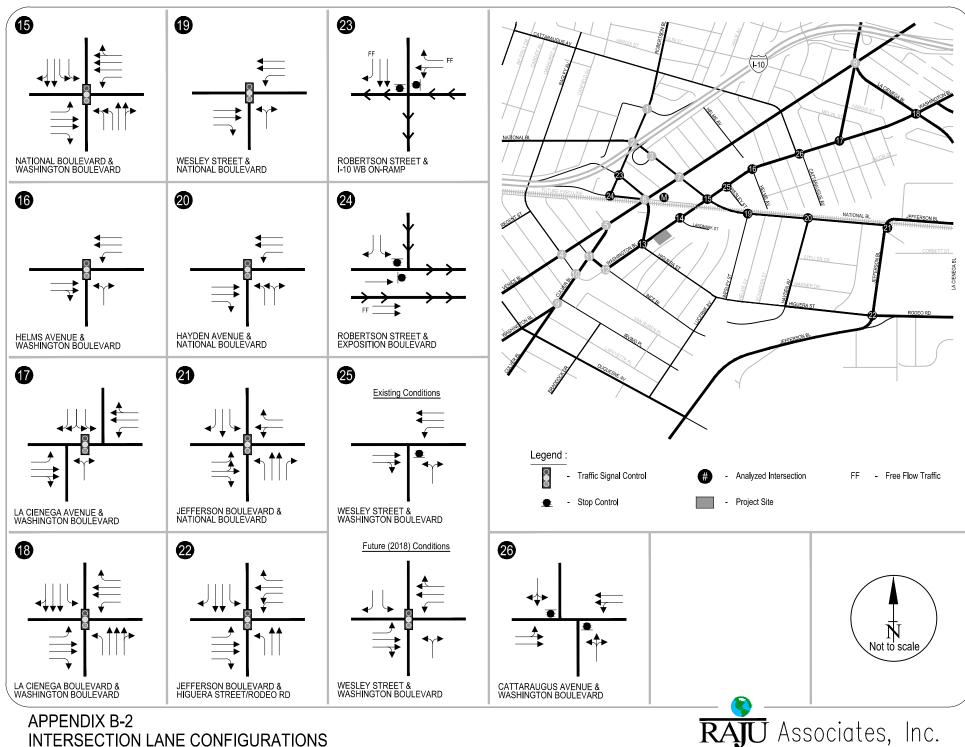
APPENDIX B

Intersection Lane Configurations



INTERSECTION LANE CONFIGURATIONS

RAJU Associates, Inc.



APPENDIX B-2 INTERSECTION LANE CONFIGURATIONS

APPENDIX C

Traffic Counts



STREET:

North/South Robertson Boulevard

East/West I-10 Westbound Off-Ramp/Kincardine Avenue

Day: Thursday Date: September 24, 2015 Weather: SUNNY

Hours: 7-10 & 3-6 Chekrs: AimTD LLC

School Day: YES District: I/S CODE

	N/B		S/B			E/B			W/B	
DUAL-					_					
WHEELED	190		274			11			109	
BIKES	20		21			5			5	
BUSES	46		39			0			12	
	N/B	TIME	S/B	TIME	=	E/B	TIME	_	W/B	TIME
AM PK 15 MIN	341	8 30	394	8 15		50	7.30		80	7 4 5

AM PK 15 MIN	341	8.30	394	8.15	50	7.30	80	7.45
PM PK 15 MIN	243	15.30	393	17.00	62	15.15	226	16.30
AM PK HOUR	1307	7.45	1528	8.45	191	7.30	249	7.00

 PM PK HOUR
 930
 17.00
 1511
 17.00
 174
 15.00
 856
 16.30

Hours 7-8 8-9 9-10 15-16 16-17 17-18

NORTHBOUND Approach	SOUTHBOUND Approach	TOTAL	XING S/L	XING N/L
---------------------	---------------------	-------	----------	----------

Hours	Lt	Th	Rt	Total
7-8	77	971	0	1048
8-9	39	1255	0	1294
9-10	17	1121	0	1138
15-16	33	844	0	877
16-17	39	794	0	833
17-18	46	884	0	930

TOTAL 251 5860 0 6120 TOTAL 0 8302 353 86									
101AL 231 3809 0 0120 101AL 0 8302 333 80	TOTAL	251	5869	0 6120	TOTAL	0	8302	3531	8655

Lt	Th	Rt	Total	N-S	Ped	Sch	Ped	Sch
0	1266	91	1357	2405	51	16	135	12
0	1431	70	1501	2795	24	1	35	0
0	1412	64	1476	2614	22	0	5	0
0	1386	43	1429	2306	31	28	28	0
0	1340	41	1381	2214	17	9	9	0
0	1467	44	1511	2441	6	0	3	0
0	8302	353	8655	14775	151	54	215	12

EASTBOUNI	D Approa	ach			WESTBOUN	D Appro	ach				TOTAL	XING	W/L	XI	NG E	/L
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total	, ,	E-W	Ped	Sch	1	Ped	Sc

Hours	Lt	ın	Κī	Total
7-8	63	0	103	166
8-9	121	0	35	156
9-10	85	0	31	116
15-16	73	0	101	174
16-17	82	0	87	169
17-18	71	0	64	135
TOTAL	495	0	421	916

			SCII
7-8 55 76 118 249 415 190	30	73	7
8-9 71 23 87 181 337 60	3	42	0
9-10 83 5 120 208 324 25	1	4	0
15-16 203 57 404 664 838 308	28	16	0
16-17 264 56 513 833 1002 123	10	16	0
17-18 278 40 522 840 975 66	2	3	0
TOTAL 954 257 1764 2975 3891 772	74	154	7

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

 DATE:
 LOCATION:
 Culver City
 PROJECT #:
 SC0715

 Thu, Sep 24, 15
 NORTH & SOUTH:
 Robertson
 LOCATION #:
 9

 EAST & WEST:
 Kincardine - I10 WB Off-Ramp
 CONTROL:
 SIGNAL

NOTES:

										PM MD OTHER	⋖ W	N S ▼	E▶
		NORTHBOU Robertson	ND		SOUTHBOUI Robertson	ND		EASTBOUN Kincardine	D		WESTBOUN Westbound Off-R		
LANES	NL : 1	NT 2	NR X	SL X	ST 2	SR 0	EL 0.5	ET X	ER 0.5	WL 0.5	WT 0.5	WR 1	TOTAL
7:00 AM	18	193	0	0	296	18	16	0	15	12	13	34	615
7:15 AM	12	211	0	0	318	25	9	0	27	11	11	30	654
7:30 AM	25	251	0	0	326	25	17	0	33	13	26	19	735
7:45 AM	22	316	0	0	326	23	21	0	28	19	26	35	816
8:00 AM	19	283	0	0	340	19	32	0	17	16	9	29	764
8:15 AM	12	314	0	0	378	16	33	0	10	15	7	25	810
8:30 AM	4	337	0	0	343	18	22	0	4	15	6	14	763
8:45 AM	4	321	0	0	370	17	34	0	4	25	1	19	795
9:00 AM	6	270	0	0	336	27	32	0	10	19	2	24	726
9:15 AM	1	312	0	0	374	10	21	0	5	19	0	19	761
9:30 AM	4	270	0	0	380	14	17	0	9	26	2	40	762
9:45 AM	6	269	0	0	322	13	15	0	7	19	1	37	689
VOLUMES	133	3,347	0	0	4,109	225	269	0	169	209	104	325	8,893
APPROACH %	4%	96%	0%	0%	95%	5%	61%	0%	38%	33%	16%	51%	
APP/DEPART	3,482	1	3,941	4,334	/	4,489	439	/	3	638	/	460	0
BEGIN PEAK HR		7:45 AM											
VOLUMES	57	1,250	0	0	1,387	76	108	0	59	65	48	103	3,153
APPROACH %	4%	96%	0%	0%	95%	5%	65%	0%	35%	30%	22%	48%	
PEAK HR FACTOR		0.958			0.928			0.852			0.675		0.96
APP/DEPART	1,307	/	1,461	1,463	/	1,512	167	/	0	216	/	180	0
03:00 PM	8	190	0	0	335	13	22	0	23	43	13	86	733
3:15 PM	14	212	0	0	349	5	25	0	37	55	13	107	817
3:30 PM	4	239	0	0	349	11	17	0	29	50	17	97	813
3:45 PM	7	203	0	0	353	14	9	0	12	55	14	114	781
4:00 PM	8	207	0	0	369	12	12	0	17	59	11	122	817
4:15 PM	9	197	0	0	327	9	29	0	24	53	21	119	788
4:30 PM	11	214	0	0	308	5	20	0	23	71	15	140	807
4:45 PM	11	176	0	0	336	15	21	0	23	81	9	132	804
5:00 PM	12	221	0	0	384	9	18	0	15	66	9	131	865
5:15 PM	12	217	0	0	360	12	18	0	12	75	8	119	833
5:30 PM	9	231	0	0	362	9	19	0	13	70	9	146	868
5:45 PM	13	215	0	0	361	14	16	0	24	67	14	126	850
VOLUMES	118	2,522	0	0	4,193	128	226	0	252	745	153	1,439	9,779
APPROACH %	4%	95%	0%	0%	97%	3%	47%	0%	53%	32%	7%	62%	
APP/DEPART	2,642	/ E 00 DM	4,187	4,321	/	5,190	479	/	3	2,337	/	399	0
BEGIN PEAK HR	4,	5:00 PM	0		1 4/7	4.4	7,	0		070	40	F00	2 417
VOLUMES	46	884	0	0	1,467	44	71	0	64	278	40	522	3,416
APPROACH %	5%	95%	0%	0%	97%	3%	53%	0%	47%	33%	5%	62%	0.00
PEAK HR FACTOR	000	0.969	4 477	1.511	0.961	1.000	405	0.844		0.40	0.933	100	0.98
APP/DEPART	930	/	1,477	1,511	/	1,809	135	/	0	840	/	130	0

		NORTH SIDE		
Robertson	WEST SIDE		EAST SIDE	Robertson
		SOUTH SIDE		
		Kincardine		

Kincardine



STREET: North/South Robertson Boulevard East/West National Boulevard September 24, 2015 Day: Thursday Date: Weather: **SUNNY** 7-10 & 3-6 Hours: Chekrs: AimTD LLC School Day: YES District: I/S CODE N/B S/BE/B W/B DUAL-WHEELED BIKES BUSES TIME S/B TIME E/B TIME W/B TIME N/B AM PK 15 MIN 8.30 8.00 8.15 7.15 PM PK 15 MIN 17.15 17.30 17.30 16.45 AM PK HOUR 8.15 7.30 8.00 7.15 PM PK HOUR 17.00 16.45 16.45 17.00 NORTHBOUND Approach **SOUTHBOUND Approach TOTAL** XING S/L XING N/L Hours Rt Total Hours Th Rt Total N-S Ped Sch Ped Sch Lt 7-8 7-8 8-9 8-9 9-10 9-10 15-16 15-16 16-17 16-17 17-18 17-18 TOTAL TOTAL **EASTBOUND Approach** WESTBOUND Approach TOTAL XING W/L XING E/L Hours Th Rt Total Hours Th Rt Total E-W Ped Sch Ped Sch 7-8 7-8 8-9 8-9 9-10 9-10 15-16 15-16 16-17 16-17 17-18 17-18 **TOTAL TOTAL**

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: LOCATION: **Culver City** PROJECT #: SC0715 NORTH & SOUTH: Thu, Sep 24, 15 Robertson LOCATION #: EAST & WEST: **National** CONTROL: **SIGNAL** NOTES: \blacksquare Ν **⋖**W E► S ▼ NORTHBOUND SOUTHBOUND **EASTBOUND** WESTBOUND Robertson Robertson NL NT NR SL ST SR ET ER WL WT WR TOTAL FΙ LANES 7:15 AM 1,040 7:30 AM 7:45 AM 1.091 8:00 AM 1,142 8:15 AM 1,110 8:30 AM 1.081 8:45 AM 1,106 9:00 AM 1,038 9:15 AM ₹ 9:30 AM 9:45 AM VOLUMES 1,892 1,520 2,529 1,570 12,260 APPROACH % 9% 86% 33% 54% 48% 5% 56% 11% 24% 22% 17% 35% APP/DEPART 2,202 3,506 4,542 3,603 2.908 3,206 2,608 1.945 BEGIN PEAK HR 8:00 AM 4,439 VOLUMES APPROACH % 9% 87% 4% 33% 59% 8% 22% 54% 24% 15% 50% 36% PEAK HR FACTOR 0.905 0.917 0.894 0.922 0.972 1,556 APP/DEPART 1.280 1 329 1 191 1 195 Ω 03:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 1.009 4:45 PM 1,046 5:00 PM 1,066 5:15 PM 1,089 Σ

		Robertson		
		NORTH SIDE		
National	WEST SIDE		EAST SIDE	National
		SOUTH SIDE		
		Robertson		

2,582

53%

0.969

D = I = - 4 = - -

50%

12%

3,109

1.126

11%

3,296

1.158

13%

15%

2,556

80%

0.965

78%

4.825

7%

1.706

8%

1.847

13%

15%

42%

42%

0.940

1,531

45%

43%

1,076

1.054

12,143

Ω

4.285

0.984

5:30 PM

5:45 PM

VOLUMES

VOLUMES

APPROACH %

BEGIN PEAK HR

APPROACH %

APP/DFPART

PEAK HR FACTOR

APP/DEPART

1.834

6%

8%

1.397

76%

5:00 PM

73%

0.891

16%

2,678

21%

1,965

5,166

1.802

35%

38%

STREET:

North/South National Boulevard

East/West I-10 Eastbound On-Ramp

September 24, 2015 Day: Thursday Date: Weather: SUNNY

7-10 & 3-6 Hours: Chekrs: AimTD LLC

School Day: YES District: I/S CODE

	N/B	S/B	E/B	W/B
DUAL-				
WHEELED	219	294	0	0
BIKES	19	21	1	0
BUSES	28	57	0	0

-	N/B	TIME	S/B	TIME	E/B	TIME	W/B	TIME
AM PK 15 MIN	281	7.15	315	8.00	0	0.00	0	0.00
PM PK 15 MIN	221	17.30	435	17.30	0	0.00	0	0.00
AM PK HOUR	1023	7.00	1165	7.45	0	0.00	0	0.00
PM PK HOUR	809	17.00	1666	16.45	0	0.00	0	0.00

Hours

7-8

8-9

9-10

15-16

16-17

17-18

TOTAL

Hours

7-8

8-9

9-10

15-16

16-17 17-18

TOTAL

NORTHBOUND A	Approach
--------------	----------

Hours

7-8

8-9

9-10

15-16

16-17

17-18

TOTAL

Lt	Th	Rt	Total
		Κι	
69	954	0	1023
40	823	0	863
64	706	0	770
50	570	0	620
75	568	0	643
135	674	0	809
422	4205	Λ	4720

SOUTHBOUND A	Approach

Lt	Th	Rt	Total
0	508	485	993
0	714	441	1155
0	629	420	1049
0	985	457	1442
0	903	684	1587
0	915	701	1616
0	4654	3188	7842

N-S	Ped	Sch	
2016	0	0	Ī
2018	0	0	Ī
1819	0	0	Ī
2062	0	0	Ī
2230 2425	2	0	
2425	0	0	
			_
12570	2	0	

XING S/L

TOTAL

Ped	Sch
3	0
11	0
20	0
35	1
35	0
12	0

116

XING N/L

EASTBOUND Approach

Hours	Lt	Th	Rt	Total
7-8	0	0	0	0
8-9	0	0	0	0
9-10	0	0	0	0
15-16	0	0	0	0
16-17	0	0	0	0
17-18	0	0	0	0
TOTAL	0	0	0	0

WESTBOUND A _l	pproach
--------------------------	---------

Lt	Th	Rt	Total
0	0	0	0
0	0	0	0
0	0	0	0
0	0	0	0
0	0	0	0
0	0	0	0
0	0	0	0

XING E/L TOTAL XING W/L

E-W	Ped	Sch	Ped	Sch
0	53	0	3	0
0	21	0	2	0
0	18	0	3	0
0	47	4	17	3
0	37	2	9	0
0	37	0	7	1
<u>-</u>	·			
0	213	6	41	4

	Thu, Sep 24, 15	LOCATION NORTH & EAST & W	SOUTH:	PREPA	Culver City National	AimTD LLC. y oound On-R		3 7888 paci	fic@aimtd.c	PROJECT 7 LOCATION CONTROL:	#:	SC0715 11 SIGNAL		
	NOTES:										AM PM MD OTHER	⋖ W	N S	E►
		N	NORTHBOUN	ID		SOUTHBOU	ND		EASTBOUNI	D	OTHER ▼ WESTBOUND			
		NL	National NT	NR	SL	National ST	SR	I-10 EL	0 Eastbound On-F	Ramp	VL	0 Eastbound On-F	Ramp WR	TOTAL
	LANES:	1	2	Χ	X	2	1	X	X	X	X	X	X	
	7:00 AM	29	248	0	0	78	139	0	0	0	0	0	0	494
	7:15 AM 7:30 AM	22 9	259 234	0	0	105 144	137 95	0	0	0	0	0	0	523 482
	7:45 AM	9	213	0	0	181	114	0	0	0	0	0	0	517
	8:00 AM	7	239	0	0	196	119	0	0	0	0	0	0	561
	8:15 AM	10	208	0	0	192	118	0	0	0	0	0	0	528
	8:30 AM 8:45 AM	9 14	192 184	0	0	156 170	89 115	0	0	0	0	0	0	446 483
	9:00 AM	14	175	0	0	196	90	0	0	0	0	0	0	475
Ξ	9:15 AM	13	182	0	0	174	103	0	0	0	0	0	0	472
1	9:30 AM	18	167	0	0	126	122	0	0	0	0	0	0	433
	9:45 AM VOLUMES	19 173	182 2,483	0	0	133 1,851	105 1,346	0	0	0	0	0	0	439 5,856
	APPROACH %	7%	93%	0%	0%	58%	42%	0%	0%	0%	0%	0%	0%	3,030
	APP/DEPART	2,656	1	2,484	3,198	/	1,851	0	/	0	0	/	1,519	0
	BEGIN PEAK HR	25	7:30 AM	0	0	710	447		0	0	0	0	0	2.000
	VOLUMES APPROACH %	35 4%	894 96%	0 0%	0 0%	713 62%	446 38%	0 0%	0 0%	0 0%	0 0%	0 0%	0 0%	2,088
	PEAK HR FACTOR	470	0.944	070	070	0.920	3070	070	0.000	070	070	0.000	070	0.930
	APP/DEPART	929	1	894	1,159	/	713	0	/	0	0	/	481	0
	03:00 PM	12	176	0	0	222	102	0	0	0	0	0	0	512
	3:15 PM 3:30 PM	14 10	125 127	0	0	255 270	114 114	0	0	0	0	0	0	508 521
	3:45 PM	14	142	0	0	238	127	0	0	0	0	0	0	521
	4:00 PM	22	121	0	0	226	170	0	0	0	0	0	0	539
	4:15 PM 4:30 PM	19 13	142 153	0	0	220 207	159 177	0	0	0	0	0	0	540 550
	4:45 PM	21	153	0	0	250	177	0	0	0	0	0	0	601
	5:00 PM	23	169	0	0	234	143	0	0	0	0	0	0	569
٤	5:15 PM	30	166	0	0	222	204	0	0	0	0	0	0	622
١.	5:30 PM 5:45 PM	41 41	180 159	0	0	255 204	180 174	0	0	0	0	0	0	656 578
	VOLUMES	260	1,812	0	0	2,803	1,842	0	0	0	0	0	0	6,723
	APPROACH %	13%	87%	0%	0%	60%	40%	0%	0%	0%	0%	0%	0%	
	APP/DEPART	2,074		1,815	4,646	/	2,805	0	/	0	0	/	2,101	0
	BEGIN PEAK HR VOLUMES	115	4:45 PM 667	0	0	961	705	0	0	0	0	0	0	2,448
	APPROACH %	15%	85%	0%	0%	58%	42%	0%	0%	0%	0%	0%	0%	2,440
	PEAK HR FACTOR		0.885			0.957			0.000			0.000		0.932
	APP/DEPART	782		667	1,666	/	961	0	/	0	0	/	820	0
					ĺ	National		1						
						NORTH SID	ÞΕ				-			
	I-10 Eastbound	On-Ramp)	WEST SIDE				EAST SIDE	Ē	I-10 East	bound On	-Ramp		
					1	SOUTH SID)F				_			

National



STREET: North/South	Bagley Aven	ue						
East/West	Venice Boule	evard						
Day:	Thursday	Date:	September 24, 2	Weather:	SUNNY			
Hours: 7-10	& 3-6		Chek	AimTD LI	<u>c </u>			
School Day:	YES	District:		I/S COD	DE			
DUAL	N/B	_	S/B	<u>E/B</u>	_	W/B		
DUAL- WHEELED BIKES	35 35		35 48	309 94		370 150		
BUSES	2		26	77		97		
	N/B	TIME	S/B TIME	E/B	TIME _	W/B TIME		
AM PK 15 MIN	104	8.30	122 8.00	364	8.30	442 9.30		
PM PK 15 MIN	57	15.30	111 17.15	409	17.45	464 17.15		
AM PK HOUR	374	7.45	448 8.00	1422	8.00	1607 9.00		
PM PK HOUR	203	16.15	414 16.30	1412	17.00	1760 17.00		
NORTHBOUND A	Approach		SOUTHBOU	JND Approach		TOTAL	XING S/L	XING N/L
Hours L 7-8 8-9 9-10 15-16 16-17 17-18	Th 51 191 66 251 43 174 46 95 39 142 50 112	Rt Total 43 285 29 346 19 236 33 174 14 195 37 199	Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt Th 35 126 63 244 33 177 49 160 53 244 63 268	Rt Total 87 248 141 448 119 329 73 282 90 387 70 401	N-S 533 794 565 456 582 600	Ped Sch 43 3 36 0 30 0 56 1 42 3 56 0	Ped Sch 40 1 39 1 37 7 49 2 55 2 71 1
TOTAL	295 965	175 1435	TOTAL	296 1219	580 2095	3530	263 7	291 14
EASTBOUND App	proach		WESTBOUN	ND Approach		TOTAL	XING W/L	XING E/L
17-18	t Th 64 1087 59 1337 96 1029 94 1211 103 1163 116 1236	Rt Total 19 1170 26 1422 24 1149 75 1380 104 1370 60 1412 308 7903	Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt Th 35 1297 52 1431 44 1533 95 1282 104 1315 111 1604 441 8462	Rt Total 29 1361 30 1513 30 1607 48 1425 40 1459 45 1760 222 9125	E-W 2531 2935 2756 2805 2829 3172	Ped Sch 28 0 38 2 30 0 49 3 51 7 85 8	Ped Sch 41 1 75 3 67 1 66 4 60 4 67 2 376 15

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com DATE: LOCATION: **Culver City** PROJECT #: SC0715 NORTH & SOUTH: Thu, Sep 24, 15 **Bagley** LOCATION #: EAST & WEST: Venice CONTROL: **SIGNAL** NOTES: \blacksquare Ν **⋖**W E► S ▼ NORTHBOUND SOUTHBOUND **EASTBOUND** WESTBOUND Bagley Bagley Venice NL NT NR SL SR EL ET ER WL WT WR TOTAL ST LANES 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM 9:00 AM 9:15 AM ₹ 9:30 AM 9:45 AM VOLUMES 3,453 4,261 10,114 92% APPROACH % 10% 34% 2% 95% 2% 18% 71% 13% 53% 6% 3% APP/DEPART 1.025 3,741 3.695 4,481 4,834 BEGIN PEAK HR 8:00 AM VOLUMES 1,337 1,431 3.729 APPROACH % 19% 73% 8% 14% 54% 31% 4% 94% 2% 3% 95% 2% PEAK HR FACTOR 0.832 0.918 0.977 0.953 0.970 APP/DEPART 1 422 1.437 1 513 1,653 Ω 03:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM Q 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM Σ 5:30 PM 5:45 PM 1,022 VOLUMES 3,610 4,201 10,444 APPROACH % 24% 61% 15% 15% 63% 22% 8% 6% 7% 90% 3% 87% APP/DEPART 1,070 1.140 4,162 3.940 4.644 4,650 Ω BEGIN PEAK HR 5:00 PM 1,236 1,604 VOLUMES 3,772 16% 19% 17% 88% APPROACH % 25% 56% 67% 8% 4% 6% 91% 3% PEAK HR FACTOR 0.939 0.903 0.863 0.948 0.923 1,412 1.354 1.760 1,746 APP/DFPART **Bagley**

		NORTH SIDE		
Venice	WEST SIDE		EAST SIDE	Venice
		SOUTH SIDE		
		Bagley		



TOTAL

TOTAL

STREET: North/South Culver Boulevard East/West Venice Boulevard October 15, 2015 Day: Thursday Date: Weather: **SUNNY** 7-10 & 3-6 Hours: Chekrs: AimTD LLC School Day: YES District: I/S CODE N/B S/BE/B W/B DUAL-WHEELED BIKES BUSES TIME S/B TIME TIME W/B TIME N/B E/B AM PK 15 MIN 9.00 8.45 8.00 9.45 PM PK 15 MIN 17.45 17.30 15.00 17.30 AM PK HOUR 8.15 8.15 7.30 9.00 PM PK HOUR 17.00 16.00 15.00 17.00 TOTAL NORTHBOUND Approach **SOUTHBOUND Approach** XING S/L XING N/L Hours Rt Total Hours Th Rt Total N-S Ped Sch Ped Sch Lt 7-8 7-8 8-9 8-9 9-10 9-10 15-16 15-16 16-17 16-17 17-18 17-18 TOTAL TOTAL **EASTBOUND Approach** WESTBOUND Approach TOTAL XING W/L XING E/L Hours Th Rt Total Hours Th Rt Total E-W Ped Sch Ped Sch 7-8 7-8 8-9 8-9 9-10 9-10 15-16 15-16 16-17 16-17 17-18 17-18

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

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 DATE:
 LOCATION:
 Culver
 PROJECT #:
 SC0743

 Thu, Oct 15, 15
 NORTH & SOUTH:
 Culver
 LOCATION #:
 1

 EAST & WEST:
 Venice
 CONTROL:
 SIGNAL

NOTES:

											MD	⋖ W	_	E ▶
											OTHER OTHER		S ▼	
													·	
		1	NORTHBOU	ND	S	OUTHBOUN	ID		EASTBOUN	D	/	WESTBOUN	D	
			Culver			Culver		Venice		Venice				
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	1	1	2	1	0.5	0.5	1	3	0	2	3	0	
	7:00 AM	3	5	111	20	5	6	1	216	1	44	307	25	744
	7:15 AM	11	8	160	25	7	3	5	229	3	76	350	24	901
	7:30 AM	8	14	164	30	7	3	5	357	3	61	360	25	1,037
	7:45 AM	5	13	169	35	7	5	3	293	1	68	363	17	979
	8:00 AM	7	9	180	32	5	5	3	359	5	71	420	33	1,129
	8:15 AM	9	12	154	30	11	11	8	314	1	87	379	30	1,046
	8:30 AM	12	7	190	40	8	6	4	317	3	75	351	42	1,055
	8:45 AM	8	15	152	40	13	7	5	295	4	91	373	35	1,038
	9:00 AM	14	15	181	28	9	12	7	280	6	88	360	33	1,033
~	9:15 AM	11	4	154	28	10	6	9	286	3	83	408	37	1,039
AM	9:30 AM	15	13	148	28	4	10	5	226	4	88	379	37	957
	9:45 AM	14	10	146	34	14	6	9	260	8	86	409	46	1,042
	VOLUMES	117	125	1,909	370	100	80	64	3,432	42	918	4,459	384	12,000
	APPROACH %	5%	6%	89%	67%	18%	15%	2%	97%	1%	16%	77%	7%	,
	APP/DEPART	2,151	1	572	550	/	1,060	3,538	/	5,712	5,761	/	4,656	0
	BEGIN PEAK HR	_,	8:00 AM				.,	-,	·	-,		·	.,,,,,	
	VOLUMES	36	43	676	142	37	29	20	1.285	13	324	1,523	140	4,268
	APPROACH %	5%	6%	90%	68%	18%	14%	2%	97%	1%	16%	77%	7%	1,200
	PEAK HR FACTOR	0,0	0.903	,0,0	0070	0.867	,0	270	0.898	.,,	.070	0.948	,,,,	0.945
	APP/DEPART	755	1	202	208	/	373	1.318	/	2.104	1.987	/	1.589	0.710
	03:00 PM	20	9	168	44	13	8	10	321	8	80	329	34	1.044
	3:15 PM	15	16	176	45	12	4	4	300	7	80	337	33	1,029
	3:30 PM	17	18	192	55	9	3	2	299	15	94	360	39	1,103
	3:45 PM	13	10	195	49	5	8	3	323	6	88	349	38	1,087
	4:00 PM	21	5	203	60	7	5	3	309	7	91	322	27	1,060
	4:15 PM	16	9	185	55	5	7	5	320	4	88	361	34	1,089
	4:30 PM	14	16	215	64	5	6	3	274	5	81	342	40	1,065
	4:45 PM	17	11	186	61	8	6	4	314	1	110	336	22	1,076
	5:00 PM	20	9	180	53	10	3	1	321	4	104	352	22	1,079
_	E 45 D14	21	16	210	50	6	10	1	281	3	77	369	33	1,077
₹	5:30 PM	22	7	200	67	10	4	4	284	6	103	435	40	1,182
	5:45 PM	12	15	221	59	9	6	3	304	4	93	437	33	1,196
	VOLUMES	208	141	2,331	662	99	70	43	3,650	70	1,089	4,329	395	13,087
	APPROACH %	8%	5%	87%	80%	12%	8%	1%	97%	2%	19%	74%	7%	13,007
	APP/DEPART	2.680	1	579	831	/	1.256	3.763	1	6.646	5.813	/	4.606	0
	BEGIN PEAK HR	2,000	5:00 PM	317	001	,	1,230	5,705		0,040	0,010		7,000	J
	VOLUMES	75	47	811	229	35	23	9	1,190	17	377	1,593	128	4,534
	APPROACH %	8%	5%	87%	80%	12%	23 8%	1%	98%	1%	18%	76%	6%	7,004
	PEAK HR FACTOR	0 70	0.941	0170	00 70	0.886	0 70	1 /0	0.933	1 70	1070	0.907	0 /0	0.948
	APP/DEPART	933	U.741	184	287	/	428	1,216	U.733 /	2,231	2.098	0.707	1,691	0.948
	ALT/DEFAILT	733		104	207	/	420	1,210		۷,۷۵۱	2,070	/	1,071	U

		NORTH SIDE		
Venice	WEST SIDE		EAST SIDE	Venice
		SOUTH SIDE		
		Culver		

Culver

Turning Movement Count Report AM

Location ID: 5

North/South: Robertson Blvd Date: 02/18/15
East/West: Venice Blvd City: Culver City, CA

	5	Southbound	d	١	Nestbound	1	^	Vorthboun	d		Eastbound	1	
	1	2	3	4	5	6	7	8	9	10	11	12	Totals:
Movements:	R	Т	L	R	Т	L	R	Т	L	R	Т	L	TOtals.
7:00	53	36	30	60	234	7	8	64	10	5	242	65	814
7:15	69	29	39	54	222	7	9	94	21	6	286	64	900
7:30	70	36	48	44	274	6	7	91	20	12	349	89	1046
7:45	71	67	69	34	285	5	8	90	25	9	322	90	1075
8:00	77	69	64	53	281	12	7	98	20	9	390	61	1141
8:15	68	57	59	36	317	13	9	90	28	9	408	98	1192
8:30	101	50	59	60	310	13	8	100	17	19	404	98	1239
8:45	97	73	59	51	344	10	16	85	15	23	408	86	1267
9:00	102	70	54	38	336	9	9	101	19	12	350	89	1189
9:15	95	53	45	75	324	14	13	79	14	18	342	88	1160
9:30	77	60	56	99	267	16	8	75	15	18	331	71	1093
9:45	98	49	52	60	329	6	21	69	17	24	300	63	1088
Total Volume:	978	649	634	664	3523	118	123	1036	221	164	4132	962	13204
Approach %	43%	29%	28%	15%	82%	3%	9%	75%	16%	3%	79%	18%	
		_			4.407								-
Peak Hr Begin:	8:15				1407								
PHV	368	250	231	185	1307	45	42	376	79	63	1570	371	4887
PHF		0.927			0.949			0.963			0.962		0.964

City Count, LLC. www.citycount.com

Turning Movement Count Report PM

Location ID: 5

North/South: Robertson Blvd Date: 02/18/15
East/West: Venice Blvd City: Culver City, CA

	S	outhbound	d	١	Nestbound	1	^	Vorthboun	d		Eastbound	1	
	1	2	3	4	5	6	7	8	9	10	11	12	Totals:
Movements:	R	Т	L	R	Т	L	R	Т	L	R	Т	L	TOtals.
15:00	70	54	59	25	278	10	10	67	20	26	437	79	1135
15:15	79	33	43	20	237	6	11	62	12	37	402	70	1012
15:30	78	46	60	21	297	12	12	48	10	31	440	81	1136
15:45	88	39	56	22	241	6	11	65	22	23	447	74	1094
16:00	89	41	52	21	242	6	12	63	18	33	441	68	1086
16:15	64	45	56	20	263	9	14	46	20	33	468	79	1117
16:30	82	35	61	19	246	9	11	87	17	24	445	97	1133
16:45	75	30	51	24	275	13	15	75	22	29	367	98	1074
17:00	71	32	41	23	299	10	15	84	15	21	442	95	1148
17:15	86	46	41	33	301	15	13	86	23	25	485	101	1255
17:30	104	39	36	19	344	17	17	90	27	28	422	119	1262
17:45	83	45	42	30	292	19	17	86	32	23	382	131	1182
	-												-
Total Volume:	969	485	598	277	3315	132	158	859	238	333	5178	1092	13634
Approach %	47%	24%	29%	7%	89%	4%	13%	68%	19%	5%	78%	17%	
	- '	•			4.400			·	·		·		- -
Peak Hr Begin:	17:00				1436								
PHV	344	162	160	105	1236	61	62	346	97	97	1731	446	4847
PHF		0.930			0.922			0.935			0.930		0.960

City Count, LLC. www.citycount.com



STREET:

North/South National Boulevard

East/West Venice Boulevard

Day: Thursday Date: September 24, 2015 Weather: SUNNY

Hours: 7-10 & 3-6 Chekrs: AimTD LLC

School Day: YES District: I/S CODE

	N/B	S/B	E/B	W/B
DUAL-				· <u> </u>
WHEELED	258	184	402	378
BIKES	23	34	85	160
BUSES	22	45	159	85

-	N/B	TIME	S/B	TIME	E/B	TIME	W/B	TIME
AM PK 15 MIN	314	7.00	205	9.00	519	8.00	444	9.30
PM PK 15 MIN	236	17.00	301	15.30	545	17.45	393	17.00
AM PK HOUR	1113	7.00	751	7.45	1991	8.00	1583	9.00
PM PK HOUR	895	17.00	1031	16.45	2108	15 45	1471	17 00

Hours 7-8 8-9 9-10

NORTHBOUND Approach	SOUTHBOUND Approach	TOTAL	XING S/L	XING N/L
---------------------	---------------------	-------	----------	----------

Hours	Lt	Th	Rt	Total
7-8	297	792	24	1113
8-9	225	625	27	877
9-10	203	575	38	816
15-16	159	447	57	663
16-17	200	475	82	757
17-18	199	603	93	895
			•	
TOTAL	1283	3517	321	5121

159	447	57	663	15-16	180	681	76	937
200	475	82	757	16-17	118	713	61	892
199	603	93	895	17-18	140	771	55	966
1283	3517	321	5121	TOTAL	686	3548	415	4649

Lt	Th	Rt	Total	N-S	Ped	Sch	Ped	l Sch
53	371	60	484	1597	93	35	86	56
104	557	80	741	1618	47	0	55	0
91	455	83	629	1445	38	0	66	6
180	681	76	937	1600	59	13	97	43
118	713	61	892	1649	64	5	73	18
140	771	55	966	1861	40	3	76	5 14
			<u>.</u>	<u></u>			<u>-</u>	
686	3548	415	4649	9770	341	56	453	3 137

Ped

113

419

Sch

12

144

EASTBOUND Approach	WESTBOUND Approach	TOTAL	XING W/L	XING E/L
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Hours	Lt	Th	Rt	Total
7-8	144	1073	357	1574
8-9	141	1441	409	1991
9-10	126	1173	361	1660
15-16	131	1555	296	1982
16-17	140	1603	322	2065
17-18	163	1539	307	2009
	-			<u></u>
TOTAL	845	8384	2052	11281

Hours	Lt	Th	Rt	Total	E-W	 Ped	Sch	_	
7-8	54	1272	96	1422	2996	118	47		
8-9	69	1233	80	1382	3373	63	1		_
9-10	64	1405	114	1583	3243	34	2		
15-16	62	1041	55	1158	3140	94	78		
16-17	69	1192	49	1310	3375	75	34		
17-18	89	1324	58	1471	3480	72	32		
·								•	
TOTAL	407	7467	452	8326	19607	456	194		

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: LOCATION: **Culver City** PROJECT #: SC0715 National Thu, Sep 24, 15 NORTH & SOUTH: LOCATION #: EAST & WEST: Venice CONTROL: **SIGNAL** NOTES: \blacksquare Ν **⋖**W E► S ▼ NORTHBOUND SOUTHBOUND **EASTBOUND** WESTBOUND National National Venice NL NT NR SL SR ET ER WL WT WR TOTAL ST FΙ LANES 1.109 7:15 AM 1,144 7:30 AM 1,096 1,244 7:45 AM 8:00 AM 1,338 8:15 AM 1,240 8:30 AM 1,214 8:45 AM 1,199 9:00 AM 1,211 9:15 AM O 1,189 ξ 9:30 AM 1,140 9:45 AM 1.148 VOLUMES 1,992 1,383 3,687 1,127 14,272 APPROACH % 3% 75% 89% 26% 71% 13% 12% 8% 71% 22% 4% 7% APP/DEPART 2,806 2,683 1,854 2,697 5,225 4,024 4,387 4,868 BEGIN PEAK HR 7:45 AM 5,036 1,398 1,252 VOLUMES APPROACH % 25% 71% 4% 13% 78% 10% 6% 71% 23% 5% 90% 5% PEAK HR FACTOR 0.942 0.929 0.944 0.942 0.941 APP/DEPART 1 093 1 960 1.526 1.391 1 566 Ω 1,178 03:00 PM 3:15 PM 1,079 3:30 PM 1,272 1,211 3:45 PM 4:00 PM 1.235

Venice WEST SIDE EAST SIDE Venice

SOUTH SIDE

National

4:15 PM

4:30 PM

4:45 PM

5:00 PM

5:15 PM

5:30 PM

5:45 PM

VOLUMES

VOLUMES

APPROACH %

BEGIN PEAK HR

APPROACH %

APP/DFPART

PEAK HR FACTOR

APP/DEPART

2,315

22%

24%

1,525

66%

5:00 PM

67%

0.948

10%

2,102

10%

2,795

14%

16%

2,165

77%

80%

0.901

3,298

1.162

6%

7%

6,056

2.009

8%

7%

4,697

1,539

77%

0.922

78%

5,378

15%

1.776

15%

3.939

1,471

6%

6%

3.557

1,324

90%

0.936

90%

4,327

1.585

4%

4%

1,264

1.280

1,245

1,407

1,283

1,369

1.282

15,105

Ω

5,341

0.949

Intersection Turning Movement Prepared by: National Data & Surveying Services

Project ID: 16-5759-001 Day: Wednesday

Date: 11/9/2016

City: Los Angeles AM

NS/EW Streets:	la	Cienega Blv	d	lai	Cienega Blv	'd		/enice Blvd		\	/enice Blvd		
1437 EVV 311 0013.		ORTHBOUN			OUTHBOUN			EASTBOUND	`		VESTBOUND	<u> </u>	
	144	OKTHBOON	D	30	JUTIBOUN	ID.	EASTBOOND		,	WESTBOOND			
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	1	3	0	1	3	0	2	3	0	1	3.5	0.5	
7:00 AM	38	377	23	9	196	37	52	198	16	26	390	6	1368
7:15 AM	46	414	18	6	264	42	52	248	19	23	365	3	1500
7:30 AM	41	463	17	12	216	27	75	248	11	49	366	4	1529
7:45 AM	49	403	9	20	269	47	65	292	23	48	317	9	1551
8:00 AM	42	474	20	31	315	45	68	264	33	57	296	12	1657
8:15 AM	48	385	16	27	330	58	68	322	27	43	283	27	1634
8:30 AM	39	416	11	35	219	55	76	302	27	40	323	29	1572
8:45 AM	43	358	10	25	296	84	62	299	40	39	332	17	1605
9:00 AM	42	384	13	23	259	66	69	278	39	36	363	24	1596
9:15 AM	47	300	7	14	286	54	65	236	32	44	346	16	1447
9:30 AM	37	322	15	11	251	67	59	227	25	41	371	12	1438
9:45 AM	48	241	10	17	327	75	54	225	33	38	306	6	1380
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	520	4537	169	230	3228	657	765	3139	325	484	4058	165	18277
APPROACH %'s:	9.95%	86.82%	3.23%	5.59%	78.44%	15.97%	18.09%	74.23%	7.69%	10.28%	86.21%	3.51%	
PEAK HR START TIME :	800 /	AM											TOTAL
PEAK HR VOL:	172	1633	57	118	1160	242	274	1187	127	179	1234	85	6468
PEAK HR FACTOR:		0.868			0.916			0.952			0.955		0.976

CONTROL : Sginalized

Intersection Turning Movement Prepared by: National Data & Surveying Services

Project ID: 16-5759-001 Day: Wednesday City: Los Angeles Date: 11/9/2016

				PM								-	
NS/EW Streets:	La	Cienega Blv	d	La	Cienega Blv	rd	١	venice Blvd Venice Blvd					
	N	ORTHBOUN	D	SC	OUTHBOUN	D	EASTBOUND			WESTBOUND			
LANES:	NL 1	NT 3	NR 0	SL 1	ST 3	SR 0	EL 2	ET 3	ER 0	WL 1	WT 3.5	WR 0.5	TOTAL
LANES.		J	U		3	U	2	J	O		3.3	0.5	
3:00 PM	17	224	13	10	298	51	73	345	48	39	218	3	1339
3:15 PM	15	233	10	18	284	57	73	325	39	38	232	4	1328
3:30 PM	20	217	19	20	310	62	76	350	43	49	250	11	1427
3:45 PM	19	214	11	19	370	59	58	305	41	39	201	6	1342
4:00 PM	12	218	18	14	310	43	60	356	30	30	233	6	1330
4:15 PM	24	191	13	12	326	52	68	331	42	39	225	5	1328
4:30 PM	14	246	19	23	335	48	66	367	40	48	249	3	1458
4:45 PM	22	251	22	13	334	61	70	329	42	46	248	3	1441
5:00 PM	25	239	18	10	334	44	82	362	48	46	272	6	1486
5:15 PM	27	233	20	18	399	47	70	340	33	36	261	15	1499
5:30 PM	17	238	15	19	322	47	64	365	29	44	310	5	1475
5:45 PM	19	216	15	26	319	60	71	304	44	44	257	10	1385
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	231	2720	193	202	3941	631	831	4079	479	498	2956	77	16838
APPROACH %'s:	7.35%	86.51%	6.14%	4.23%	82.55%	13.22%	15.42%	75.69%	8.89%	14.10%	83.72%	2.18%	
PEAK HR START TIME :	445 l	PM											TOTAL
PEAK HR VOL:	91	961	75	60	1389	199	286	1396	152	172	1091	29	5901
PEAK HR FACTOR:		0.955			0.888			0.932			0.900		0.984

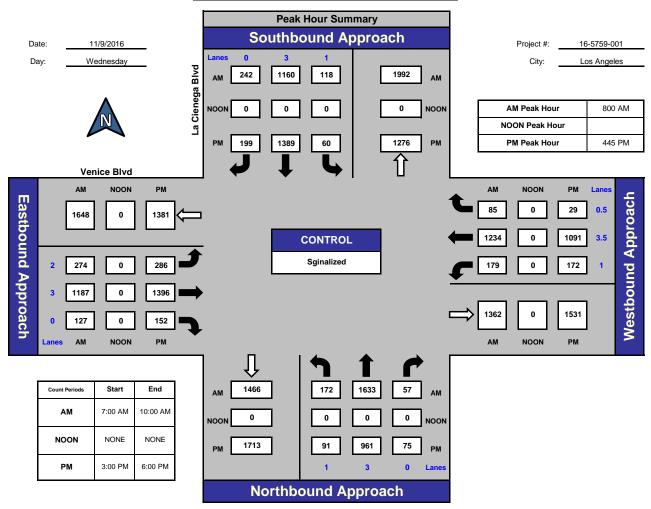
CONTROL : Sginalized

ITM Peak Hour Summary

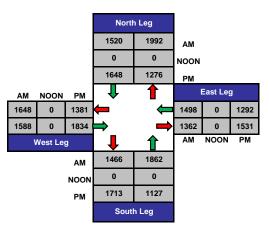


National Data & Surveying Services

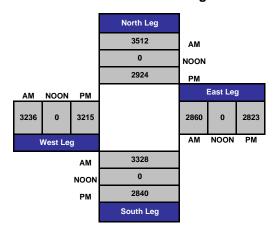
La Cienega Blvd and Venice Blvd , Los Angeles



Total Ins & Outs



Total Volume Per Leg



PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

<u>DATE:</u> Tue, Apr 14, 15

LOCATION: NORTH & SOUTH:

Culver City Washington-Irving Place

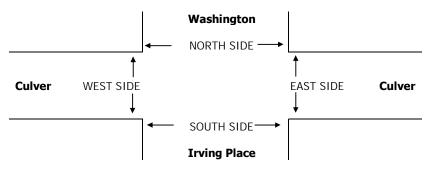
PROJECT #: LOCATION #:

SC0575 76

EAST & WEST: Culver CONTROL: SIGNAL

NOTES:	AM		A	I
	PM		N	
	MD	▼ W	-: -	E►
	OTHER		S	
	OTHER		▼	

		NORTHBOUND			SC	OUTHBOU	ND	EASTBOUND			WESTBOUND			
			Irving Place			Washington			Culver			Culver		
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	1	X	1	2	X	0	X	3	0	1	3	0	
	7:00 AM	8	0	15	57	0	5	0	203	0	4	282	0	574
	7:15 AM	6	0	8	84	0	3	0	265	0	3	349	0	718
	7:30 AM	7	0	13	110	0	0	0	294	0	7	411	0	842
	7:45 AM	19	0	15	141	0	2	0	287	0	10	476	0	950
	8:00 AM	32	0	24	152	0	8	0	269	0	9	347	0	841
	8:15 AM	26	0	24	146	0	9	0	317	0	13	396	0	931
	8:30 AM	32	0	23	158	0	8	0	275	0	11	388	0	895
Ā	8:45 AM	30	0	31	146	0	6	0	280	0	7	438	0	938
⋖	VOLUMES	160	0	153	994	0	41	0	2,190	0	64	3,087	0	6,689
	APPROACH %	51%	0%	49%	96%	0%	4%	0%	100%	0%	2%	98%	0%	
	APP/DEPART	313	1	0	1,035	/	64	2,190	/	3,337	3,151	/	3,288	0
	BEGIN PEAK HR		7:45 AM											
	VOLUMES	109	0	86	597	0	27	0	1,148	0	43	1,607	0	3,617
	APPROACH %	56%	0%	44%	96%	0%	4%	0%	100%	0%	3%	97%	0%	
	PEAK HR FACTOR		0.871			0.940			0.905			0.849		0.952
	APP/DEPART	195		0	624	/	43	1,148	/	1,831	1,650	/	1,743	0
	4:00 PM	8	0	11	183	0	1	0	279	0	6	315	0	803
	4:15 PM	10	0	16	172	0	2	0	253	0	7	298	0	758
	4:30 PM	21	0	17	222	0	6	0	229	0	7	337	0	839
	4:45 PM	11	0	7	193	0	5	0	289	0	11	295	0	811
	5:00 PM	8	0	13	206	0	3	0	270	0	5	291	0	796
	5:15 PM	9	0	17	235	0	4	0	294	0	9	301	0	869
	5:30 PM	8	0	12	224	0	6	0	323	0	7	351	0	931
Σ	5:45 PM	9	0	18	237	0	5	0	315	0	12	337	0	933
-	VOLUMES	84	0	111	1,672	0	32	0	2,252	0	64	2,525	0	6,740
	APPROACH %	43%	0%	57%	98%	0%	2%	0%	100%	0%	2%	98%	0%	
	APP/DEPART	195		0	1,704	/	64	2,252	/	4,035	2,589	/	2,641	0
	BEGIN PEAK HR		5:00 PM											
	VOLUMES	34	0	60	902	0	18	0	1,202	0	33	1,280	0	3,529
	APPROACH %	36%	0%	64%	98%	0%	2%	0%	100%	0%	3%	97%	0%	
	PEAK HR FACTOR		0.870			0.950			0.930			0.917		0.946
	APP/DEPART	94	/	0	920	/	33	1,202	/	2,164	1,313	/	1,332	0



PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

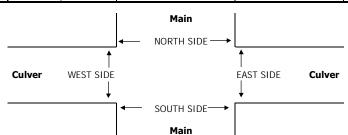
 DATE:
 LOCATION:
 Culver City
 PROJECT #:
 SC0715

 Thu, Sep 24, 15
 NORTH & SOUTH:
 Main
 LOCATION #:
 1

 EAST & WEST:
 Culver
 CONTROL:
 SIGNAL

NOTES:	AM	A	
	PM	N	
	MD ◀ W	•	E►
	OTHER	S	
	OTHER	•	

		NORTHBOUND			SOUTHBOUND		ND	EASTBOUND			WESTBOUND			
			Main			Main			Culver			Culver		
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	X	X	Χ	1	X	1	1	3	X	X	3	0	
Г	7:00 AM	0	0	0	15	0	14	42	295	0	0	280	11	657
	7:15 AM	0	0	0	16	0	26	46	300	0	0	299	17	704
	7:30 AM	0	0	0	20	0	51	66	322	0	0	322	22	803
	7:45 AM	0	0	0	19	0	39	66	409	0	0	375	43	951
	8:00 AM	0	0	0	21	0	66	58	395	0	0	312	31	883
	8:15 AM	0	0	0	25	0	53	65	407	0	0	336	32	918
	8:30 AM	0	0	0	23	0	52	67	392	0	0	357	19	910
Α	8:45 AM	0	0	0	18	0	62	72	430	0	0	309	18	909
₹	VOLUMES	0	0	0	157	0	363	482	2,950	0	0	2,590	193	6,735
	APPROACH %	0%	0%	0%	30%	0%	70%	14%	86%	0%	0%	93%	7%	
	APP/DEPART	0		667	520	/	0	3,432	/	3,107	2,783	/	2,961	0
	BEGIN PEAK HR		7:45 AM											
	VOLUMES	0	0	0	88	0	210	256	1,603	0	0	1,380	125	3,662
	APPROACH %	0%	0%	0%	30%	0%	70%	14%	86%	0%	0%	92%	8%	
	PEAK HR FACTOR		0.000			0.856			0.978			0.900		0.963
	APP/DEPART	0	1	379	298	/	0	1,859	/	1,691	1,505	/	1,592	0
	4:00 PM	0	0	0	47	0	57	39	419	0	0	246	10	818
	4:15 PM	0	0	0	62	0	40	46	443	0	0	263	14	868
	4:30 PM	0	0	0	65	0	44	35	394	0	0	274	13	825
	4:45 PM	0	0	0	69	0	56	41	454	0	1	255	16	892
	5:00 PM	0	0	0	58	0	44	40	429	0	0	271	27	869
	5:15 PM	0	0	0	49	0	51	29	465	0	0	276	23	893
	5:30 PM	0	0	0	51	0	56	30	429	0	0	278	25	869
Σ	5:45 PM	0	0	0	52	0	59	39	414	0	0	263	21	848
I۳	VOLUMES	0	0	0	453	0	407	299	3,447	0	1	2,126	149	6,882
	APPROACH %	0%	0%	0%	53%	0%	47%	8%	92%	0%	0%	93%	7%	
	APP/DEPART	0		435	860	/	0	3,746	/	3,901	2,276	/	2,546	0
	BEGIN PEAK HR	_	4:45 PM	_		_				_	_			
	VOLUMES	0	0	0	227	0	207	140	1,777	0	1	1,080	91	3,523
	APPROACH %	0%	0%	0%	52%	0%	48%	7%	93%	0%	0%	92%	8%	
	PEAK HR FACTOR		0.000			0.868			0.968			0.967		0.986
	APP/DEPART	0		225	434	/	0	1,917	/	2,005	1,172	/	1,293	0



	7:00 AM
	7:15 AM
	7:30 AM
	7:45 AM
Α	8:00 AM
_	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
	4:45 PM
Μ	5:00 PM
Ι-	5:15 PM
	5:30 PM
	5:45 PM
	TOTAL

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
2	2	0	5	9
5	0	5	3	13
10	0	4	3	17
10	0	3	10	23
4	0	5	2	11
12	0	13	12	37
17	0	11	13	41
7	2	7	5	21
67	4	48	53	172
16	0	7	19	42
31	1	14	16	62
30	0	9	20	59
30	2	5	15	52
15	1	8	20	44
45	1	8	15	69
35	0	18	25	78
34	2	12	36	84
236	7	81	166	490

	PEDESTI	RIAN CF	ROSSING	S
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
1	0	0	4	5
4	0	4	3	11
5	0	3	3	11
10	0	3	10	23
3	0	5	2	10
9	0	13	8	30
14	0	10	12	36
5	0	5	5	15
51	0	43	47	141
14	0	6	18	38
28	0	14	14	56
30	0	9	17	56
28	0	4	14	46
13	0	7	19	39
44	0	7	13	64
33	0	17	24	74
33				
33	0	11	33	77

				_
		E CROS		
NS	SS	ES	WS	TOTAL
1	2	0	1	4
1	0	1	0	2
5	0	1	0	6
0	0	0	0	0
1	0	0	0	1
3	0	0	4	7
3	0	1	1	5
2	2	2	0	6
16	4	5	6	31
2	0	1	1	4
3	1	0	2	6
0	0	0	3	3
2	2	1	1	6
2	1	1	1	5
1	1	1	2	5
2	0	1	1	4
1	2	1	3	7
13	7	6	14	40

Turning Movement Count Report AM

Location ID:

North/South: Canfield/Ince Blvd 02/18/15 Date: Culver City, CA City:

East/West: Culver Blvd

	9	Southboun	d		Westbound	d	/	Northboun	d	Eastbound			
	1	2	3	4	5	6	7	8	9	10	11	12	Totals:
Movements:	R	Т	L	R	Т	L	R	Т	L	R	Т	L	TOtals.
7:00	1	0	0	1	55	4	9	3	239	127	125	0	564
7:15	1	0	0	1	48	4	6	1	276	160	136	3	636
7:30	2	0	0	0	68	5	9	2	296	225	157	3	767
7:45	0	0	0	2	62	7	13	2	356	224	159	2	827
8:00	2	0	0	0	56	6	10	6	296	264	180	1	821
8:15	4	0	0	0	58	6	15	1	309	255	166	1	815
8:30	1	0	0	0	64	9	11	4	308	257	175	3	832
8:45	1	0	0	1	92	9	16	6	289	260	177	2	853
9:00	2	0	0	0	74	12	20	4	275	251	169	2	809
9:15	2	0	0	1	73	15	19	2	262	200	173	2	749
9:30	0	0	0	2	72	15	15	1	240	180	167	2	694
9:45	5	0	0	3	72	16	12	1	241	185	147	1	683
												•	-
Total Volume:	21	0	0	11	794	108	155	33	3387	2588	1931	22	9050
Approach %	100%	0%	0%	1%	87%	12%	4%	1%	95%	57%	43%	0%	

Total Volume:	21	0	0	11	794	108	155	33	3387	2588	1931	22	9050
Approach %	100%	0%	0%	1%	87%	12%	4%	1%	95%	57%	43%	0%	

Peak Hr Begin:	8:00												
PHV	8	0	0	1	270	30	52	17	1202	1036	698	7	3321
PHF		0.500			0.738			0.978			0.973		

City Count, LLC. www.citycount.com

Turning Movement Count Report PM

Location ID: 2

North/South: Canfield/Ince Blvd

East/West: Culver Blvd

Date: 02/18/15

City: Culver City, CA

	Southbound		l	Westbound			Northbound			Eastbound			
	1	2	3	4	5	6	7	8	9	10	11	12	Totals:
Movements:	R	T	L	R	T	L	R	T	L	R	T	L	TOtals.
15:00	8	0	0	4	50	9	22	5	216	244	158	6	722
15:15	4	0	0	4	60	7	18	2	194	298	170	2	759
15:30	5	0	0	6	78	10	18	7	180	273	152	3	732
15:45	3	0	0	7	80	10	21	9	205	261	160	6	762
16:00	5	0	0	4	91	12	13	1	197	296	175	10	804
16:15	4	0	0	1	68	8	21	2	206	332	175	5	822
16:30	5	0	0	1	89	5	23	6	193	310	154	5	791
16:45	5	0	0	8	97	12	15	5	213	300	162	9	826
17:00	7	0	0	3	60	8	25	3	218	314	182	6	826
17:15	3	0	0	3	89	6	27	5	230	300	209	5	877
17:30	9	0	0	7	102	12	24	1	202	298	220	6	881
17:45	6	0	0	6	90	9	22	5	242	295	185	6	866
Total Volume:	64	0	0	54	954	108	249	51	2496	3521	2102	69	9668
Approach %	100%	0%	0%	5%	85%	10%	9%	2%	89%	62%	37%	1%	

Peak Hr Begin:	17:00												
PHV	25	0	0	19	341	35	98	14	892	1207	796	23	3450
PHF		0.694			0.816			0.933			0.979		

City Count, LLC. www.citycount.com

Turning Movement Count Report AM

Location ID: 3

North/South: Ince Blvd Date: 02/18/15
East/West: Washington Blvd City: Culver City, CA

Northbound Southbound Westbound Eastbound Totals: Т Т Movements: R Т L R L R L R Т 7:00 7:15 7:30 7:45 8:00 8:15 8:30 8:45 9:00 9:15 9:30 9:45 Total Volume: Approach % 5% 0% 0% 11% 89% 95% 0% 46% 54% 0% 36% 64%

Peak Hr Begin:	7:45												
PHV	5	87	910	1185	1	56	110	160	0	1	3	0	2518
PHF		0.911			0.897			0.833			0.955		

City Count, LLC. www.citycount.com

Turning Movement Count Report PM

Location ID: 3

PHV

PHF

85

0.906

1226

830

0

0.974

North/South: Ince Blvd Date: 02/18/15
East/West: Washington Blvd City: Culver City, CA

	S	outhboun	d	I	Nestbound	1	/	Vorthboun	d		Eastbouna	1]
	1	2	3	4	5	6	7	8	9	10	11	12	Totals:
Movements:	R	T	L	R	T	L	R	T	L	R	Т	L	TOLAIS.
15:00	1	17	225	210	0	20	25	24	0	0	1	0	523
15:15	1	25	259	199	0	16	20	14	0	0	2	0	536
15:30	2	19	281	180	0	16	19	23	0	2	0	0	542
15:45	2	17	253	216	0	14	22	20	0	1	2	0	547
16:00	4	19	280	193	0	24	18	22	0	2	5	0	567
16:15	0	26	337	210	0	27	14	18	0	0	3	0	635
16:30	1	15	299	204	0	25	20	20	0	0	3	0	587
16:45	0	26	316	195	0	28	19	26	0	1	3	0	614
17:00	4	18	274	221	0	13	24	22	0	0	1	0	577
17:15	1	19	282	208	0	25	34	36	0	1	0	0	606
17:30	5	13	290	225	0	26	28	17	0	3	2	0	609
17:45	5	15	261	239	0	32	32	24	0	3	0	0	611
Total Volume:	26	229	3357	2500	0	266	275	266	0	13	22	0	6954
Approach %	1%	6%	93%	90%	0%	10%	51%	49%	0%	37%	63%	0%	
Peak Hr Begin:	16:15												

93

77

86

0.886

0

City Count, LLC. www.citycount.com

1

10

0.688

2413

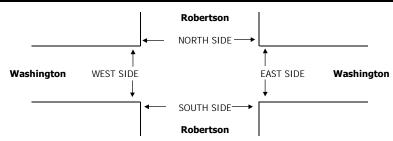
0.950

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: LOCATION: Culver City PROJECT #: SC0715
Thu, Sep 24, 15 NORTH & SOUTH: Robertson LOCATION #: 2
EAST & WEST: Washington CONTROL: SIGNAL

NOTES:	AM	A	
	PM	N	
	MD ◀ W		E▶
	OTHER	S	
	OTHER	▼	

		NO	ORTHBOU	IND	SC	OUTHBOU	ND	F.	ASTBOUN	ID	W	'ESTBOUN	ID.	
		140	Robertson			Robertson	110		Washington		"	Washington		
		NL	NT	NR	SL	ST	SR	EL	FT	ER	WL	WT	WR	TOTAL
	LANES:	1	1	1	1	1	1	1	2	0	1	2	1	TOTAL
г	7:00 AM	12	48	18	11	29	6	10	95	11	11	205	21	477
	7:15 AM	13	105	21	13	28	10	14	106	3	7	228	36	584
	7:30 AM	17	86	17	23	43	12	9	119	14	3	260	18	621
	7:45 AM	13	108	22	31	55	15	6	161	18	9	281	17	736
	8:00 AM	24	78	42	39	49	20	11	185	12	15	254	32	761
	8:15 AM	15	78	36	23	51	21	12	155	13	22	279	36	741
	8:30 AM	18	85	14	21	63	21	7	148	18	16	259	37	707
١	8:45 AM	28	109	31	17	73	23	12	148	21	24	239	36	761
AΜ	VOLUMES	140	697	201	178	391	128	81	1,117	110	107	2,005	233	5,388
	APPROACH %	13%	67%	19%	26%	56%	18%	6%	85%	8%	5%	86%	10%	
	APP/DEPART	1,038	- 1	1,011	697	/	608	1,308	/	1,496	2,345	/	2,273	0
	BEGIN PEAK HR		8:00 AM											
	VOLUMES	85	350	123	100	236	85	42	636	64	77	1,031	141	2,970
	APPROACH %	15%	63%	22%	24%	56%	20%	6%	86%	9%	6%	83%	11%	
	PEAK HR FACTOR		0.830			0.931			0.892			0.927		0.976
	APP/DEPART	558	- /	533	421	/	377	742	/	859	1,249	/	1,201	0
	4:00 PM	8	44	10	31	42	12	36	208	27	19	105	36	578
	4:15 PM	8	54	21	30	44	10	30	212	20	23	124	39	615
	4:30 PM	8	46	17	22	60	17	33	247	33	12	136	44	675
	4:45 PM	5	38	16	30	47	17	33	266	19	22	143	41	677
	5:00 PM	9	48	22	38	64	25	54	270	12	22	184	53	801
	5:15 PM	10	47	20	30	47	14	57	274	15	26	177	48	765
	5:30 PM	10	75	20	27	65	19	47	214	27	18	157	43	722
Σ	5:45 PM	7	62	25	28	57	13	33	260	18	15	127	56	701
4	VOLUMES	65	414	151	236	426	127	323	1,951	171	157	1,153	360	5,534
	APPROACH %	10%	66%	24%	30%	54%	16%	13%	80%	7%	9%	69%	22%	
	APP/DEPART	630		1,097	789	/	754	2,445	/	2,338	1,670	/	1,345	0
	BEGIN PEAK HR		5:00 PM											
	VOLUMES	36	232	87	123	233	71	191	1,018	72	81	645	200	2,989
	APPROACH %	10%	65%	25%	29%	55%	17%	15%	79%	6%	9%	70%	22%	
1	PEAK HR FACTOR		0.845			0.841			0.926			0.894		0.933
	APP/DEPART	355	1	623	427	/	386	1,281	/	1,228	926	/	752	0



	7:00 AM
	7:15 AM
	7:30 AM
l	7:45 AM
¥	8:00 AM
	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
	4:45 PM
Σ	5:00 PM
Ι-	5:15 PM
	5:30 PM
	5:45 PM
	TOTAL

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
5	1	5	5	16
4	1	1	1	7
16	2	1	2	21
5	1	3	3	12
8	5	2	4	19
10	3	2	5	20
7	5	5	4	21
8	10	3	15	36
63	28	22	39	152
3	7	3	6	19
4	2	1	4	11
4	3	1	3	11
6	8	4	5	23
11	5	3	7	26
6	5	12	5	28
7	10	2	6	25
9	13	6	4	32
50	53	32	40	175

	PEDESTI	RIAN CF	ROSSING	iS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
5	0	5	4	14
4	1	1	1	7
7	2	1	2	12
5	0	2	3	10
5	3	1	4	13
9	2	2	4	17
5	4	2	3	14
6	7	3	11	27
46	19	17	32	114
3	5	3	5	16
3	1	1	4	9
4	2	0	3	9
4	7	2	4	17
10	4	2	4	20
~~~~~~~~~	4 5	2 11	4	20 25
10				
10 5	5	11	4	25

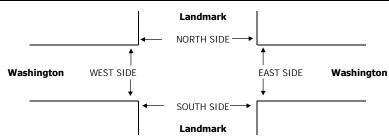
В	ICYCL	E CROS	SSING	5
NS	SS	ES	WS	TOTAL
0	1	0	1	2
0	0	0	0	0
9	0	0	0	9
0	1	1	0	2
3	2	1	0	6
1	1	0	1	3
2	1	3	1	7
2	3	0	4	9
17	9	5	7	38
0	2	0	1	3
0	2	0	1 0	2
1 0 2	1	0 1 2	0 0 1	2
1	1	0 1	0	2
1 0 2	1 1 1	0 1 2	0 0 1	2 2 6
1 0 2	1 1 1	0 1 2 1	0 0 1 3	2 2 6 6
1 0 2 1	1 1 1 1 0	0 1 2 1 1	0 0 1 3	2 2 6 6 3

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: LOCATION: Culver City PROJECT #: SC0715
Thu, Sep 24, 15 NORTH & SOUTH: Landmark LOCATION #: 3
EAST & WEST: Washington CONTROL: SIGNAL

NOTES:	AM	<b>A</b>	
	PM	N	
	MD ◀W		-
	MD 1		⊏▶
	OTHER	S	

		NC	ORTHBOU	IND	SC	OUTHBOU	ND	E.A	ASTBOUN	ID	W	ESTBOUN	ND.	
			Landmark			Landmark			Washington			Washington		
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	1	X	1	Χ	X	Χ	X	2	0	1	2	X	
	7:00 AM	5	0	4	0	0	0	0	116	12	9	260	0	406
	7:15 AM	0	0	4	0	0	0	0	100	9	3	229	0	345
	7:30 AM	7	0	6	0	0	0	0	146	26	13	295	0	493
	7:45 AM	13	0	9	0	0	0	0	178	30	16	324	0	570
	8:00 AM	11	0	14	0	0	0	0	234	28	13	256	0	556
	8:15 AM	19	0	15	0	0	0	0	199	21	23	307	0	584
	8:30 AM	10	0	9	0	0	0	0	185	13	10	312	0	539
ΑM	8:45 AM	3	0	3	0	0	0	0	165	8	10	274	0	463
⋖	VOLUMES	68	0	64	0	0	0	0	1,323	147	97	2,257	0	3,956
	APPROACH %	52%	0%	48%	0%	0%	0%	0%	90%	10%	4%	96%	0%	
	APP/DEPART	132	1	0	0	/	243	1,470	/	1,388	2,354	/	2,325	0
	BEGIN PEAK HR		7:45 AM											
	VOLUMES	53	0	47	0	0	0	0	796	92	62	1,199	0	2,249
	APPROACH %	53%	0%	47%	0%	0%	0%	0%	90%	10%	5%	95%	0%	
	PEAK HR FACTOR		0.735			0.000			0.847			0.927		0.963
	APP/DEPART	100		0	0	/	154	888	/	843	1,261	/	1,252	0
	4:00 PM	19	0	19	0	0	0	0	235	8	11	136	0	428
	4:15 PM	9	0	18	0	0	0	0	251	3	7	146	0	434
	4:30 PM	18	0	16	0	0	0	0	269	7	4	162	0	476
	4:45 PM	16	0	11	0	0	0	0	308	5	2	181	0	523
	5:00 PM	11	0	11	0	0	0	0	327	2	3	251	0	605
	5:15 PM	6	0	4	0	0	0	0	328	2	2	242	0	584
	5:30 PM	1	0	11	0	0	0	0	267	1	0	229	0	509
Σ	5:45 PM	5	0	7	0	0	0	0	316	1	1	204	0	534
I٩	VOLUMES	85	0	97	0	0	0	0	2,301	29	30	1,551	0	4,093
	APPROACH %	47%	0%	53%	0%	0%	0%	0%	99%	1%	2%	98%	0%	
	APP/DEPART	182		0	0	/	54	2,330	/	2,403	1,581	/	1,636	0
	BEGIN PEAK HR		5:00 PM		_	_	_	_			_		_	
	VOLUMES	23	0	33	0	0	0	0	1,238	6	6	926	0	2,232
	APPROACH %	41%	0%	59%	0%	0%	0%	0%	100%	0%	1%	99%	0%	
	PEAK HR FACTOR		0.636			0.000			0.942	4 075	000	0.917	0.10	0.922
	APP/DEPART	56		0	0	/	8	1,244	/	1,275	932	/	949	0



	7:00 AM
	7:15 AM
	7:30 AM
	7:45 AM
¥	8:00 AM
`	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
	4:45 PM
Σ	4:45 PM 5:00 PM
PM	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
Δd	5:00 PM
PM	5:00 PM 5:15 PM

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
0	1	9	1	11
0	1	3	0	4
3	1	0	0	4
1	1	2	2	6
0	7	3	0	10
0	1	2	0	3
1	1	1	0	3
1	4	4	1	10
6	17	24	4	51
0	3	4	3	10
0	0	1	0	1
0	1	3	0	4
0	2	0	0	2
1	1	5	0	7
2	4	3	0	9
0	3	0	0	3
1	2	2	0	5
4	16	18	3	41

	PEDESTI	RIAN CR	ROSSING	S
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
0	0	9	1	10
0	0	3	0	3
0	1	0	0	1
0	0	2	2	4
0	5	3	0	8
0	0	2	0	2
0	1	1	0	2
0	1	4	1	6
0	8	24	4	36
0	1	4	3	8
		1		1
0	0		0	'
0	0	2	0	2
				-
0	0	2	0	2
0	0	2	0	2
0	0 0 0	2 0 5	0 0	2 0 5
0 0 0	0 0 0	2 0 5	0 0 0	2 0 5 3

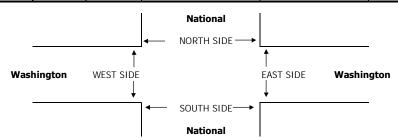
В	ICYCL	E CRO	SSING	S
NS	SS	ES	WS	TOTAL
0	1	0	0	1
0	1	0	0	1
3	0	0	0	3
1	1	0	0	2
0	2	0	0	2
0	1	0	0	1
1	0	0	0	1
1	3	0	0	4
6	9	0	0	15
0	2	0	0	2
0	0	0	0	0
0	1	1	0	2
0	2	0	0	2
1	1	0	0	2
2	4	0	0	6
0	2	0	0	2
1	2	0	0	3
	14	1	0	19

## PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: Thu, Sep 24, 15 NORTH & SOUTH: National LOCATION #: 4
EAST & WEST: Washington CONTROL: SIGNAL

NOTES:	AM		<b>A</b>	
	PM		N	
	MD	<b>■</b> W	,	E▶
	MD	- VV		
	OTHER	7 11	S	

		NC	ORTHBOU	ND	SC	OUTHBOU	ND	E/	ASTBOUN	ID	W	ESTBOUN	ND.	
			National			National			Washington			Washington		
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	2	2	0	2	2	0	1	2	1	1	2.5	0.5	
Г	7:00 AM	56	212	7	11	85	10	10	78	18	12	180	38	717
	7:15 AM	46	238	6	12	86	13	9	100	19	9	228	66	832
	7:30 AM	47	181	7	18	119	13	16	133	21	39	311	50	955
	7:45 AM	55	224	8	20	181	22	14	167	26	50	353	49	1,169
	8:00 AM	45	132	11	18	191	20	7	138	51	35	266	44	958
	8:15 AM	62	189	10	25	186	26	23	148	41	36	271	36	1,053
	8:30 AM	25	147	6	22	199	17	12	130	38	23	234	42	895
ΑM	8:45 AM	31	166	6	16	192	14	9	140	39	25	353	56	1,047
۱₹	VOLUMES	367	1,489	61	142	1,239	135	100	1,034	253	229	2,196	381	7,626
	APPROACH %	19%	78%	3%	9%	82%	9%	7%	75%	18%	8%	78%	14%	
	APP/DEPART	1,917	- /	1,970	1,516	/	1,721	1,387	/	1,236	2,806	/	2,699	0
	BEGIN PEAK HR		7:30 AM											
	VOLUMES	209	726	36	81	677	81	60	586	139	160	1,201	179	4,135
	APPROACH %	22%	75%	4%	10%	81%	10%	8%	75%	18%	10%	78%	12%	
	PEAK HR FACTOR		0.846			0.885			0.926			0.852		0.884
	APP/DEPART	971		965	839	/	976	785	/	702	1,540	/	1,492	0
	4:00 PM	36	132	19	64	156	12	13	185	59	17	148	18	859
	4:15 PM	33	154	27	48	217	14	6	183	59	16	140	20	917
	4:30 PM	40	147	20	47	192	6	12	225	42	20	133	20	904
	4:45 PM	41	149	23	68	228	10	13	257	48	26	141	31	1,035
	5:00 PM	51	170	19	54	225	13	24	275	60	35	217	31	1,174
	5:15 PM	39	164	18	52	259	6	20	277	45	30	199	29	1,138
	5:30 PM	65	199	18	56	234	17	17	216	51	38	193	24	1,128
Δ	5:45 PM	52	200	24	76	210	15	23	261	42	22	166	19	1,110
I۵	VOLUMES	357	1,315	168	465	1,721	93	128	1,879	406	204	1,337	192	8,265
	APPROACH %	19%	71%	9%	20%	76%	4%	5%	78%	17%	12%	77%	11%	
	APP/DEPART	1,840		1,635	2,279	/	2,330	2,413	/	2,513	1,733	/	1,787	0
	BEGIN PEAK HR		5:00 PM											
	VOLUMES	207	733	79	238	928	51	84	1,029	198	125	775	103	4,550
	APPROACH %	20%	72%	8%	20%	76%	4%	6%	78%	15%	12%	77%	10%	
1	PEAK HR FACTOR		0.903			0.960			0.913			0.886		0.969
	APP/DEPART	1,019		920	1,217	/	1,251	1,311	/	1,346	1,003	/	1,033	0



	7:00 AM
	7:15 AM
	7:30 AM
_	7:45 AM
AM	8:00 AM
,	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
_	4:45 PM
ΡM	5:00 PM
	5:15 PM
	5:30 PM
	5:45 PM
	TOTAL

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
2	0	2	8	12
0	4	0	10	14
3	2	0	9	14
6	5	0	11	22
0	2	2	13	17
2	0	0	5	7
0	1	1	5	7
10	0	0	6	16
23	14	5	67	109
1	4	0	26	31
3	2	0	9	14
1	0	0	9	10
5	0	0	7	12
3	1	0	13	17
5	2	1	17	25
5	0	0	8	13
1	0	1	13	15
24	9	2	102	137

	PEDESTRIAN CROSSINGS									
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL						
2	0	0	6	8						
0	1	0	2	3						
2	2	0	8	12						
6	2	0	7	15						
0	2	2	13	17						
1	0	0	3	4						
0	0	1	4	5						
10	0	0	4	14						
21	7	3	47	78						
1	4	0	26	31						
2	1	0	7	10						
1	0	0	6	7						
5	0	0	7	12						
1	0	0	11	12						
2	0	1	12	15						
5	0	0	6	11						
1	0	1	11	13						
18	5	2	86	111						

BICYCLE CROSSINGS										
NS	SS	ES ES	WS	TOTAL						
0	0	2	2	4						
0	3	0	8	11						
1	0	0	1	2						
0	3	0	4	7						
0	0	0	0	0						
1	0	0	2	3						
0	1	0	1	2						
0	0	0	2	2						
2	7	2	20	31						
_	_	0	0	0						
0	0	U		U						
1	1	0	2	4						
1	1	0	2	4						
1 0 0	1 0	0	2	4 3 0 5						
1 0 0	1 0 0	0 0 0	2 3 0	4 3 0 5 10						
1 0 0	1 0 0	0 0 0 0	2 3 0 2 5 2	4 3 0 5 10 2						
1 0 0 2 3	1 0 0 1 2	0 0 0 0	2 3 0 2 5	4 3 0 5 10						

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

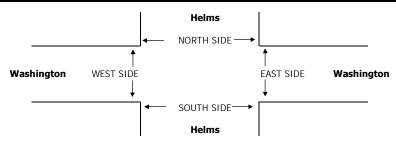
 DATE:
 LOCATION:
 Culver City
 PROJECT #:
 SC0715

 Thu, Sep 24, 15
 NORTH & SOUTH:
 Helms
 LOCATION #:
 5

 EAST & WEST:
 Washington
 CONTROL:
 SIGNAL

NOTES:	AM	
	PM PM	
	MD ◀ W	E►
	OTHER	

		N(	ORTHBOU	IND	S	OUTHBOU	ND	F.A	ASTBOUN	ID	W	FSTBOUN	ID.	
			Helms			Helms			Washington		''	Washington		
		NL	NT	NR	SL	ST	SR	EL	FT	ER	WL	WT	WR	TOTAL
	LANES:	0	X	0	X	X	X	X	2	0	1	2	X	TOTAL
Г	7:00 AM	5	0	1	0	0	0	0	116	0	3	290	0	415
	7:15 AM	14	0	2	0	0	0	0	117	1	0	313	0	447
	7:30 AM	11	0	1	0	0	0	0	124	1	1	353	0	491
	7:45 AM	28	0	1	0	0	0	0	163	8	3	373	0	576
	8:00 AM	23	0	3	0	0	0	0	181	6	4	327	0	544
	8:15 AM	31	0	4	0	0	0	0	196	4	2	346	0	583
	8:30 AM	17	0	6	0	0	0	0	176	5	2	344	0	550
15	8:45 AM	17	0	4	0	0	0	0	154	4	2	333	0	514
AΜ	VOLUMES	146	0	22	0	0	0	0	1,227	29	17	2,679	0	4,120
	APPROACH %	87%	0%	13%	0%	0%	0%	0%	98%	2%	1%	99%	0%	
	APP/DEPART	168	- 1	0	0	/	46	1,256	/	1,249	2,696	/	2,825	0
	BEGIN PEAK HR		7:45 AM											
	VOLUMES	99	0	14	0	0	0	0	716	23	11	1,390	0	2,253
	APPROACH %	88%	0%	12%	0%	0%	0%	0%	97%	3%	1%	99%	0%	
	PEAK HR FACTOR		0.807			0.000			0.924			0.932		0.966
	APP/DEPART	113	- /	0	0	/	34	739	/	730	1,401	/	1,489	0
	4:00 PM	13	0	3	0	0	0	0	267	5	2	184	0	474
	4:15 PM	13	0	2	0	0	0	0	273	8	5	210	0	511
	4:30 PM	9	0	7	0	0	0	0	323	10	3	188	0	540
	4:45 PM	15	0	1	0	0	0	0	357	15	5	208	0	601
	5:00 PM	19	0	0	0	0	0	0	282	20	4	250	0	575
	5:15 PM	17	0	2	0	0	0	0	307	21	5	243	0	595
	5:30 PM	18	0	2	0	0	0	0	310	14	8	189	0	541
Σ	5:45 PM	10	0	3	0	0	0	1	327	8	2	194	0	545
4	VOLUMES	114	0	20	0	0	0	1	2,446	101	34	1,666	0	4,382
	APPROACH %	85%	0%	15%	0%	0%	0%	0%	96%	4%	2%	98%	0%	
	APP/DEPART	134		0	0	/	132	2,548	/	2,469	1,700	/	1,781	0
	BEGIN PEAK HR		4:45 PM											
	VOLUMES	69	0	5	0	0	0	0	1,256	70	22	890	0	2,312
	APPROACH %	93%	0%	7%	0%	0%	0%	0%	95%	5%	2%	98%	0%	
1	PEAK HR FACTOR		0.925			0.000			0.891			0.898		0.962
L	APP/DEPART	74	1	0	0	/	90	1,326	/	1,263	912	/	959	0



	7:00 AM
	7:15 AM
	7:30 AM
	7:45 AM
Ψ	8:00 AM
1	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
	4:45 PM
Σ	5:00 PM
Ι-	5:15 PM
	5:30 PM
	5:45 PM
	TOTAL

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
0	1	0	1	2
0	3	3	3	9
2	4	1	1	8
1	4	2	1	8
2	1	5	3	11
1	1	3	5	10
1	3	9	5	18
0	1	3	2	6
7	18	26	21	72
2	3	9	3	17
1	3	5	1	10
1	0	3	4	8
0	1	8	3	12
1	0	1	8	10
1	4	6	2	13
0	4	6	6	16
1	1	1	1	4
7	16	39	28	90

	PEDESTI	RIAN CR	ROSSING	S
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
0	1	0	1	2
0	3	3	3	9
0	4	1	1	6
0	3	2	1	6
0	1	5	3	9
0	1	3	5	9
0	3	7	5	15
0	0	3	2	5
0	16	24	21	61
0	2	8	3	13
0	2	5	1	8
0	0	2	3	5
0	0	8	2	10
0	0	1	8	9
0	0	6	2	8
0	3	5	6	14
0	0	1	1	2
0	7	36	26	69

В	ICYCL	E CROS	SSING	S
NS	SS	ES	WS	TOTAL
0	0	0	0	0
0	0	0	0	0
2	0	0	0	2
1	1	0	0	2
2	0	0	0	2
1	0	0	0	1
1	0	2	0	3
0	1	0	0	1
7	2	2	0	11
2	1	1	0	4
1	1	0	0	2
1	0	1	1	3
1	0 1	0	1	3 2
************				
0	1	0	1	2
0	1 0	0	1 0	2
1	1 0 4	0 0 0	1 0 0	2 1 5

PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: Thu, Sep 24, 15

NOTES:

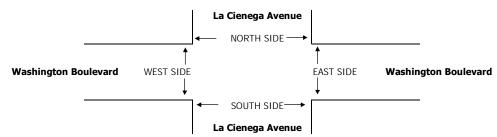
LOCATION: NORTH & SOUTH: EAST & WEST: Culver City La Cienega Avenue Washington Boulevard PROJECT #: LOCATION #: CONTROL:

AM N N N OTHER S

SC0715

6 SIGNAL

											UTHER		•	
		NO	ORTHBOL	IND	SC	OUTHBOU	ND	E/	ASTBOUN	ID	W	'ESTBOUN	ND	
		Li	a Cienega Aver	nue	La	Cienega Avenu	e	Was	hington Boule	vard	Wa	ashington Boul	evard	
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	0	1	0	0	1	0	0	2	0	0	2	0	
	7:00 AM	1	0	4	5	0	17	5	111	2	3	284	2	434
	7:15 AM	1	0	1	2	0	13	1	131	2	3	332	2	488
	7:30 AM	3	0	2	6	0	32	2	131	2	3	355	2	538
	7:45 AM	10	0	3	18	0	34	5	158	6	3	324	6	567
	8:00 AM	18	0	5	35	0	28	3	201	1	4	313	12	620
	8:15 AM	35	0	11	14	0	39	5	173	1	4	346	8	636
	8:30 AM	12	0	3	7	0	33	2	150	5	1	315	1	529
Α	8:45 AM	4	0	1	9	0	32	5	150	3	1	339	7	551
⋖	VOLUMES	84	0	30	96	0	228	28	1,205	22	22	2,608	40	4,363
	APPROACH %	74%	0%	26%	30%	0%	70%	2%	96%	2%	1%	98%	1%	
	APP/DEPART	114	1	67	324	/	43	1,255	/	1,332	2,670	/	2,921	0
	BEGIN PEAK HR		7:30 AM											
	VOLUMES	66	0	21	73	0	133	15	663	10	14	1,338	28	2,361
	APPROACH %	76%	0%	24%	35%	0%	65%	2%	96%	1%	1%	97%	2%	
	PEAK HR FACTOR		0.473			0.817			0.839			0.958		0.928
	APP/DEPART	87		42	206	/	24	688	/	757	1,380	/	1,538	0
	4:00 PM	10	0	3	16	0	13	6	291	15	1	168	2	525
	4:15 PM	17	0	3	12	0	22	4	257	11	1	148	4	479
	4:30 PM	8	0	9	23	0	18	5	339	10	6	154	7	579
	4:45 PM	26	0	2	16	0	26	2	289	9	0	185	12	567
	5:00 PM	37	0	5	30	0	29	6	276	0	2	200	5	590
	5:15 PM	5	0	5	23	0	18	8	283	1	2	165	7	517
	5:30 PM	5	0	2	13	0	16	4	303	7	3	149	1	503
Σ	5:45 PM	5	0	5	24	0	24	5	310	3	2	155	6	539
۵	VOLUMES	113	0	34	157	0	166	40	2,348	56	17	1,324	44	4,299
	APPROACH %	77%	0%	23%	49%	0%	51%	2%	96%	2%	1%	96%	3%	
	APP/DEPART	147		83	323	/	72	2,444	/	2,540	1,385	/	1,604	0
	BEGIN PEAK HR		4:30 PM											
	VOLUMES	76	0	21	92	0	91	21	1,187	20	10	704	31	2,253
	APPROACH %	78%	0%	22%	50%	0%	50%	2%	97%	2%	1%	94%	4%	
1	PEAK HR FACTOR		0.577			0.775			0.867			0.900		0.955
	APP/DEPART	97		51	183	/	29	1,228	/	1,301	745	/	872	0



	7:00 AM
	7:15 AM
	7:30 AM
	7:45 AM
Ψ	8:00 AM
	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
	4:45 PM
Μ	5:00 PM
_	5:15 PM
	5:30 PM
	5:45 PM
	TOTAL

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
0	0	2	0	2
3	1	2	1	7
3	0	0	0	3
1	1	0	0	2
0	0	0	0	0
5	1	1	0	7
4	1	3	0	8
0	0	1	0	1
16	4	9	1	30
1	2	7	0	10
7	1	8	0	16
4	0	7	0	11
3	1	6	0	10
4	0	3	0	7
4	1	3	0	8
4	0	5	0	9
6	5	12	1	24
		51		95

	PEDESTI	RIAN CR	OSSING	S
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
0	0	1	0	1
1	0	2	0	3
1	0	0	0	1
1	0	0	0	1
0	0	0	0	0
3	1	1	0	5
4	0	2	0	6
0	0	1	0	1
10	1	7	0	18
1	2	6	0	9
4	0	8	0	12
4	0	6	0	10
2	0	6	0	8
3	0	3	0	6
3	0	2	0	5
3	0	5	0	8
4	0	9	0	13
24	2	45	0	71

В	ICYCL	E CRO	SSING	5
NS	SS	ES	WS	TOTAL
0	0	1	0	1
2	1	0	1	4
2	0	0	0	2
0	1	0	0	1
0	0	0	0	0
2	0	0	0	2
0	1	1	0	2
0	0	0	0	0
6	3	2	1	12
0	0	1	0	1
3	1	0	0	4
0	0	1	0	1
1	1	0	0	2
1	0	0	0	1
	1	1	0	3
1				
1	0	0	0	1
		0	0	1 11

Project ID: 16-5759-004 Day: Wednesday

City: Culver City Date: 11/9/2016

-						AN	/I						
NS/EW Streets:	La	Cienega Blv	d	La	Cienega Blv	d	Wa	shington Bl	vd .	Was	shington Blv	/d	
	N	ORTHBOUN	D	SC	OUTHBOUN	D	E	ASTBOUN	)	V	VESTBOUNI	)	
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	1	3	0	1	3	0	1	2	1	1	2	1	
7:00 AM	36	388	2	23	206	4	5	98	7	15	334	91	1209
7:15 AM	91	385	2	13	253	7	12	122	7	8	340	83	1323
7:30 AM	99	416	3	26	229	12	10	146	24	18	332	83	1398
7:45 AM	95	381	2	21	212	10	13	172	19	11	306	65	1307
8:00 AM	73	412	7	39	283	9	15	184	28	14	331	80	1475
8:15 AM	71	357	9	39	273	17	17	214	33	25	332	92	1479
8:30 AM	75	392	7	28	233	10	14	202	35	13	331	75	1415
8:45 AM	91	353	6	27	253	13	11	160	26	17	320	73	1350
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	631	3084	38	216	1942	82	97	1298	179	121	2626	642	10956
APPROACH %'s:	16.81%	82.17%	1.01%	9.64%	86.70%	3.66%	6.16%	82.47%	11.37%	3.57%	77.49%	18.94%	
PEAK HR START TIME :	800	AM											TOTAL
PEAK HR VOL:	310	1514	29	133	1042	49	57	760	122	69	1314	320	5719
PEAK HR FACTOR:		0.942			0.924			0.889			0.948		0.967

# Intersection Turning Movement Prepared by:

## National Data & Surveying Services

Project ID: 16-5759-004 Day: Wednesday City: Culver City Date: 11/9/2016

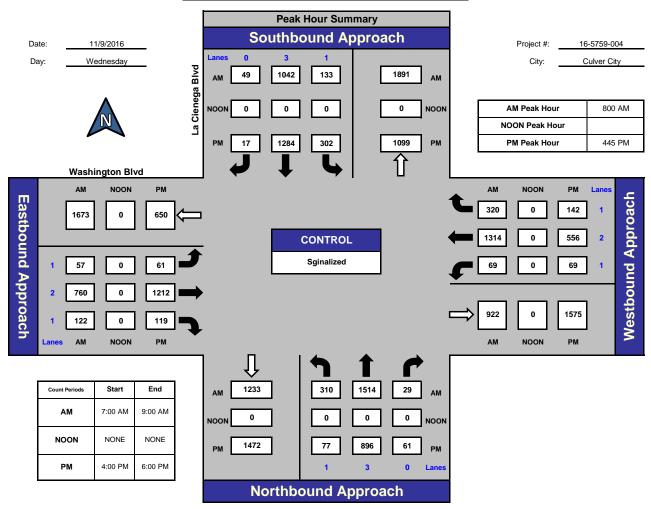
	PM												
NS/EW Streets:	La	Cienega Blv	⁄d	La	Cienega Blv	d	Wa	shington Blv	/d	Was	shington Blv	/d	
	N	ORTHBOUN	ID	S	OUTHBOUN	D	[	EASTBOUND	)	V	VESTBOUNI	)	
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	1	3	0	1	3	0	1	2	1	1	2	1	
4:00 PM	26	205	12	66	308	9	15	299	29	18	128	26	1141
4:15 PM	20	177	11	63	284	3	12	301	39	22	106	33	1071
4:30 PM	14	230	23	82	308	7	16	304	28	23	118	30	1183
4:45 PM	22	226	18	74	328	4	17	292	31	12	125	35	1184
5:00 PM	25	221	16	73	321	5	24	310	33	19	127	33	1207
5:15 PM	10	221	15	81	348	3	10	293	25	19	151	44	1220
5:30 PM	20	228	12	74	287	5	10	317	30	19	153	30	1185
5:45 PM	10	202	16	63	321	9	11	321	22	18	122	33	1148
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	147	1710	123	576	2505	45	115	2437	237	150	1030	264	9339
APPROACH %'s :	7.42%	86.36%	6.21%	18.43%	80.13%	1.44%	4.12%	87.38%	8.50%	10.39%	71.33%	18.28%	
PEAK HR START TIME :	445	PM											TOTAL
PEAK HR VOL:	77	896	61	302	1284	17	61	1212	119	69	556	142	4796
PEAK HR FACTOR:		0.972			0.928			0.948			0.896		0.983

## ITM Peak Hour Summary

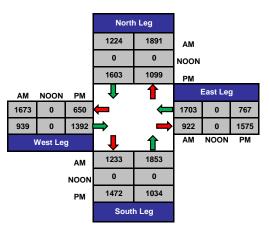


National Data & Surveying Services

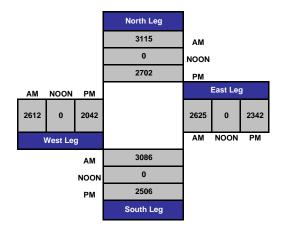
## La Cienega Blvd and Washington Blvd , Culver City



## **Total Ins & Outs**



## **Total Volume Per Leg**

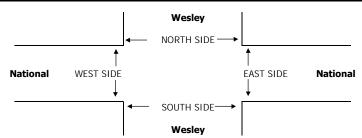


## PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: Thu, Sep 24, 15 LOCATION: Culver City PROJECT #: SC0715
NORTH & SOUTH: Wesley LOCATION #: 7
EAST & WEST: National CONTROL: SIGNAL

ı	NOTES:	AM		<b>A</b>	
ı				N	
			<b>⋖</b> W		E►
ı				S	
ı		OTHER		▼	

		NC	RTHBOU	IND	SC	OUTHBOU	ND	E.A	ASTBOUN	ID	W	'ESTBOUN	ID.	
			Wesley			Wesley			National			National		
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	0	X	0	X	X	X	X	2	1	1	2	X	
	7:00 AM	1	0	1	0	0	0	0	123	2	1	307	0	435
	7:15 AM	6	0	4	0	0	0	0	127	8	4	283	0	432
	7:30 AM	10	0	6	0	0	0	0	158	14	5	268	0	461
	7:45 AM	22	0	13	0	0	0	0	195	47	7	204	0	488
	8:00 AM	56	0	34	0	0	0	0	179	96	4	167	0	536
	8:15 AM	55	0	25	0	0	0	0	190	80	6	186	0	542
	8:30 AM	21	0	13	0	0	0	0	215	30	3	144	0	426
Σ	8:45 AM	6	0	1	0	0	0	0	231	15	3	159	0	415
⋖	8:45 AM VOLUMES	177	0	97	0	0	0	0	1,418	292	33	1,718	0	3,735
	APPROACH %	65%	0%	35%	0%	0%	0%	0%	83%	17%	2%	98%	0%	
	APP/DEPART	274		0	0	/	325	1,710	/	1,515	1,751	/	1,895	0
	BEGIN PEAK HR		7:30 AM											
	VOLUMES	143	0	78	0	0	0	0	722	237	22	825	0	2,027
	APPROACH %	65%	0%	35%	0%	0%	0%	0%	75%	25%	3%	97%	0%	
	PEAK HR FACTOR		0.614			0.000			0.872			0.776		0.935
	APP/DEPART	221		0	0	/	259	959	/	800	847	/	968	0
	4:00 PM	18	0	4	0	0	0	0	210	24	4	163	0	423
	4:15 PM	31	0	5	0	0	0	0	239	30	4	182	0	491
	4:30 PM	36	0	16	0	0	0	0	254	26	3	185	0	520
	4:45 PM	26	0	4	0	0	0	0	275	15	1	196	0	517
	5:00 PM	22	0	5	0	0	0	0	330	9	2	228	0	596
	5:15 PM	9	0	4	0	0	0	0	315	15	5	214	0	562
	5:30 PM	11	0	5	0	0	0	0	257	56	3	230	0	562
Σ	5:45 PM	30	0	11	0	0	0	0	247	12	4	249	0	553
•	VOLUMES	183	0	54	0	0	0	0	2,127	187	26	1,647	0	4,230
	APPROACH %	77%	0%	23%	0%	0%	0%	0%	92%	8%	2%	98%	0%	
	APP/DEPART	237		0	0	/	213	2,320	/	2,181	1,673	/	1,836	0
	BEGIN PEAK HR		5:00 PM											
	VOLUMES	72	0	25	0	0	0	0	1,149	92	14	921	0	2,274
	APPROACH %	74%	0%	26%	0%	0%	0%	0%	93%	7%	1%	99%	0%	
	PEAK HR FACTOR		0.591			0.000			0.916			0.924		0.954
ı	APP/DEPART	97	1	0	0	/	106	1,242	/	1,174	935	/	994	0



	7:00 AM
	7:15 AM
	7:30 AM
l_	7:45 AM
Ψ	8:00 AM
-	8:15 AM
	8:30 AM
	8:45 AM
	TOTAL
	4:00 PM
	4:15 PM
	4:30 PM
l_	4:45 PM
Μ	5:00 PM
	5:15 PM
	5:30 PM
	5:45 PM
	TOTAL

PED	ESTRIA	N + BIKE	CROSSI	NGS
N SIDE	S SIDE	E SIDE	W SIDE	TOTAL
1	1	2	0	4
0	4	0	0	4
0	6	4	0	10
0	2	4	1	7
0	4	4	0	8
0	7	6	0	13
0	6	6	1	13
0	3	7	0	10
1	33	33	2	69
0	4	9	0	13
1	18	13	0	32
0	6	1	0	7
0	5	5	0	10
0	18	22	0	40
0	2	8	0	10
0	6	12	0	18
1	9	3	0	13
2	68	73	0	143

PEDESTRIAN CROSSINGS													
N SIDE S SIDE E SIDE W SIDE TOTAL													
0	1	1	0	2									
0	3	0	0	3									
0	5	4	0	9									
0	2	3	1	6									
0	4	1	0	5									
0	5	2	0	7									
0	4	1	0	5									
0	1	2	0	3									
0	25	14	1	40									
0	2	8	0	10									
0	14	10	0	24									
0	4	0	0	4									
0	4	3	0	7									
0	16	20	0	36									
0	1	1	0	2									
0	5	10	0	15									
0	4	1	0	5									
0	50	53	0	103									

BICYCLE CROSSINGS													
NS	SS	ES	WS	TOTAL									
1	0	1	0	2									
0	1	0	0	1									
0	1	0	0	1									
0	0	1	0	1									
0	0	3	0	3									
0	2	4	0	6									
0	2	5	1	8									
0	2	5	0	7									
1	8	19	1	29									
0	2	1	0	3									
1	4	3	0	8									
<u> </u>	2	1	0	3									
0	2		U	J									
0	1	2	0	3									
0	1	2	0	3									
0	1 2	2	0	3									
0 0 0	1 2 1	2 2 7	0 0 0	3 4 8									

Project ID: 16-5759-005 Day: Wednesday

Date: 11/9/2016

City: Culver City

_	AIVI										•		
NS/EW Streets:	Н	ayden Ave		1	Hayden Ave	)	N	ational Blvd		N	ational Blvd		
•	NO	ORTHBOUN	ID	S	OUTHBOU	ND	E	ASTBOUN	)	V	VESTBOUND	)	<u> </u>
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	1.5	0	0.5	0	0	0	0	2	1	1	2	0	
7:00 AM	71	0	3	0	0	0	0	75	30	28	251	0	458
7:15 AM	55	0	5	0	0	0	0	109	24	43	221	0	457
7:30 AM	51	0	4	0	0	0	0	111	25	30	146	0	367
7:45 AM	75	0	14	0	0	0	0	132	50	41	177	0	489
8:00 AM	87	0	11	0	0	0	0	143	49	44	134	0	468
8:15 AM	53	0	8	0	0	0	0	170	43	46	149	0	469
8:30 AM	78	0	10	0	0	0	1	152	69	43	156	0	509
8:45 AM	70	0	14	0	0	0	0	175	93	52	163	0	567
T	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	540	0	69	0	0	0	1	1067	383	327	1397	0	3784
APPROACH %'s:	88.67%	0.00%	11.33%	#DIV/0!	#DIV/0!	#DIV/0!	0.07%	73.54%	26.40%	18.97%	81.03%	0.00%	l I
PEAK HR START TIME :	800 <i>F</i>	MA											TOTAL
PEAK HR VOL:	288	0	43	0	0	0	1	640	254	185	602	0	2013
PEAK HR FACTOR:	0.844		0.000			0.835					0.888		

## Intersection Turning Movement

## National Data & Surveying Services

Project ID: 16-5759-005 Day: Wednesday

Date: 11/9/2016

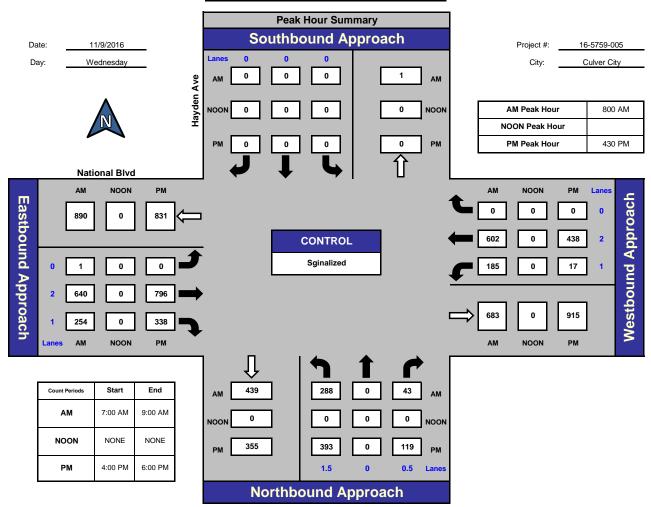
City: Culver City РМ NS/EW Streets Hayden Ave Hayden Ave National Blvd National Blvd NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND NLNT NR SL  $\mathsf{ST}$  $\mathsf{SR}$ EL ΕT ER WL  $\mathsf{WT}$ WR TOTAL LANES: 1.5 0.5 1 107 4:00 PM 110 188 73 497 14 0 0 0 0 0 5 5 3 0 0 0 0 0 16 4:15 PM 4:30 PM 82 98 64 78 79 0 225 79 471 26 0 0 0 231 106 0 542 4:45 PM 91 27 0 0 0 0 207 108 0 517 91 5:00 PM 102 0 37 0 0 0 197 118 0 549 5:15 PM 102 0 29 0 0 0 0 161 90 106 0 493 5:30 PM 122 0 17 0 0 0 0 123 95 6 140 0 503 5:45 PM 87 0 13 0 0 0 132 123 4 101 0 461 SL WL WT NL NT NR ST SR EL ΕT ER WR TOTAL TOTAL VOLUMES 794 179 1464 693 865 4033 APPROACH %'s 81.60% 0.00% 18.40% #DIV/0! #DIV/0! #DIV/0! 0.05% 67.84% 32.11% 4.10% 95.90% 0.00% PEAK HR START TIME 430 PM TOTAL PEAK HR VOL 393 0 119 0 0 0 0 796 338 17 438 0 2101 PEAK HR FACTOR 0.921 0.000 0.917 0.932 0.957

## ITM Peak Hour Summary

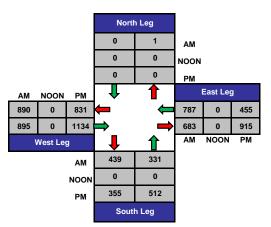


National Data & Surveying Services

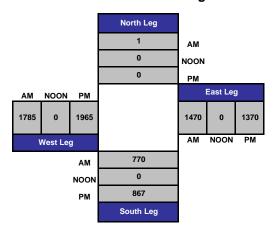
## Hayden Ave and National Blvd , Culver City



## **Total Ins & Outs**



## **Total Volume Per Leg**



Project ID: 16-5759-002 Day: Wednesday

Date: 11/9/2016

City: Los Angeles

-	AM												
NS/EW Streets:	Je	fferson Blvd		Je	fferson Blvd	i	Na	ational Blvd		N	ational Blvd		
•	N	ORTHBOUN	D	SC	OUTHBOUN	D	Е	ASTBOUND	)	V	VESTBOUNI	D	
LANES:	NL 1	NT 3	NR 0	SL 1	ST	SR 1	EL 1.5	ET 0.5	ER 1	WL 0.5	WT 0.5	WR 1	TOTAL
LANES.	•	3	U		·		1.5	0.5		0.5	0.5		
7:00 AM	123	156	2	0	143	151	26	0	45	1	4	0	651
7:15 AM	115	158	2	4	183	158	52	0	48	0	2	1	723
7:30 AM	93	160	2	3	188	127	31	2	58	0	3	2	669
7:45 AM	61	132	3	2	264	173	63	0	46	0	1	0	745
8:00 AM	75	182	1	2	212	147	62	1	57	1	3	0	743
8:15 AM	81	221	1	3	196	122	81	2	67	0	1	1	776
8:30 AM	80	189	3	2	208	147	61	4	72	0	3	2	771
8:45 AM	83	164	10	8	218	181	66	4	78	2	5	2	821
9:00 AM	82	138	10	5	234	224	61	13	67	0	1	3	838
9:15 AM	72	129	6	10	180	200	47	9	71	3	2	0	729
9:30 AM	89	139	3	15	174	202	55	14	58	0	1	1	751
9:45 AM	107	122	1	4	138	172	43	5	69	1	5	0	667
T	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	1061	1890	44	58	2338	2004	648	54	736	8	31	12	8884
APPROACH %'s:	35.43%	63.11%	1.47%	1.32%	53.14%	45.55%	45.06%	3.76%	51.18%	15.69%	60.78%	23.53%	
PEAK HR START TIME :	815 /	AM											TOTAL
PEAK HR VOL:	326	712	24	18	856	674	269	23	284	2	10	8	3206
PEAK HR FACTOR:		0.876			0.836			0.960			0.556		0.956

# Intersection Turning Movement Prepared by:

## National Data & Surveying Services

Project ID: 16-5759-002 Day: Wednesday City: Los Angeles Date: 11/9/2016

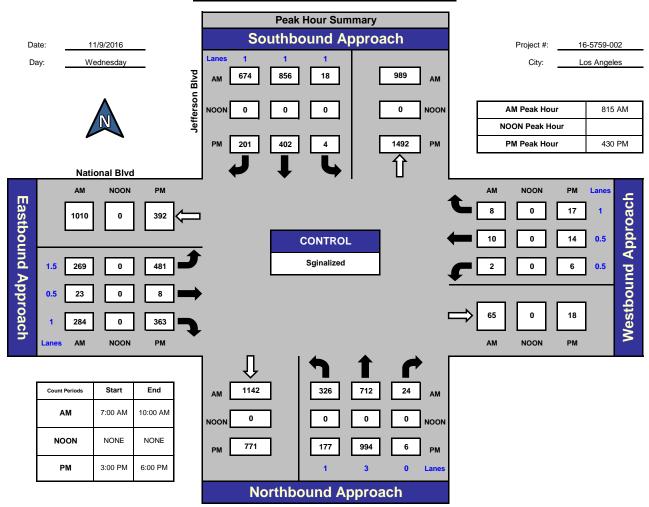
City:	Los Angeles				PI	M			Date: 11/9/201				
NS/EW Streets:	Jet	fferson Blvd		Je	fferson Blvc	ŀ	Na	ational Blvd		N	ational Blvd		
	NO	ORTHBOUN	D	SC	OUTHBOUN	D	E	ASTBOUNE	)	V	VESTBOUNI	)	
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	1	3	0	1	1	1	1.5	0.5	1	0.5	0.5	1	
3:00 PM	45	163	1	1	83	51	125	1	86	1	4	1	562
3:15 PM	38	157	2	0	84	58	125	1	97	1	1	0	564
3:30 PM	61	229	1	0	83	50	128	0	96	1	2	0	651
3:45 PM	36	195	4	2	96	47	148	3	100	1	1	4	637
4:00 PM	44	222	3	0	98	56	105	2	66	3	2	8	609
4:15 PM	38	246	3	2	78	44	104	0	110	0	3	5	633
4:30 PM	47	243	3	1	118	47	119	4	93	1	4	3	683
4:45 PM	41	220	1	0	88	49	142	1	107	2	5	2	658
5:00 PM	48	260	0	2	83	58	118	1	105	1	3	6	685
5:15 PM	41	271	2	1	113	47	102	2	58	2	2	6	647
5:30 PM	48	248	1	2	79	47	130	2	76	2	3	8	646
5:45 PM	37	243	2	0	72	46	105	2	99	2	1	2	611
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	524	2697	23	11	1075	600	1451	19	1093	17	31	45	7586
APPROACH %'s :	16.15%	83.14%	0.71%	0.65%	63.76%	35.59%	56.61%	0.74%	42.65%	18.28%	33.33%	48.39%	
PEAK HR START TIME:	430 F	PM											TOTAL
PEAK HR VOL:	177	994	6	4	402	201	481	8	363	6	14	17	2673
PEAK HR FACTOR:		0.937			0.914			0.852			0.925		0.976

## ITM Peak Hour Summary

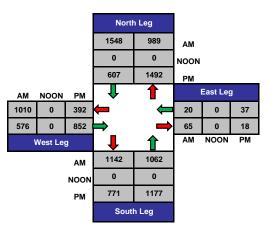


National Data & Surveying Services

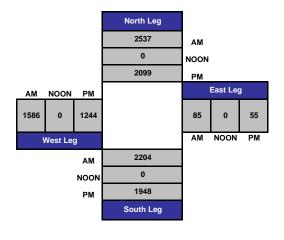
## Jefferson Blvd and National Blvd , Los Angeles



## **Total Ins & Outs**



## **Total Volume Per Leg**



Project ID: 16-5759-103 Day: Wednesday

City: Los Angeles Date: 11/9/2016 AM

NS/EW Streets:	Jef	ferson Blv	d	J	efferson Blv	/d	Higuera St/Rodeo Rd			Higu	eo Rd		
	NO	ORTHBOU	ND	5	OUTHBOU	ND		EASTBOUN	D	,	WESTBOUN	ID	
LANES:	NL 0	NT 0	NR 1	SL 0	ST 0	SR 0	EL 0	ET 0	ER 0	WL 0	WT 0	WR 0	TOTAL
7:00 AM	0	0	59	0	0	0	0	0	0	0	0	0	59
7:15 AM	0	0	99	0	0	0	0	0	0	0	0	0	99
7:30 AM	0	0	100	0	0	0	0	0	0	0	0	0	100
7:45 AM	Ō	0	114	0	0	0	0	0	0	0	0	0	114
8:00 AM	0	0	109	0	0	0	0	0	0	0	0	0	109
8:15 AM	0	0	104	0	0	0	0	0	0	0	0	0	104
8:30 AM	0	0	118	0	0	0	0	0	0	0	0	0	118
8:45 AM	0	0	131	0	0	0	0	0	0	0	0	0	131
9:00 AM	0	0	94	0	0	0	0	0	0	0	0	0	94
9:15 AM	0	0	113	0	0	0	0	0	0	0	0	0	113
9:30 AM	0	0	76	0	0	0	0	0	0	0	0	0	76
9:45 AM	0	0	84	0	0	0	0	0	0	0	0	0	84
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	0	0	1201	0	0	0	0	0	0	0	0	0	1201
APPROACH %'s:	0.00%	0.00%	100.00%	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	l
PEAK HR START TIME :	800 A	M											TOTAL
PEAK HR VOL:			462										462
PEAK HR FACTOR:													

Project ID: 16-5759-103 Day: Wednesday City: Los Angeles Date: 11/9/2016

City: I	City: Los Angeles						М			Date: 11/9/2016			
NS/EW Streets:	Jef	ferson Blv	d	Je	efferson Blv	rd	Higu	era St/Rode	o Rd	Higu	era St/Rode	eo Rd	
	NC	RTHBOUN	ND .	S	OUTHBOU	ND		EASTBOUN	D		WESTBOUN	ID	
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	0	0	1	0	0	0	0	0	0	0	0	0	
3:00 PM	0	0	235	0	0	0	0	0	0	0	0	0	235
3:15 PM	0	0	209	0	0	0	0	0	0	0	0	0	209
3:30 PM	0	0	219	0	0	0	0	0	0	0	0	0	219
3:45 PM	0	0	241	0	0	0	0	0	0	0	0	0	241
4:00 PM	0	0	251	0	0	0	0	0	0	0	0	0	251
4:15 PM	0	0	233	0	0	0	0	0	0	0	0	0	233
4:30 PM	0	0	228	0	0	0	0	0	0	0	0	0	228
4:45 PM	0	0	158	0	0	0	0	0	0	0	0	0	158
5:00 PM	0	0	212	0	0	0	0	0	0	0	0	0	212
5:15 PM	0	0	173	0	0	0	0	0	0	0	0	0	173
5:30 PM	0	0	220	0	0	0	0	0	0	0	0	0	220
5:45 PM	0	0	227	0	0	0	0	0	0	0	0	0	227
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	0	0	2606	0	0	0	0	0	0	0	0	0	2606
APPROACH %'s:	0.00%	0.00%	100.00%	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	l I
PEAK HR START TIME :	430 F	M											TOTAL
PEAK HR VOL:			771										771
PEAK HR FACTOR:													

Project ID: 16-5759-103 Day: Wednesday

City: Los Angeles Date: 11/9/2016 AM

NS/EW Streets:	Jef	ferson Blv	d	J	efferson Blv	/d	Higuera St/Rodeo Rd			Higu	eo Rd		
	NO	ORTHBOU	ND	5	OUTHBOU	ND		EASTBOUN	D	,	WESTBOUN	ID	
LANES:	NL 0	NT 0	NR 1	SL 0	ST 0	SR 0	EL 0	ET 0	ER 0	WL 0	WT 0	WR 0	TOTAL
7:00 AM	0	0	59	0	0	0	0	0	0	0	0	0	59
7:15 AM	0	0	99	0	0	0	0	0	0	0	0	0	99
7:30 AM	0	0	100	0	0	0	0	0	0	0	0	0	100
7:45 AM	Ō	0	114	0	0	0	0	0	0	0	0	0	114
8:00 AM	0	0	109	0	0	0	0	0	0	0	0	0	109
8:15 AM	0	0	104	0	0	0	0	0	0	0	0	0	104
8:30 AM	0	0	118	0	0	0	0	0	0	0	0	0	118
8:45 AM	0	0	131	0	0	0	0	0	0	0	0	0	131
9:00 AM	0	0	94	0	0	0	0	0	0	0	0	0	94
9:15 AM	0	0	113	0	0	0	0	0	0	0	0	0	113
9:30 AM	0	0	76	0	0	0	0	0	0	0	0	0	76
9:45 AM	0	0	84	0	0	0	0	0	0	0	0	0	84
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	0	0	1201	0	0	0	0	0	0	0	0	0	1201
APPROACH %'s:	0.00%	0.00%	100.00%	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	l
PEAK HR START TIME :	800 A	M											TOTAL
PEAK HR VOL:			462										462
PEAK HR FACTOR:													

Project ID: 16-5759-103 Day: Wednesday City: Los Angeles Date: 11/9/2016

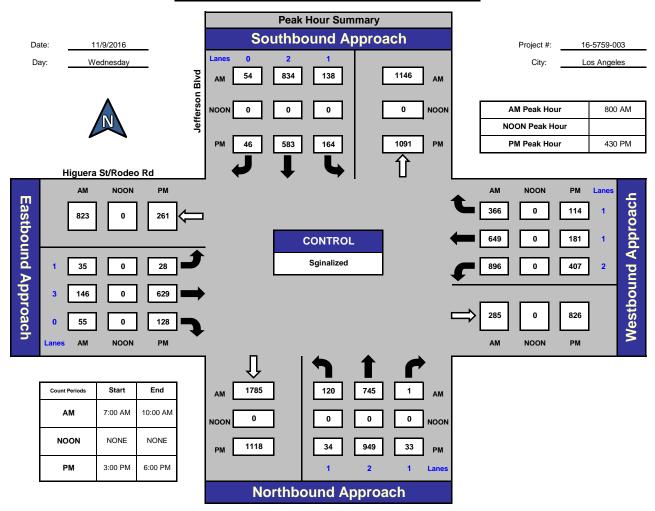
City: I	City: Los Angeles						М			Date: 11/9/2016			
NS/EW Streets:	Jef	ferson Blv	d	Je	efferson Blv	rd	Higu	era St/Rode	o Rd	Higu	era St/Rode	eo Rd	
	NC	RTHBOUN	ND .	S	OUTHBOU	ND		EASTBOUN	D		WESTBOUN	ID	
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
LANES:	0	0	1	0	0	0	0	0	0	0	0	0	
3:00 PM	0	0	235	0	0	0	0	0	0	0	0	0	235
3:15 PM	0	0	209	0	0	0	0	0	0	0	0	0	209
3:30 PM	0	0	219	0	0	0	0	0	0	0	0	0	219
3:45 PM	0	0	241	0	0	0	0	0	0	0	0	0	241
4:00 PM	0	0	251	0	0	0	0	0	0	0	0	0	251
4:15 PM	0	0	233	0	0	0	0	0	0	0	0	0	233
4:30 PM	0	0	228	0	0	0	0	0	0	0	0	0	228
4:45 PM	0	0	158	0	0	0	0	0	0	0	0	0	158
5:00 PM	0	0	212	0	0	0	0	0	0	0	0	0	212
5:15 PM	0	0	173	0	0	0	0	0	0	0	0	0	173
5:30 PM	0	0	220	0	0	0	0	0	0	0	0	0	220
5:45 PM	0	0	227	0	0	0	0	0	0	0	0	0	227
	NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
TOTAL VOLUMES:	0	0	2606	0	0	0	0	0	0	0	0	0	2606
APPROACH %'s:	0.00%	0.00%	100.00%	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	l I
PEAK HR START TIME :	430 F	M											TOTAL
PEAK HR VOL:			771										771
PEAK HR FACTOR:													

## ITM Peak Hour Summary

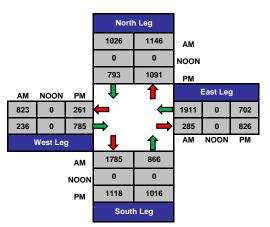


National Data & Surveying Services

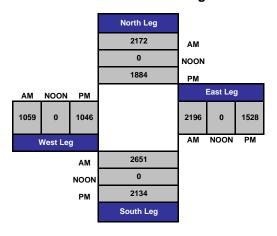
## Jefferson Blvd and Higuera St/Rodeo Rd , Los Angeles







## **Total Volume Per Leg**

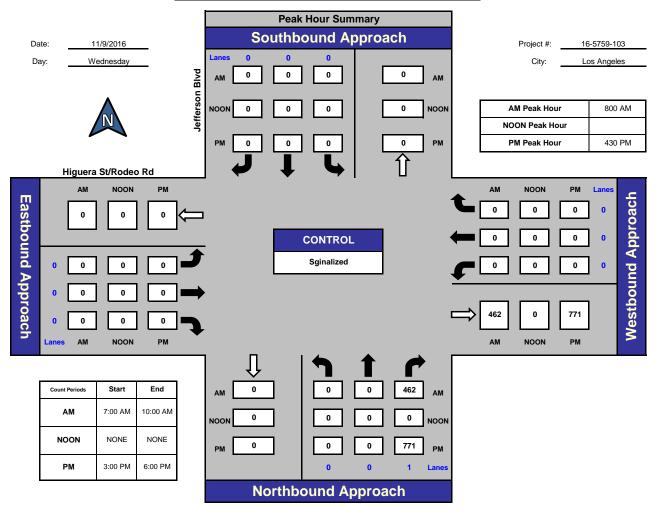


## ITM Peak Hour Summary

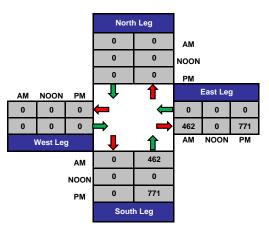


National Data & Surveying Services

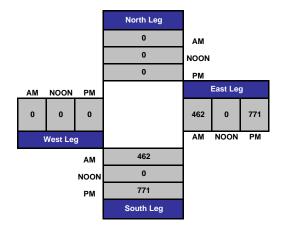
## Jefferson Blvd and Higuera St/Rodeo Rd, Los Angeles







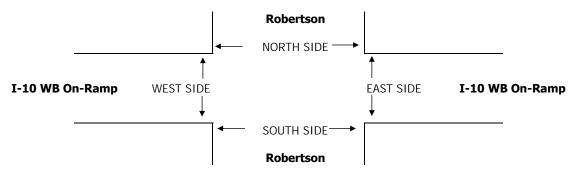
**Total Volume Per Leg** 



PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: Thu, Mar 3, 16 LOCATION:CulverPROJECT #:SC1603NORTH & SOUTH:RobertsonLOCATION #:3EAST & WEST:I-10 WB On-RampCONTROL:STOP S/W

	NOTES:										AM		<b>A</b>	
											PM		N	
											MD	<b>⋖</b> W	•	E▶
											OTHER		S	
											OTHER		▼	
		NI	ODTUDOL	IND	C.	SUTUBOL	IND		ACTROUN	ID.		/ECTROLIN		
		IN	ORTHBOL	IND	50	DUTHBOU	טאינ		ASTBOUN			/ESTBOUI		
		NII	Robertson	ND	CI	Robertson	CD		-10 WB On-Rar			I-10 WB On-R		TOTAL
	LANES:	NL X	NT X	NR X	SL X	ST 2	SR 1	EL X	ET X	ER X	WL 0.5	WT 0.5	WR 1	TOTAL
										Į.				
	7:00 AM	0	0	0	0	44	181	0	0	0	4	150	113	492
	7:15 AM	0	0	0	0	40	208	0	0	0	6	165	153	572
	7:30 AM	0	0	0	0	56	225	0	0	0	3	153	171	608
1	7:45 AM	0	0	0	0	62	236	0	0	0	5	140	165	608
	8:00 AM	0	0	0	0	54	211	0	0	0	3	155	182	605
	8:15 AM	0	0	0	0	63	202	0	0	0	7	142	186	600
	8:30 AM	0	0	0	0	55	213	0	0	0	5	139	229	641
Σ	8:45 AM VOLUMES	0	0	0	0	68	207	0	0	0	4	146	192	617
⋖	VOLUMES	0	0	0	0	442	1,683	0	0	0	37	1,190	1,391	4,743
	APPROACH %	0%	0%	0%	0%	21%	79%	0%	0%	0%	1%	45%	53%	
	APP/DEPART	0	/	1,391	2,125	/	479	0	/	0	2,618	/	2,873	0
	BEGIN PEAK HR	_	8:00 AM		_			_	_	_				
	VOLUMES	0	0	0	0	240	833	0	0	0	19	582	789	2,463
	APPROACH %	0%	0%	0%	0%	22%	78%	0%	0%	0%	1%	42%	57%	
	PEAK HR FACTOR		0.000			0.975			0.000			0.932		0.961
	APP/DEPART	0		789	1,073	/	259	0	/	0	1,390	/	1,415	0
	4:00 PM	0	0	0	0	94	145	0	0	0	7	108	131	485
	4:15 PM	0	0	0	0	119	119	0	0	0	6	76	139	459
	4:30 PM	0	0	0	0	114	129	0	0	0	9	100	140	492
	4:45 PM	0	0	0	0	122	111	0	0	0	15	106	134	488
	5:00 PM	0	0	0	0	112	132	0	0	0	5	110	126	485
	5:15 PM	0	0	0	0	119	134	0	0	0	11	121	134	519
1	5:30 PM	0	0	0	0	115	149	0	0	0	17	109	164	554
Σ	5:45 PM	0	0	0	0	138	117	0	0	0	5	134	143	537
ľ	VOLUMES	0	0	0	0	933	1,036	0	0	0	75 407	864	1,111	4,019
1	APPROACH %	0%	0%	0%	0%	47%	53%	0%	0%	0%	4%	42%	54%	
	APP/DEPART	0		1,111	1,969	/	1,008	0	/	0	2,050	/	1,900	0
	BEGIN PEAK HR		5:00 PM											
1	VOLUMES	0	0	0	0	484	532	0	0	0	38	474	567	2,095
I	APPROACH %	0%	0%	0%	0%	48%	52%	0%	0%	0%	4%	44%	53%	l
	PEAK HR FACTOR		0.000			0.962			0.000			0.930		0.945
L	APP/DEPART	0		567	1,016	/	522	0	/	0	1,079	/	1,006	0



PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

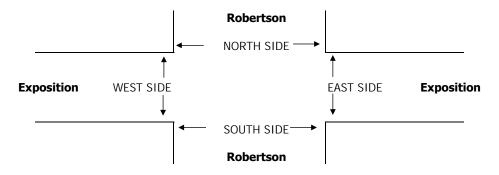
DATE: Thu, Mar 3, 16 LOCATION:CulverPROJECT #:SC1603NORTH & SOUTH:RobertsonLOCATION #:2EAST & WEST:ExpositionCONTROL:STOP S/E

NOTES:

NR - I-10 WB Off Ramp

AM		<b>A</b>	
PM		N	
MD	<b>⋖</b> W	•	E►
OTHER		S	
OTHER		•	

		NORTHBOUND Robertson				OUTHBOU	ND	E	ASTBOUN	ID	V	/ESTBOUN	D	
			Robertson			Robertson			Exposition			Exposition		
		NL	NT	NR	SL	ST	SR	EL	ET	ER	WL	WT	WR	TOTAL
	LANES:	X	X	1	1	X	1	X	1	X	X	X	Χ	
	7:00 AM	0	0	152	43	0	5	0	4	0	0	0	0	204
	7:15 AM	0	0	179	41	0	1	0	3	0	0	0	0	224
	7:30 AM	0	0	211	56	0	1	0	0	0	0	0	0	268
	7:45 AM	0	0	246	60	0	4	0	1	0	0	0	0	311
	8:00 AM	0	0	300	53	0	1	0	0	0	0	0	0	354
	8:15 AM	0	0	310	68	0	5	0	1	0	0	0	0	384
	8:30 AM	0	0	316	61	0	1	0	0	0	0	0	0	378
AΜ	8:45 AM	0	0	321	65	0	4	0	3	0	0	0	0	393
₹	VOLUMES	0	0	2,035	447	0	22	0	12	0	0	0	0	2,516
	APPROACH %	0%	0%	100%	95%	0%	5%	0%	100%	0%	0%	0%	0%	
	APP/DEPART	2,035		0	469	/	0	12	/	2,494	0	/	22	0
	BEGIN PEAK HR		8:00 AM											
	VOLUMES	0	0	1,247	247	0	11	0	4	0	0	0	0	1,509
	APPROACH %	0%	0%	100%	96%	0%	4%	0%	100%	0%	0%	0%	0%	
	PEAK HR FACTOR		0.971			0.884			0.333			0.000		0.960
	APP/DEPART	1,247	1	0	258	/	0	4	/	1,498	0	/	11	0
	4:00 PM	0	0	158	89	0	17	0	17	0	0	0	0	281
	4:15 PM	0	0	126	111	0	15	0	17	0	0	0	0	269
	4:30 PM	0	0	133	106	0	14	0	11	0	0	0	0	264
	4:45 PM	0	0	137	125	0	16	0	21	0	0	0	0	299
	5:00 PM	0	0	136	108	0	11	0	12	0	0	0	0	267
	5:15 PM	0	0	115	130	0	10	0	10	0	0	0	0	265
	5:30 PM	0	0	129	111	0	15	0	16	0	0	0	0	271
Σ	5:45 PM	0	0	123	127	0	8	0	15	0	0	0	0	273
l a	VOLUMES	0	0	1,057	907	0	106	0	119	0	0	0	0	2,189
	APPROACH %	0%	0%	100%	90%	0%	10%	0%	100%	0%	0%	0%	0%	
	APP/DEPART	1,057		0	1,013	/	0	119	/	2,083	0	/	106	0
	BEGIN PEAK HR		4:00 PM											
	VOLUMES	0	0	554	431	0	62	0	66	0	0	0	0	1,113
	APPROACH %	0%	0%	100%	87%	0%	13%	0%	100%	0%	0%	0%	0%	
	PEAK HR FACTOR		0.877			0.874			0.786			0.000		0.931
	APP/DEPART	554		0	493	/	0	66	/	1,051	0	/	62	0



PREPARED BY: Video & AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

DATE: Thu, Sep 24, 15

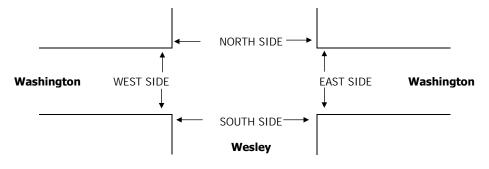
NOTES:

LOCATION: NORTH & SOUTH: EAST & WEST: Culver City Wesley Washington

PROJECT #: SC0715 LOCATION #: 27 CONTROL: UNSIGNAL

Ν

NORTHBOUND   SOUTHBOUND   EASTBOUND   Westbound   W											MD	<b>⋖</b> W	1	E▶
NORTHBOUND   Wesley   NORTHBOUND   Wesley   W												,	S	
NORTHBOUND   NORTHBOUND   Westery   Westery													_	
Name		NG	DTUDOU	ND		VIITUDOU	NID		ACTROLIA	ID.		ECTROUR	•	
LANES:   NL   NT   NR   SL   ST   SR   EL   ET   ER   WL   WT   WR   TOTAL		NC		ND	SC	OUTHROU	ND	E,		ID	VV			
LANES:   0		NII		ND	CI	СТ	CD			- FD	\ A /I			TOTAL
7:00 AM	I ANES:		1							1				TOTAL
7:15 AM				U	_					_				
7:30 AM				1	_	1 -				_				
7:45 AM			•	,	_	_	_	_		_	-		)	
8:00 AM         1         0         1         0         0         0         167         6         2         345         0         522           8:15 AM         1         0         2         0         0         0         0         183         5         3         343         0         537           8:30 AM         4         0         1         0         0         0         0         158         9         2         299         0         473           8:45 AM         2         0         0         0         0         162         0         4         434         0         602           VOLUMES         12         0         7         0         0         0         0         12,236         37         26         2,806         0         4,124           APPROACH %         63%         0%         37%         0%         0%         0%         97%         3%         1%         99%         0%           APPOEPART         19         1         0         0         0         0         0         70         2         20         11         1,540         0         2,280								•					)	
8:15 AM         1         0         2         0         0         0         183         5         3         343         0         537           8:30 AM         4         0         1         0         0         0         0         158         9         2         299         0         473           8:45 AM         2         0         0         0         0         0         0         162         0         4         434         0         602           VOLUMES         12         0         7         0         0         0         0         1,236         37         26         2,806         0         4,124           APPROECH %         63%         0%         37%         0%         0%         0%         97%         3%         1%         99%         0%           APPOEDEART         19         1         0         0         0         0         702         20         11         1,540         0         2,280           APPROECH %         29%         0%         71%         0%         0%         0%         97%         3%         1%         99%         0%           APPOEDEART			_	•	•		_	•		·	_			
8:30 AM         4         0         1         0         0         0         158         9         2         299         0         473           8:45 AM         2         0         0         0         0         0         162         0         4         434         0         602           VOLUMES         12         0         7         0         0         0         0         1,236         37         26         2,806         0         4,124           APP/DEPART         19         J         0         0         J         638         1%         99%         0%           APP/DEPART         19         J         0         0         J         63         1,273         J         1,243         2,832         J         2,818         0           BEGIN PEAK HR         730 AM         VOLUMES         2         0         5         0         0         0         70         22         20         11         1,540         0         2,280           APPROACH %         29%         0%         71%         0%         0%         0%         0%         97%         3%         1%         99%         0% </td <td></td> <td>•</td> <td></td> <td>•</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td></td>		•		•						_				
S:45 AM		-	_				_							
VOLUMES				•	_	_				-				
APPROACH %   63%   0%   37%   0%   0%   0%   0%   97%   3%   1%   99%   0%   0%   APP/DEPART   19			_	_									Ţ	
APP/DEPART			_	•	_	-		-				,	-	4,124
BEGIN PEAK HR   VOLUMES   2			0%			0%			97%			99%		
VOLUMES         2         0         5         0         0         0         0         702         20         11         1,540         0         2,280           APPROACH %         29%         0%         71%         0%         0%         0%         0%         97%         3%         1%         99%         0%           PEAK HR FACTOR         0.583         0.000         0         0.907         0.848         0.868           APP/DEPART         7         7         0         0         /         31         722         /         707         1,551         /         1,542         0           4:15 PM         2         0         11         0         0         0         0         268         2         1         183         0         473           4:15 PM         2         0         11         0         0         0         258         3         1         176         0         451           4:30 PM         7         0         7         0         0         0         292         2         3         173         0         484           4:45 PM         4         0         3		19		0	0	/	63	1,273	/	1,243	2,832	/	2,818	0
APPROACH % PEAK HR FACTOR         29%         0%         71%         0%         0%         0%         0%         97%         3%         1%         99%         0%           APP/DEPART         7         1         0         0         7         31         722         7         707         1,551         7         1,542         0           4:00 PM         8         0         11         0         0         0         268         2         1         183         0         473           4:15 PM         2         0         11         0         0         0         258         3         1         176         0         451           4:30 PM         7         0         7         0         0         0         292         2         3         173         0         484           4:30 PM         7         0         7         0         0         0         292         2         3         173         0         484           4:45 PM         4         0         3         0         0         0         348         1         1         283         0         638           5:15 PM	-		7:30 AM											
PEAK HR FACTOR	VOLUMES	2	0		0	0	0	0	702	20	11	1,540	0	2,280
APP/DEPART         7         1         0         0         /         31         722         /         707         1,551         /         1,542         0           4:00 PM         8         0         11         0         0         0         268         2         1         183         0         473           4:15 PM         2         0         11         0         0         0         258         3         1         176         0         451           4:30 PM         7         0         7         0         0         0         292         2         3         173         0         484           4:45 PM         4         0         3         0         0         0         348         3         2         197         0         557           5:00 PM         1         0         4         0         0         0         348         1         1         283         0         638           5:15 PM         0         0         2         0         0         0         347         0         1         258         0         608           5:30 PM         4         0<	APPROACH %	29%	0%	71%	0%	0%	0%	0%	97%	3%	1%	99%	0%	
4:00 PM         8         0         11         0         0         0         268         2         1         183         0         473           4:15 PM         2         0         11         0         0         0         0         258         3         1         176         0         451           4:30 PM         7         0         7         0         0         0         0         292         2         3         173         0         484           4:45 PM         4         0         3         0         0         0         0         348         3         2         197         0         557           5:00 PM         1         0         4         0         0         0         348         1         1         283         0         638           5:15 PM         0         0         2         0         0         0         347         0         1         258         0         608           5:30 PM         4         0         3         0         0         0         361         1         1         207         0         573           VOLUMES	PEAK HR FACTOR		0.583			0.000			0.907			0.848		0.868
4:15 PM         2         0         11         0         0         0         258         3         1         176         0         451           4:30 PM         7         0         7         0         0         0         292         2         3         173         0         484           4:45 PM         4         0         3         0         0         0         348         3         2         197         0         557           5:00 PM         1         0         4         0         0         0         348         1         1         283         0         638           5:15 PM         0         0         2         0         0         0         347         0         1         258         0         608           5:30 PM         4         0         3         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42	APP/DEPART	7	1	0	0	/	31	722	/	707	1,551	/	1,542	0
4:30 PM         7         0         7         0         0         0         292         2         3         173         0         484           4:45 PM         4         0         3         0         0         0         0         348         3         2         197         0         557           5:00 PM         1         0         4         0         0         0         0         348         1         1         283         0         638           5:15 PM         0         0         2         0         0         0         347         0         1         258         0         608           5:30 PM         4         0         3         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42         0         0         0         0         2,512         13         12         1,732         0         4,339           APP/DEPART	4:00 PM	8	0	11	0	0	0	0	268	2	1	183	0	473
4:45 PM         4         0         3         0         0         0         0         348         3         2         197         0         557           5:00 PM         1         0         4         0         0         0         0         348         1         1         283         0         638           5:15 PM         0         0         2         0         0         0         0         347         0         1         258         0         608           5:30 PM         4         0         3         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42         0         0         0         0         2,555         1,744         /         1,760         0           APP/DEPART </td <td>4:15 PM</td> <td>2</td> <td>0</td> <td>11</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>258</td> <td>3</td> <td>1</td> <td>176</td> <td>0</td> <td>451</td>	4:15 PM	2	0	11	0	0	0	0	258	3	1	176	0	451
5:00 PM         1         0         4         0         0         0         348         1         1         283         0         638           5:15 PM         0         0         2         0         0         0         0         347         0         1         258         0         608           5:30 PM         4         0         3         0         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42         0         0         0         0         361         1         1         207         0         573           APPROACH %         40%         0%         60%         0%         0%         0%         99%         1%         1%         99%         0%           APP/DEPART         70         1         0         0         0         0         0         1,346         3         5         1,003         0         2,374		7	0	7	0	0	0	0	292	2	3	173	0	484
5:15 PM         0         0         2         0         0         0         347         0         1         258         0         608           5:30 PM         4         0         3         0         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42         0         0         0         0         2,512         13         12         1,732         0         4,339           APPROACH %         40%         0%         60%         0%         0%         0%         99%         1%         1%         99%         0%           APP/DEPART         70         1         0         0         0         0         0         1,346         3         5         1,744         /         1,760         0           BEGIN PEAK HR         5:00 PM         5:00 PM         0%         0%         0%         0%         0%         0%         0%         0%         0% <td>4:45 PM</td> <td>4</td> <td>0</td> <td>3</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>348</td> <td>3</td> <td>2</td> <td>197</td> <td>0</td> <td>557</td>	4:45 PM	4	0	3	0	0	0	0	348	3	2	197	0	557
5:30 PM         4         0         3         0         0         0         0         290         1         2         255         0         555           5:45 PM         2         0         1         0         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42         0         0         0         0         2,512         13         12         1,732         0         4,339           APPROACH %         40%         0%         60%         0%         0%         0%         99%         1%         1%         99%         0%           APP/DEPART         70         /         0         0         /         24         2,525         /         2,555         1,744         /         1,760         0           BEGIN PEAK HR         5:00 PM         5:00 PM         0         0         0         0         1,346         3         5         1,003         0         2,374           APPROACH %         41%         0%         59%         0%         0%         0%         0%         0%         0%         0%         0%	5:00 PM	1	0	4	0	0	0	0	348	1	1	283	0	638
5:45 PM         2         0         1         0         0         0         361         1         1         207         0         573           VOLUMES         28         0         42         0         0         0         0         2,512         13         12         1,732         0         4,339           APPROACH %         40%         0%         60%         0%         0%         0%         99%         1%         1%         99%         0%           APP/DEPART         70         /         0         0         /         24         2,525         /         2,555         1,744         /         1,760         0           BEGIN PEAK HR         5:00 PM         5:00 PM         5:00 PM         7         0         10         0         0         0         1,346         3         5         1,003         0         2,374           APPROACH %         41%         0%         59%         0%         0%         0%         100%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         <	5:15 PM	0	0	2	0	0	0	0	347	0	1	258	0	608
VOLUMES         28         0         42         0         0         0         0         2,512         13         12         1,732         0         4,339           APPROACH %         40%         0%         60%         0%         0%         0%         99%         1%         1%         99%         0%           APP/DEPART         70         /         0         0         /         24         2,525         /         2,555         1,744         /         1,760         0           BEGIN PEAK HR         5:00 PM         5:00 PM         5:00 PM         7         0         10         0         0         0         1,346         3         5         1,003         0         2,374           APPROACH %         41%         0%         59%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         0%         <	5:30 PM	4	0	3	0	0	0	0	290	1	2	255	0	555
APPROACH %	5:45 PM	2	0	1	0	0	0	0	361	1	1	207	0	573
APP/DEPART         70         /         0         0         /         24         2,525         /         2,555         1,744         /         1,760         0           BEGIN PEAK HR         5:00 PM         6:00	VOLUMES	28	0	42	0	0	0	0	2,512	13	12	1,732	0	4,339
APP/DEPART         70         /         0         0         /         24         2,525         /         2,555         1,744         /         1,760         0           BEGIN PEAK HR         5:00 PM         6:00	APPROACH %	40%	0%	60%	0%	0%	0%	0%					0%	
BEGIN PEAK HR         5:00 PM           VOLUMES         7         0         10         0         0         0         1,346         3         5         1,003         0         2,374           APPROACH %         41%         0%         59%         0%         0%         0%         100%         0%         0%         100%         0%           PEAK HR FACTOR         0.607         0.000         0.932         0.887         0.930		70	1	0	0	/	24	2,525	/		1,744	/	1,760	0
APPROACH %         41%         0%         59%         0%         0%         0%         100%         0%         100%         0%           PEAK HR FACTOR         0.607         0.000         0.932         0.887         0.930			5:00 PM											
APPROACH %         41%         0%         59%         0%         0%         0%         100%         0%         100%         0%           PEAK HR FACTOR         0.607         0.000         0.932         0.887         0.930	VOLUMES	7	0	10	0	0	0	0	1,346	3	5	1,003	0	2,374
PEAK HR FACTOR 0.607 0.000 0.932 0.887 0.930		41%	-		-	-		_	•	-	-	,	-	=,
														0.930
	APP/DEPART	17	1	0	0	/	7	1,349	/	1,357	1,008	/	1,010	0.700



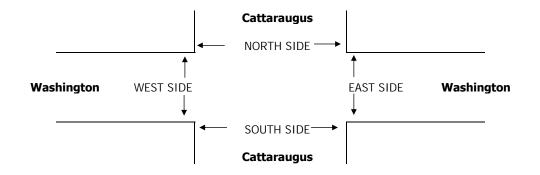
PREPARED BY: AimTD LLC. tel: 714 253 7888 pacific@aimtd.com

<u>DATE:</u> Thu, Mar 3, 16

APP/DEPART

LOCATION:CulverPROJECT #:SC1603NORTH & SOUTH:CattaraugusLOCATION #:1EAST & WEST:WashingtonCONTROL:STOP N\S

NOTES: Ν ■ W E► S NORTHBOUND SOUTHBOUND **EASTBOUND** WESTBOUND Cattaraugus Cattaraugus Washington Washington TOTAL NT SL ST EL ET WL WT WR NL NR SR ER LANES: O O 7:00 AM 7:15 AM 7:30 AM 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM **VOLUMES** 1,277 2,711 5,045 1% APPROACH % 37% 27% 37% 42% 57% 5% 94% 1% 1% 79% 20% 1,385 3,436 2,849 APP/DEPART 1,360 BEGIN PEAK HR 7:45 AM 2,639 **VOLUMES** 1,357 15% 45% 2% APPROACH % 40% 43% 56% 5% 93% 1% 1% 78% 21% PEAK HR FACTOR 0.833 0.824 0.899 0.885 0.953 APP/DEPART 1.731 1.430 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM **VOLUMES** 2,376 1,315 4,255 9% 2% APPROACH % 45% 59% 4% 38% 3% 95% 1% 91% 8% 45% APP/DEPART 2,498 1,442 1,440 2,562 BEGIN PEAK HR 4:30 PM **VOLUMES** 1,205 2,168 3% APPROACH % 56% 0% 44% 63% 95% 2% 1% 92% 7% 1% 36% PEAK HR FACTOR 0.934 0.957 0.978 0.563 0.815



1,266

1,306

Ω

## **APPENDIX D**

**Level of Service Worksheets** 



(Circular 212 Method)



I/S #:	North-South Street:	Roberts	on Boulevar	ď		Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	,
1	East-West Street:	I-10 WB	Off-Ramp -	Kincardir	ne Av	Proje	ction Year	2018		Pea	ak Hour:	AM	Revie	wed by:	R	RA	Project:		RA491	
	posed Ø'ing: N/S-1, E/W-2 o Turns: FREE-1, NRTOR-2 o ATSAC-1 or ATSAC-	r OLA-3? ATCS-2?	NB 0 EB 0	SB WB	2 0 0 0 2	NB EB	0 SE 0 W		NB EB	0 0	SB WB	2 0 0 0 2	NB EB	0	SB WB	2 0 0 0 2	NB EB	0	SB WB	2 0 0 0 2
	Override	Capacity	FYISTI	NG CONDI	0 TION	FYIST	ING PLUS PI		FUTUR	E CONDITI	ON W/O PR		FUTUE	RE CONDIT	ION W/ PR	•	FUTURE	W/ PROJE	CT W/ MIT	
	MOVEMENT			No. of Lanes	Lane Volume	Project Traffic	Total	Lane	Added Volume	Total Volume	No. of	Lane	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of	Lane Volume
	↑ Left		Volume 58	Lanes 1	58	0	Volume 58	Volume 58	Volume	volume 59	Lanes 1	volume 59	0 0	59	Lanes	59	Volume	59	Lanes 1	59
NORTHBOUND	Left Left-Through Through-Right Right Left-Through-Right Left-Through-Right		1263 0	0 2 0 0 0	632 0	1 0	1264 0	632	42 0	1330 0	0 2 0 0 0	665 0	1 0	1331	0 2 0 0 0	666 0	0	1331	0 2 0 0 0	666
SOUTHBOUND	Left  Left-Through  Through  Through-Right  Right  Left-Through-Right  Left-Right		0 1401 77	0 0 1 1 0 0	7 <b>39</b>	0 5 0	0 1406 77	0 <b>742</b> 77	0 49 0	0 1478 79	0 0 1 1 0 0	0 <b>779</b> 79	0 5 0	0 1483 79	0 0 1 1 1 0 0	0 <b>781</b> 79	0 0	0 1483 79	0 0 1 1 1 0 0	0 <b>781</b> 79
EASTBOUND	☐ Left ☐ Left-Through ☐ Through ☐ Through-Right ☐ Right ☐ Left-Through-Right ☐ Left-Right		109 0 60	0 0 0 0 0 0	109 0 <b>169</b>	0 0	109 0 60	109 0 <b>169</b>	0 0	111 0 61	0 0 0 0 0 0	111 0 <b>172</b>	0 0	111 0 61	0 0 0 0 0 0	111 0 <b>172</b>	0 0	111 0 61	0 0 0 0 0 0	111 0 <b>172</b>
WESTBOUND	← Left  ← Left-Through  ← Through-Right  ← Right  ← Left-Through-Right  ← Left-Right		66 48 104	0 1 0 0 1 0	66 114 104	4 0 0	70 48 104	<b>70</b> 118 104	135	202 49 106	0 1 0 0 1 0	<b>202</b> 251 106	4 0 0	206 49 106	0 1 0 0 1 0 0	<b>206</b> 255 106	0 0 0	206 49 106	0 1 0 0 1 0	<b>206</b> 255 106
	CRITICAL V			th-South: ast-West: SUM:	797 235 1032		rth-South: East-West: SUM:	800 239 1039			th-South: ast-West: SUM:	838 374 1212			th-South: ast-West: SUM:				th-South: ast-West: SUM:	840 378 1218
V/C	VOLUME/CAPACITY (V/C C LESS ATSAC/ATCS ADJU	STMENT:			0.688 <b>0.588</b> A			0.693 <b>0.593</b>				0.808 0.708 C				0.812 0.712 C				0.812 0.712 C
<u> </u>	LEVEL OF SERVICE (LOS		<u> </u>										<u> </u>							

REMARKS:

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.004  $\Delta v/c$  after minimal Significant impacted? NO Fully m

 $\Delta v/c$  after mitigation: 0.004 Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Roberts	on Boulevar	d		Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
1	East-West Street:	I-10 WB	Off-Ramp -	Kincardir	ne Av		ction Year				ak Hour:	PM		wed by:		RA	Project:		RA491	
		f Phases			2	,		2				2				2	,			2
Орр	oosed Ø'ing: N/S-1, E/W-2 or	Both-3?	ND 0	66	0	N/C	0 0	0	ME	0	65	0	NE	0	65	0	N/C	0	65	0
Right	Turns: FREE-1, NRTOR-2 or	r OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SE		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	ATSAC-1 or ATSAC+	ATCS-2?		2	2			2				2				2				2
	Override	Capacity			0			0				0				0				0
	MOVEMENT		EXISTI	NG CONDI			ING PLUS P				ON W/O PR			RE CONDIT				W/ PROJE		
	IVIO V EIVIEN I		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
	↑ Left		46	1	46	0	46	46	0	47	1	47	0	47	1	47	0	47	1	47
NORTHBOUND	← Left-Through			0							0				0				0	
∥ જૂ	Through		893	2	447	5	898	449	70	981	2	491	5	986	2	493	0	986	2	493
∥ ≝ I	Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	0
O.R.	<ul><li></li></ul>			0	U		U	U		U	0	U		U	0	U		U	0	U
2	Left-Right			0							0				0				0	
_												- -								
9	<ul><li></li></ul>		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	0
	Through		1482	1	763	2	1484	764	38	1550	1	798	2	1552	1	799	0	1552	1	799
Ě	← Through-Right			1							1				1				1	
SOUTHBOUND			44	0 0	44	0	44	44	0	45	0 0	45	0	45	0	45	0	45	0 0	45
S	Left-Right			0							0				0				0	
_												=			-					
ا م ا	<ul><li>J Left</li><li>→ Left-Through</li></ul>		72	0 0	72	0	72	72	0	73	0 0	73	0	73	0	73	0	73	0 0	73
Ž	→ Leπ-Inrougn → Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
EASTBOUND	→ Through-Right			0							0				0			,	0	
AST	Right		65	0	137	0	65	137	0	66	0 0	139	0	66	0	139	0	66	0	139
ш	★ Left-Through-Right     → Left-Right			0 1							1				1				U 1	
	*																	_		
ا ۾	✓ Left		281	0	281	2	283	283	83	370	0	370	2	372	0	372	0	372	0	372
WESTBOUND			40	1 0	321	0	40	323	0	41	1 0	411	0	41	1 0	413	0	41	1 0	413
]B0	Through-Right		"	0	321		10	020			0			• • •	Ö				0	1.0
EST	Right  Left-Through-Right		527	1	527	0	527	527	0	538	1	538	0	538	1	538	0	538	1	538
Š	Left-Through-Right Left-Right			0 0							0 0				0				0 0	
	North-South:		809	No	rth-South:	810		Nor	th-South:	845		Nor	th-South:	846		Nor	th-South:	846		
	CRITICAL V	OLUMES	E	ast-West:	599	1	East-West:	599		E	ast-West:	611		E	ast-West:			E	ast-West:	611
-	VOLUME/CARACITY (V/O	1 DATIC:		SUM:	1408		SUM:	1409			SUM:	1456			SUM:				SUM:	
1400	VOLUME/CAPACITY (V/C	,			0.939			0.939				0.971				0.971				0.971
V/C	LESS ATSAC/ATCS ADJUS				0.839			0.839				0.871				0.871				0.871
	LEVEL OF SERVICE (LOS):  REMARKS:				D			D				D				D				D

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.000  $\Delta v/c$  after Significant impacted? NO Fully

 $\triangle v/c$  after mitigation: 0.000 Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Roberts	on Boulevar	d		Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	,
2	East-West Street:	National	Boulevard			Proje	ction Year	2018		Pea	ak Hour:	AM	Revie	wed by:	R	RA	Project:		RA491	
	posed Ø'ing: N/S-1, E/W-2 o Turns: FREE-1, NRTOR-2 o ATSAC-1 or ATSAC+	r OLA-3? -ATCS-2?	NB 0 EB 0	SB WB	4 0 0 3 2 0	NB EB	0 SE 0 W		NB EB	0 0	SB WB	4 0 0 3 2	NB EB	0	SB WB	4 0 0 3 2	NB EB	0	SB WB	4 0 0 3 2 0
	Override	Capacity	FYISTI	NG CONDI		FYIST	ING PLUS PI		FUTUR	E CONDITI	ON W/O PR		FUTUE	RE CONDIT	ION W/ PR	•	FUTUR	W/ PROJE	CT W/ MIT	
	MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
NORTHBOUND	Left Left-Through Through-Right Right Left-Through-Right Left-Right		75 713 31	1 0 1 1 0 0	75 <b>372</b> 31	0 0	75 713 31	75 <b>372</b> 31	13 4 23	90 731 55	1 0 1 1 0 0	90 <b>393</b> 55	0 0	90 731 55	1 0 1 1 0 0	90 <b>393</b> 55	0 0	90 731 55	1 0 1 1 0 0	90 <b>393</b> 55
SOUTHBOUND	Left		522 923 126	2 0 1 1 0 0	287 525 126	9 0 0	531 923 126	292 525 126	72 110 2	604 1052 131	2 0 1 1 0 0	<b>332</b> 592 131	9 0	613 1052 131	2 0 1 1 0 0	<b>337</b> 592 131	0 0 0	613 1052 131	2 0 1 1 0 0	<b>337</b> 592 131
EASTBOUND	<ul> <li>✓ Left</li> <li>→ Left-Through</li> <li>→ Through-Right</li> <li>→ Right</li> <li>✓ Left-Through-Right</li> <li>✓ Left-Right</li> </ul>		263 654 286	1 0 1 1 0 0	<b>263</b> 470 286	0 1 0	263 655 286	<b>263</b> 471 286	4 50 10	272 717 302	1 0 1 1 0 0	<b>272</b> 510 302	0 1 0	272 718 302	1 0 1 1 0 0	<b>272</b> 510 302	0 0	272 718 302	1 0 1 1 0 0	<b>272</b> 510 302
WESTBOUND	Left Left-Through Through-Right Right Left-Through-Right Left-Through-Right		131 442 316	1 0 1 0 1 0	131 <b>442</b> 29	0 0 1	131 442 317	131 <b>442</b> 25	4 20 34	138 471 356	1 0 1 0 1 0	138 <b>471</b> 24	0 0 1	138 471 357	1 0 1 0 1 0	138 <b>471</b> 20	0 0	138 471 357	1 0 1 0 1 0	138 <b>471</b> 20
	CRITICAL V			th-South: ast-West: SUM:	659 705 1364		rth-South: East-West: SUM:	664 705 1369			th-South: ast-West: SUM:	725 743 1468			th-South: ast-West: SUM:				th-South: ast-West: SUM:	730 743 1473
V/C	VOLUME/CAPACITY (V/C C LESS ATSAC/ATCS ADJUS LEVEL OF SERVIC	STMENT:			0.992 0.892 D			0.996 0.896 D				1.068 <b>0.968</b> E				1.071 <b>0.971</b> E				1.071 <b>0.971</b> E

REMARKS:

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.003  $\Delta v/c$  after mitigation: 0.003 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Roberts	on Boulevar	ď		Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	,
2	East-West Street:	National	Boulevard			Proje	ction Year	2018		Pea	ak Hour:	PM	Revie	wed by:	R	RA	Project:		RA491	
	posed Ø'ing: N/S-1, E/W-2 o Turns: FREE-1, NRTOR-2 o ATSAC-1 or ATSAC+	r OLA-3? ATCS-2?	NB 0 EB 0	SB WB	4 0 0 3 2	NB EB	0 SE 0 W	B 3 2	NB EB	0 0	SB WB	4 0 0 3 2	NB EB	0	SB WB	4 0 0 3 2	NB EB	0	SB WB	4 0 0 3 2
	Override	Capacity	EVIETI	NG CONDI	O TION	EVICT	ING PLUS P	0	FUTUR	E CONDITI	ON W/O PR	0	FUTUE	RE CONDIT	ION W/ DD	0 0.IECT	FUTUR	W/ PROJE	CT W/ MIT	O ICATION
	MOVEMENT		EXIST	No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Project	Total	No. of	Lane	Added	Total	No. of	Lane
			Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
NORTHBOUND	Left Left-Through Through-Right Right Left-Through-Right		40 480 138	1 0 1 1 0	40 <b>309</b> 138	0 0	40 480 138	40 <b>309</b> 138	11 19 59	52 509 200	1 0 1 1 0	52 <b>355</b> 200	0 0	52 509 200	1 0 1 1 0 0	52 <b>355</b> 200	0 0	52 509 200	1 0 1 1 0 0	52 <b>355</b> 200
	Left-Right  Left Left-Through		644	0 2 0	354	4	648	356	53	710	0 2 0	391	4	714	2 0	393	0	714	2 0	393
SOUTHBOUND	→ Through → Through-Right → Right → Left-Through-Right → Left-Right		970 206	1 1 0 0	588 206	0	970 206	588 206	63 3	1052 213	1 1 0 0	633 213	0	1052 213	1 1 0 0	633 213	0	1052 213	1 1 0 0	633 213
EASTBOUND	→ Left     → Left-Through     → Through		150 938 81	1 0 1 1 0 0	150 <b>510</b> 81	0 0	150 938 81	150 <b>510</b> 81	2 46 14	155 1003 97	1 0 1 1 0 0	155 <b>550</b> 97	0 0	155 1003 97	1 0 1 1 0 0	155 <b>550</b> 97	0 0	155 1003 97	1 0 1 1 0 0	155 <b>550</b> 97
WESTBOUND	← Left  C Left-Through  ← Through-Right  Right  Left-Through-Right  Left-Right		88 289 303	1 0 1 0 1 0	88 289 0	0 1 5	88 290 308	88 290 0	9 40 49	99 335 358	1 0 1 0 1 0	99 335 0	0 1 5	99 336 363	1 0 1 0 1 0	99 336 0	0 0	99 336 363	1 0 1 0 1 0	99 336 0
	CRITICAL V			th-South: ast-West: SUM:	663 598 1261		erth-South: East-West: SUM:	665 598 1263			th-South: ast-West: SUM:	746 649 1395			th-South: ast-West: SUM:				th-South: ast-West: SUM:	748 649 1397
V/0	VOLUME/CAPACITY (V/C	STMENT:			0.917 <b>0.817</b>			0.919 <b>0.819</b>				1.015 <b>0.915</b>				1.016 <b>0.916</b>				1.016 <b>0.916</b>
	LEVEL OF SERVIO			D			D				E				Е				E	

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project: 0.001 Significant impacted? NO

 $\Delta v/c$  after mitigation: 0.001



(Circular 212 Method)



I/S #:	North-South Street:	National	Boulevard			Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
3	East-West Street:	I-10 Free	way Eastbo	und On-	Ramp		ction Year				ak Hour:	AM		wed by:		RA	Project:		RA491	
		f Phases			2	,		2				2				2	,			2
Орр	posed Ø'ing: N/S-1, E/W-2 or	Both-3?	NB 0	60	0 2	N/C	0 0	0	ME	0	65	0 2	ME	0	65	0	N/C	0	66	0 2
Right	Turns: FREE-1, NRTOR-2 or	OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SE 0 W		NB EB	0	SB WB	0	NB EB	0	SB WB	2	NB EB	0	SB WB	0
	ATSAC-1 or ATSAC+A				2			2				2				2			1	2
	Override (	Capacity	EVICE		0	EV/OT		0	=11=115	- 00MDIT	01111110 DD	0				0	======			0
	MOVEMENT		EXISTI	NG CONDI	Lane	Project	ING PLUS PI		Added	E CONDITI Total	No. of	Lane	Project	RE CONDIT	No. of	Lane	Added	W/ PROJE	No. of	Lane
	mo vemerr		Volume	Lanes	Volume	Traffic	Total Volume	Lane Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
	↑ Left		35	1	35	1	36	36	33	69	1	69	1	70	1	70	0	70	1	70
I i	Left-Through		000	0	450	_	004	450		070	0	400		000	0	400		000	0	400
ВО	↑ Through ↑ Through-Right		903	2 0	452	1	904	452	58	979	2 0	490	1	980	2	490	0	980	2	490
NORTHBOUND	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	Left-Through-Right			0							0				0				0	
	→ Left-Right		<b>I</b>	0							0				0				0	
	↓ Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
N N	→ Left-Through			0							0				0				0	
BOL	<ul><li>↓ Through</li><li>✓ Through-Right</li></ul>		<b>720</b>	2 0	360	10	730	365	130	864	2 0	432	10	874	2	437	0	874	2	437
Ĕ	✓ Right		450	1	450	0	450	450	15	474	1	474	0	474	1	474	0	474	1	474
SOUTHBOUND	Left-Through-Right			0							0				0				0	
0,	↓ Left-Right			0							0				0				0	
1	ے Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	→ Left-Through			0					_		0		_		0				0	
300	→ Through  → Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
EASTBOUND	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
E	Left-Through-Right			0							0				0				0	
	- ≺ Left-Right		I	0							0				0				0	
	√ Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
WESTBOUND				0			0	0		0	0	0		0	0	0			0	0
BOI	← Through ← Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
ST	Right		0	0	0	0	0	0	0	0	0	0	0	0	Ö	0	0	0	0	0
N N	Left-Through-Right Left-Right			0 0							0 0				0				0	
	↓ Len-Right		Nor	th-South:	485	No	rth-South:	486	l	Nor	th-South:	543	l	Nor	th-South:	544		Nor	th-South:	544
	CRITICAL VO	OLUMES		ast-West:	0		East-West:	0			ast-West:	0			ast-West:	0			ast-West:	0
	VOLUMEIOARAGIEV 272	\ DAT'O		SUM:			SUM:	486			SUM:	543			SUM:		-		SUM:	
,	VOLUME/CAPACITY (V/C)				0.323			0.324				0.362				0.363				0.363
V/C	LESS ATSAC/ATCS ADJUS				0.223			0.224				0.262				0.263				0.263
	LEVEL OF SERVICE			Α			Α				Α				Α				Α	

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.001  $\Delta v/c$  after mitigation: 0.001 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	National	Boulevard			Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	7
3	East-West Street:	I-10 Free	way Eastbo	und On-l	Ramp		ction Year				ak Hour:	PM		wed by:		RA	Project:		RA491	
		f Phases			2			2				2				2	,			2
Ор	posed Ø'ing: N/S-1, E/W-2 or	Both-3?	NB 0	66	0 2		0 0	0	ME	0	65	0 2	ME	0	65	0	N/D	0	66	0 2
Right	Turns: FREE-1, NRTOR-2 or	OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SI 0 W		NB EB	0	SB WB	0	NB EB	0	SB WB	2	NB EB	0	SB WB	0
	ATSAC-1 or ATSAC+				2			2				2				2			1	2
	Override	Capacity	EVICE		0	5)//OT		0	=11=115	- 00MDIT	01111110 DD	0				0				0
	MOVEMENT		EXISTI	NG CONDI	Lane	Project	ING PLUS P		Added	E CONDITI Total	No. of	Lane	Project	RE CONDIT	No. of	Lane	Added	W/ PROJE	No. of	Lane
	mo v Emerci		Volume	Lanes	Volume	Traffic	Total Volume	Lane Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
	↑ Left		116	1	116	5	121	121	67	185	1	185	5	190	1	190	0	190	1	190
Š	← Left-Through		07.4	0			000	0.40		705	0	000		70.4	0	000		70.4	0	000
ВО	↑ Through ↑ Through-Right		674	2 0	337	6	680	340	97	785	2 0	393	6	791	2	396	0	791	2	396
NORTHBOUND	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Š	← Left-Through-Right			0							0				0				0	
			<b>I</b>	0							0				0				0	
	- Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SOUTHBOUND	→ Left-Through			0							0				0				0	
BOL	↓ Through		971	2 0	486	4	975	488	105	1096	2 0	548	4	1100	2	550	0	1100	2	550
王	→ Right		712	1	712	0	712	712	53	779	1	779	0	779	1	779	0	779	1	779
300	Left-Through-Right			0							0				0				0	
٠,	↓ Left-Right		L	0							0				0				0	
	ے Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	→ Left-Through			0							0				0				0	
JO.	→ Through  → Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
EASTBOUND	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
EA	Left-Through-Right			0							0				0				0	
	-		I	0							0				0				0	
	√ Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
WESTBOUND				0						•	0				0				0	
BOL	← Through ← Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
ST	Right  Left-Through-Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
WE	,			0 0							0 0				0				0	
	├ Left-Right		Non	th-South:	828	No	rth-South:	833		Nor	th-South:	964		Nor	th-South:	969		Nor	th-South:	969
	CRITICAL VO	OLUMES		ast-West:	0		East-West:	0			ast-West:	0			ast-West:	0			ast-West:	0
	VOLUME (0			SUM:	828		SUM:	833			SUM:	964			SUM:				SUM:	
	VOLUME/CAPACITY (V/C	•			0.552			0.555				0.643				0.646				0.646
V/C	C LESS ATSAC/ATCS ADJUS				0.452			0.455				0.543				0.546				0.546
	LEVEL OF SERVIC	E (LOS): MARKS:	<u> </u>		Α			Α				Α				Α				Α

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in *v/c* due to project: 0.003

Significant impacted? NO

 $\Delta v/c$  after mitigation: 0.003 Fully mitigated? N/A

int3_Calcadb.xls



(Circular 212 Method)



	JECT W/ MITIGATION
No. of Phases   Opposed Ø'ing: N/S-1, E/M-2 or Both-3?   Right Turns: FREE-1, NRTOR-2 or OLA-3?   NB 0   SB 0   NB	SB  WB    SB  WB    No. of   Lanes   Volun     7
Right Turns: FREE-1, NRTOR-2 or OLA-3?   NB   0   SB   0   NB   0   NB   0   SB   0   NB   0   NB   0   NB   0   N	SBWB  No. of Lanes Volun  1 7 0 29 1 1 0 0 0 0
Right Turns: FREE-1, NRTOR-2 of OLA-37   ATSAC+1 or ATSAC+ATCS-2?	WB  DECT W/ MITIGATION  No. of Lanes Volum  1 7 0 0 0 29 11 0 0 0
ATSAC-1 or ATSAC+ATCS-2? Override Capacity	No. of   Lane   Volum   1   7   0   29   1   0   0   0   0   0   0   0   0   0
EXISTING CONDITION   EXISTING PLUS PROJECT   FUTURE CONDITION W/O PROJECT   FUTURE CONDITION W/PROJECT   FUTURE CONDITION W/PROJEC	No. of   Lane   Volum
MOVEMENT   No. of   Lane   Volume   Lanes   Volume   Lane   Volume   Volu	No. of Lanes Volum  1
Volume   Lanes   Volume   Traffic   Volume   Volume   Volume   Volume   Volume   Lanes   Volume   Lanes   Volume   Volume   Volume   Volume   Lanes   Volume   Lanes   Volume   Lanes   Volume   Volume   Volume   Volume   Lanes   Volume   Lanes   Volume	Lanes   Volum
Left	1 7 0 29 1 0 0 0
Left-Through Through Through Right Left-Right  Description  Descriptio	0 0 29 1 0 0 0
Left-Right 0 0 0 0 0	1 0 0 0 0
Left-Right 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0
Left-Right 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0
Left-Right 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 6
Left 64 0 64 0 64 1 66 0 66 0 66 0 66 0 66 0	
Left   64   0   64   0   64   1   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66   0   66	
=	_
Through 246 0 452 0 246 452 3 254 0 466 0 254 0 466 0 254	0 46
$\frac{\mathbf{H}}{\mathbf{H}}$ $\leftarrow$ Through-Right 0 0	0
	0
Co Left-Inrough-Right 0 0	0
J Left 60 1 60 0 60 60 3 64 1 64 0 64 1 64 0 64 1 64 0 64 1 9 64 1 9 64 1 1 64 0 64 1 1 64 0 64 1 1 64 0 64 1 1 64 0 64 1 1 64 0 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64 1 1 64	1 6
2	2 53
maximum 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1
Right 26 0 26 0 26 0 34 61 0 61 0 61 0 61	0 6
Left-Through-Right 0 0 0 0 0	0
C Left 53 1 53 0 53 53 2 56 1 56 0 56 1 56 0 56	1 5
Q D S D S D S D S D S D S D S D S D S D	0 3 <b>53</b>
□ 11100gh 1445	0
Right 30 1 30 0 30 30 1 32 0 32 1 32 0 32 1 32 0 32 1 32 0 32 0	
Left-Through-Right  0 0 0 0 0	0
,g	orth-South: 53
CRITICAL VOLUMES East-West: 542 East-West: 543 East-West: 594 East-West: 595	East-West: 59
SUM: 1061 SUM: 1062 SUM: 1130 SUM: 1131	<b>SUM:</b> 113
VOLUME/CAPACITY (V/C) RATIO:         0.772         0.772         0.822	0.82
V/C LESS ATSAC/ATCS ADJUSTMENT: 0.672 0.672 0.722 0.723	0.72
LEVEL OF SERVICE (LOS):  B B C C C	С

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.001  $\Delta v/c$  after mitigation: 0.001 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street: Bag	ley Avenue			Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
4		ice Boulevard				ction Year				ak Hour:	PM		wed by:		RA	Project:		RA491	
	No. of Pha			4			4				4				4	,			4
Op	posed Ø'ing: N/S-1, E/W-2 or Both		65	0		0 0	0 3 0	ME	0	65	0	ME	0	65	0	N/C	0	65	0
Right	Turns: FREE-1, NRTOR-2 or OLA	3?   NB   0 EB   0	SB WB	0	NB EB	0 SI 0 W		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	ATSAC-1 or ATSAC+ATCS			2		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2				2			<del>-</del>	2				2
	Override Capa			0			0				0				0				0
	MOVEMENT	EXIST	No. of			ING PLUS P		Added	E CONDITI Total	ON W/O PR			RE CONDIT	No. of		Added	W/ PROJE	No. of	
	IIIO V LINLIY I	Volume	Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Volume	Volume	No. of Lanes	Lane Volume	Project Traffic	Volume	Lanes	Lane Volume	Volume	Volume	Lanes	Lane Volume
	↑ Left	51	1	51	0	51	51	10	62	1	62	0	62	1	62	0	62	1	62
	← Left-Through		0					_		0		_		0		_		0	
ВО	↑ Through ↑ Through-Right	113	0	150	0	113	150	2	117	0 1	158	0	117	0	158	0	117	0 1	158
NORTHBOUND	Right	37	0	0	0	37	0	3	41	0	0	0	41	0	0	0	41	0	0
Š	← Left-Through-Right		0				_			0	_			0	_			0	
			0							0				0				0	
	Left	64	0	64	0	64	64	1	66	0	66	0	66	0	66	0	66	0	66
N O	├─ Left-Through	04	0	04		04	0-1		00	0	00		00	0	00		00	0	00
SOUTHBOUND	Through	271	0	406	0	271	406	1	277	0	417	0	277	0	417	0	277	0	417
l 품	← Through-Right  → Right	71	0	0	0	71	0	2	74	0 0	0	0	74	0	0	0	74	0	0
.no	Left-Through-Right	/1	1	U		/ 1	U	2	74	1	U		74	1	0		14	1	0
S	↓ Left-Right		0							0				0				0	
		117	1	117	0	117	117	1	120	1	120	0	120	1	120	0	120	1	120
₽	→ Left-Through	117	0	117		117	117		120	0	120	0	120	Ó	120		120	0	120
l o	→ Through	1248	2	436	5	1253	438	148	1421	2	505	5	1426	2	507	0	1426	2	507
EASTBOUND	→ Through-Right → Right	61	1	61	0	61	61	33	95	1 0	95	0	95	1 0	95	0	95	1 0	95
EAS	Left-Through-Right	61	0	01		01	01	33	90	0	90		90	0	90		90	0	95
	- deft-Right - deft-Right		0							0				0				0	
	√ Left	112	1	112	0	112	112	2	116	1	116	0	116	1	116	0	116	1	116
Q.		112	0	112		112	112	_	110	0	110		110	Ó	110		110	0	110
WESTBOUND	← Through	1620	3	540	14	1634	545	182	1835	3	612	14	1849	3	616	0	1849	3	616
TB	← Through-Right ← Right	45	0 1	45	0	45	45	1	47	0 1	47	0	47	0	47	0	47	0	47
VES	Right Left-Through-Right	45	0	40		40	40		47	0	4/		47	0	41		47	0	47
	├ Left-Right		0							0				0				0	
			457 657		rth-South: East-West:	457 662			th-South: ast-West:	479 732			th-South: ast-West:	479 736			th-South: ast-West:	479 736	
	CKITICAL VOLUN	E3   E	:ast-west: SUM:		'	:ast-west SUM:	1119		E	ast-west: SUM:	732 1211		E	ast-west: SUM:			E	ast-west: SUM:	
	VOLUME/CAPACITY (V/C) RAT	IO:		0.810			0.814				0.881				0.884				0.884
V/0	C LESS ATSAC/ATCS ADJUSTME	NT:		0.710			0.714				0.781				0.784				0.784
	LEVEL OF SERVICE (LOS):			С			С				С				С				С
<u> </u>	LEVEL OF SERVICE (LOS):  REMARKS:							-				·							

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.003  $\Delta v/c$  Significant impacted? NO

 $\Delta v/c$  after mitigation: 0.003 Fully mitigated? N/A

1/24/2017-5:29 PM 2 int4_Calcadb.xls



(Circular 212 Method)



I/S #:	North-South Street:	Culver B	oulevard			Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
5	East-West Street:	Venice B	Boulevard				ction Year				ak Hour:	AM		wed by:		RA	Project:		RA491	
		Phases			4			4				4				4	,			4
Орр	posed Ø'ing: N/S-1, E/W-2 or	Both-3?	ND 3	66	1	N/C	2 2	1	ME	0	66	1	NE	0	66	1	ME	0	66	1
Right	Turns: FREE-1, NRTOR-2 or	OLA-3?	NB 3 EB 0	SB WB	0	NB EB	3 SE 0 W		NB EB	3	SB WB	0	NB EB	3	SB WB	0	NB EB	3	SB WB	0
	ATSAC-1 or ATSAC+A	ATCS-2?		2	2			2			2	2				2			2	2
	Override (	Capacity			0			0				0				0				0
	MOVEMENT		EXISTI	NG CONDIT			ING PLUS P				ON W/O PR			RE CONDIT				W/ PROJE		
	INIO V EIVIEN I		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
	↑ Left		36	1	36	0	36	36	4	41	1	41	0	41	1	41	0	41	1	41
NORTHBOUND	← Left-Through			0							0				0		-		0	
್ಷ 📗	Through		43	1	43	0	43	43	0	44	1	44	0	44	1	44	0	44	1	44
ͳΪ	Through-Right  Right		683	0 2	196	0	683	196	77	774	0 2	166	0	774	0	166	0	774	0 2	166
S S	← Left-Through-Right		000	0	190		000	190	''	114	0	100		114	0	100		114	0	100
2	Left-Right			0							0				0				0	
	1.04		140	_			440	405		4.40	4	407		4.40		407		440	4	407
9	<ul><li>↓ Left</li><li>↓ Left-Through</li></ul>		143	1 0	105	0	143	105	0	146	1 0	107	0	146	1	107	0	146	1 0	107
l lo	Through		37	0	105	0	37	105	0	38	0	107	0	38	0	107	0	38	0	107
单	→ Through-Right			0					_		0		_		0		_		0	
SOUTHBOUND			29	0 1	0	0	29	0	0	30	0 1	0	0	30	0	0	0	30	0	0
SC	↓ Left-Right			0							0				0				0	
	1																			
۾	<ul><li>J Left</li><li>→ Left-Through</li></ul>		20	1 0	20	0	20	20	0	20	1 0	20	0	20	1	20	0	20	1 0	20
N S	→ Through		1298	3	433	12	1310	437	149	1473	3	491	12	1485	3	495	0	1485	3	495
EASTBOUND	→ Through-Right			0							0				0		-		0	
ASI	Right		13	1 0	0	0	13	0	0	13	1 0	0	0	13	1	0	0	13	1 0	0
ш	★ Left-Through-Right     ★ Left-Right			0							0				0				0	
_	*				=										-					
۵	Left		327	2 0	180	0	327	180	138	472	2 0	260	0	472	2	260	0	472	2	260
WESTBOUND			1538	0 2	560	3	1541	561	117	1686	0 2	610	3	1689	2	611	0	1689	2	611
<u> </u>	Through-Right			1	,,,,					. 300	1	3.0		. 300	1			. 300	1	J.,
ESI	Right Left-Through-Right		141	0	141	0	141	141	0	144	0	144	0	144	0	144	0	144	0	144
>	Left-Through-Right Left-Right			0 0							0 0				0				0	
	North-South: CRITICAL VOLUMES East-West:		301	No	rth-South:	301		Nor	th-South:	273		Nor	th-South:	273		Nor	th-South:	273		
	CRITICAL VO	DLUMES	Ea		613	4	East-West:	617		E	ast-West:	751		E	ast-West:			E	ast-West:	755
	VOLUME/CAPACITY (V/C)	DATIO:		SUM:	914	-	SUM:	918			SUM:	1024			SUM:				SUM:	
1//0	C LESS ATSAC/ATCS ADJUS				0.665			0.668				0.745				0.748				0.748
V/C					0.565			0.568				0.645 B				0.648				0.648
<u></u>	LEVEL OF SERVICE (LOS):  REMARKS:				Α	<u> </u>		Α				R				В				В

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.003  $\Delta v/c$  after mitigation: 0.003 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Culver Bo	oulevard			Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	,
5	East-West Street:	Venice Bo	oulevard			Proje	ction Year	2018		Pea	ak Hour:	PM	Revie	wed by:	R	RA.	Project:		RA491	
Ор	No. of posed Ø'ing: N/S-1, E/W-2 or E				4			4				4				4				4
Right	Turns: FREE-1, NRTOR-2 or 0	DI A-37	NB 3 EB 0	SB WB	0	NB EB	3 SE 0 WE		NB EB	3	SB WB	0	NB EB	3 0	SB WB	0	NB EB	3	SB WB	0
	ATSAC-1 or ATSAC+A	TCS-2?			2		VVE	2		- 0	****	2		0		2			***	2
	Override C	apacity			0	_		0	_			0	_			0				0
	MOVEMENT		EXISTI	NG CONDIT			NG PLUS PF				ON W/O PR			RE CONDIT				W/ PROJE		
	IVIOVEIVIENI		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
	↑ Left		76	1	76	0	76	76	22	100	1	100	0	100	1	100	0	100	1	100
NORTHBOUND	← Left-Through			0							0				0				0	
301	Through		47	1	47	0	47	47	0	48	1	48	0	48	1	48	0	48	1	48
ΙË	Through-Right		819	0 2	240	0	819	240	216	1051	0 2	313	0	1051	0 2	313	0	1051	0 2	313
OR			018	0	240		งเฮ	240	210	1001	0	313	U	1001	0	313		1001	0	313
Z	Left-Right			0							0				0				0	
			201				201			225				205		4.45		200		4.45
9			231	1 0	145	0	231	145	0	236	1 0	148	0	236	1 0	148	0	236	1 0	148
SOUTHBOUND	Through		35	0	145	0	35	145	0	36	0	148	0	36	0	148	0	36	0	148
Η̈́B	← Through-Right			0							0				0				0	
∏ T)			23	0 1	0	0	23	0	0	23	0 1	0	0	23	0	0	0	23	0	0
SC	↓ Left-Right			0							0				0				0	
	•				=															
۵	J Left		9	1 0	9	0	9	9	0	9	1 0	9	0	9	1	9	0	9	1 0	9
N Z	→ Left-Inrough		1202	3	401	5	1207	402	152	1378	3	459	5	1383	3	461	0	1383	3	461
.BO	→ Through-Right			0			0,				0	,00		. 500	Ō			. 500	0	
EASTBOUND	Right		17	1	0	0	17	0	0	17	1	0	0	17	1	0	0	17	1	0
Э				0 0							0 0				0				0	
	) Lon-Night																			
	√ Left		381	2	210	0	381	210	93	482	2	265	0	482	2	265	0	482	2	265
WESTBOUND			1611	0 2	580	14	1625	585	162	1805	0 2	646	14	1819	0	650	0	1819	0 2	650
ВО	Through-Right		1011	1	360	14	1023	505	102	1000	1	040	14	1019	1	000		1019	1	030
EST	Right		129	0	129	0	129	129	0	132	0	132	0	132	0	132	0	132	0	132
×	Left-Through-Right			0							0				0				0	
	├ Left-Right		Nor	th-South:	385	No	rth-South:	385		Nor	th-South:	461		Non	th-South:	461		Non	th-South:	461
	CRITICAL VO	LUMES		ast-West:	611		ast-West:	612			ast-West:	724			ast-West:	726			ast-West:	726
				SUM:	996		SUM:	997			SUM:	1185			SUM:	1187			SUM:	1187
	VOLUME/CAPACITY (V/C)				0.724			0.725				0.862				0.863				0.863
V/0	C LESS ATSAC/ATCS ADJUST				0.624			0.625				0.762				0.763				0.763
	LEVEL OF SERVICE	(LOS):			В			В				С				С				С
	REM	IARKS:																		

Version: 1i Beta; 8/4/2011

### PROJECT IMPACT

Change in v/c due to project: 0.001  $\Delta v/c$  after mitigation: 0.001 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Robertse	on Boulevar	ď		Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	R	RA.	Date:		1/24/2017	
6	East-West Street:	Venice E	Boulevard			Proje	ction Year	2018		Pea	ak Hour:	AM		wed by:	R	RA.	Project:		RA491	
Ор	No. o posed Ø'ing: N/S-1, E/W-2 o	of Phases or Both-3?			4 1			4				4 1				4 1				4 1
Right	Turns: FREE-1, NRTOR-2 o	r OLA-3?	NB 3	SB	0	NB	3 SE		NB	3	SB	0	NB	3	SB	0	NB	3	SB	0
	ATSAC-1 or ATSAC-	ATCS-22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	0	WB	0 2	EB	0	WB	0 2	EB	0	WB	0 2
		Capacity			0			0				0				0				0
			EXISTI	NG CONDI	TION	EXIST	ING PLUS PI	ROJECT	FUTUR	E CONDITI	ON W/O PR	OJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MITI	GATION
	MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Project	Total	No. of	Lane	Added	Total	No. of	Lane
	<u> </u>		Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
₽	↑ Left  Left-Through		80	1 0	80	3	83	83	17	99	1 0	99	3	102	1 0	102	0	102	1 0	102
NORTHBOUND	↑ Through		380	2	190	2	382	191	16	404	2	202	2	406	2	203	0	406	2	203
¥	Through-Right			0							0				0				0	
R	Right		42	1	0	0	42	0	2	45	1	0	0	45	1	0	0	45	1	0
2	Left-Through-Right			0							0				0				0	
			<u> </u>	0							0				0				0	
	Left		233	1	233	0	233	233	74	312	1	312	0	312	1	312	0	312	1	312
l ₹	→ Left-Through			0							0				0				0	
l g	Through		<b>253</b>	1	253	8	261	261	85	343	1	343	8	351	1	351	0	351	1	351
IE	← Through-Right  → Right		372	0 1	269	0	372	269	116	495	0 1	379	0	495	0	379	0	495	0	379
SOUTHBOUND	Left-Through-Right		3/2	0	209	"	312	209	110	490	0	319	U	490	0	319		495	0	319
S	↓ Left-Right			0							0				0				0	
	Left						075		00	400				400				100	0	
Ω	→ Left → Left-Through		375	2 0	206	0	375	206	39	422	2 0	232	0	422	2	232	0	422	2	232
3	→ Through		1586	3	529	0	1586	529	163	1781	3	594	0	1781	3	594	0	1781	3	594
EASTBOUND	→ Through-Right			0							0				0				0	
ASI	Right		64	1 0	24	12	76	35	25	90	1	41	12	102	1	51	0	102	1	51
ш	<ul><li></li></ul>			0							0				0 0				0	
	Lett-right			,																
	√ Left		45	1	45	0	45	45	13	59	1	59	0	59	1	59	0	59	1	59
WESTBOUND			1404	0 3	47.6		4404	47.4	400	4570	0	504		4570	0 3	504		4570	0 3	504
B01	← Through ← Through-Right		1421	3 0	474	0	1421	474	122	1572	3 0	524	0	1572	0	524	0	1572	0	524
STI	Right		187	1	71	0	187	71	32	223	1	67	0	223	1	67	0	223	1	67
WE	Left-Through-Right			0							0				0				0	
-	├ Left-Right		A1	0 45 Carrette	450		with Count's	460		A/	0 45 Carrette	E04		M	0 4h Carreta	E00		M	0	582
	CRITICAL V	OLUMES		th-South: ast-West:	459 680		rth-South: East-West:	460 680			th-South: ast-West:	581 756			th-South: ast-West:	582 756			th-South: ast-West:	582 756
				SUM:	1139		SUM:	1140			SUM:	1337			SUM:	1338	<u> </u>		SUM:	1338
	VOLUME/CAPACITY (V/C	C) RATIO:			0.828			0.829				0.972				0.973				0.973
V/0	C LESS ATSAC/ATCS ADJU	STMENT:			0.728			0.729				0.872				0.873				0.873
	LEVEL OF SERVI	CE (LOS):			С			С				D				D				D
		FMARKS:	-			•			•				•				•			

REMARKS:

Version: 1i Beta; 8/4/2011

### PROJECT IMPACT

Change in v/c due to project: 0.001  $\Delta v/c$  after mitigation: 0.001 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Robertso	n Boulevar	d		Yea	r of Count	2016	Amb	ient Grov	wth: (%):	1	Condu	cted by:	R	RA.	Date:		1/24/2017	,
6	East-West Street:	Venice B	oulevard			Proje	ction Year	2018		Pe	ak Hour:	PM	Revie	wed by:	R	RA	Project:		RA491	
		Phases			4			4				4				4				4
Ор	posed Ø'ing: N/S-1, E/W-2 or I	Both-3?			1		0 0	1		0		1		0		1		0		1
Right	Turns: FREE-1, NRTOR-2 or	OLA-3?	NB 3 EB 0	SB WB	0	NB EB	3 SE 0 WI		NB EB	3	SB WB	0	NB EB	3	SB WB	0	NB EB	3	SB WB	0
	ATSAC-1 or ATSAC+A	ATCS-2?	LB	WD	2	LD	0 772	2	Lb	U	W.D	2	LD	U	W <i>D</i>	2		U	WD	2
	Override C	Capacity			0			0				0				0				0
			EXISTI	NG CONDIT	TION	EXIST	NG PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PR	OJECT	FUTUE	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
	MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Project	Total	No. of	Lane	Added	Total	No. of	Lane
	5 1 "		Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
Q			98	1 0	98	14	112	112	42	142	1 0	142	14	156	1 0	156	0	156	1 0	156
1	↑ Through		349	2	175	9	358	179	50	406	2	203	9	415	2	208	0	415	2	208
BC	↑ Through-Right		0.0	0			000			.00	0	200			0	200			0	200
NORTHBOUND	Right		63	1	1	0	63	1	8	72	1	0	0	72	1	0	0	72	1	0
Į į	← Left-Through-Right			0							0				0				0	
	← Left-Right			0							0				0				0	
	└ Left		162	1	162	0	162	162	46	211	1	211	0	211	1	211	0	211	1	211
N N	Left-Through		102	0	102	0	102	102	40	211	Ö	211	U	211	0	211	"	211	0	211
OO	Through		164	1	164	3	167	167	59	226	1	226	3	229	1	229	0	229	1	229
Η̈́	← Through-Right			0							0				0				0	
SOUTHBOUND	→ Right		347	1	223	0	347	223	60	414	1	256	0	414	1	256	0	414	1	256
SO	← Left-Through-Right			0 0							0 0				0				0	
	Leit-Right			U											<u> </u>				0	
	J Left		450	2	248	0	450	248	118	577	2	317	0	577	2	317	0	577	2	317
N N	→ Left-Through			0							0				0				0	
l o	→ Through → Through-Right		1748	3 0	583	0	1748	583	208	1991	3 0	664	0	1991	3 0	664	0	1991	3 0	664
EASTBOUND	→ Through-Right → Right		98	1	49	5	103	47	42	142	1	71	5	147	1	69	0	147	1	69
EA8	Left-Through-Right		•	0	.0		100	.,			0				0	00			0	00
	- Left-Right			0							0				0				0	
	C 1-6		00	4	00		00	00	4.4										4	
₽			62	1 0	62	0	62	62	14	77	1 0	77	0	77	1 0	77	0	77	1 0	77
WESTBOUND	← Through		1450	3	483	0	1450	483	158	1637	3	546	0	1637	3	546	0	1637	3	546
BC	Through-Right			0							0		_		0				0	
ESI	Right		106	1	25	0	106	25	70	178	1	73	0	178	1	73	0	178	1	73
×	Left-Through-Right			0							0				0				0	
<u> </u>	├─ Left-Right		Nor	th-South:	398	No	rth-South:	402		Nor	th-South:	459		Nor	th-South:	464		Non	th-South:	464
	CRITICAL VO	DLUMES		ast-West:	731		ast-West:	731			ast-West:	863			ast-West:	863			ast-West:	863
				SUM:	1129		SUM:	1133			SUM:	1322			SUM:				SUM:	1327
	VOLUME/CAPACITY (V/C)	RATIO:			0.821			0.824				0.961				0.965				0.965
V/C	C LESS ATSAC/ATCS ADJUST	TMENT:			0.721			0.724				0.861				0.865				0.865
	LEVEL OF SERVICE	E (LOS):			С			С				D				D				D
<u></u>	REN	NARKS:							1											

Version: 1i Beta; 8/4/2011

### PROJECT IMPACT

Change in v/c due to project: 0.004 Significant impacted? NO

 $\Delta v/c$  after mitigation: 0.004 Fully mitigated? N/A

1/24/2017-5:40 PM 2 int6_Calcadb.xls



(Circular 212 Method)



I/S #:	North-South Street:	National I	Boulevard			Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
7	East-West Street:	Venice Bo	oulevard				ction Year				ak Hour:	AM		wed by:		RA	Project:		RA491	
	No. of F				4			4				4				4	,			4
Opp	posed Ø'ing: N/S-1, E/W-2 or B		ND 0	ee.	0		0 0	0 3 0	ME	0	60	0	ME	0	66	0	ME	0	65	0
Right	Turns: FREE-1, NRTOR-2 or C		NB 0 EB 0	SB WB	0	NB EB	0 SE 0 W		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	ATSAC-1 or ATSAC+AT	TCS-2?			2			2				2				2				2
	Override Ca	apacity	=V10=11		0	5)//OT		0	=11=11=	- 00MDIT		0				0				0
	MOVEMENT	-	EXISTI	NG CONDIT	Lane	Project	ING PLUS PI		Added	Total	ON W/O PR	Lane	Project	RE CONDIT	No. of	Lane	Added	W/ PROJE	No. of	Lane
	mo v Emerci		Volume	Lanes	Volume	Traffic	Volume	Lane Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
	↑ Left		238	1	238	0	238	238	75	318	1	318	0	318	1	318	0	318	1	318
l i	Left-Through		074	0	050		070	0.55	_,		0	400			0	40.4	•		0	404
BO	↑ Through ↑ Through-Right		671	1 1	353	2	673	355	71	755	1 1	402	2	757	1	404	0	757	1	404
NORTHBOUND	→ Right		34	0	34	2	36	36	14	49	0	49	2	51	0	51	0	51	0	51
Š	Left-Through-Right			0							0				0				0	
	← Left-Right			0							0				0				0	
	. Left	I	95	1	95	0	95	95	0	97	1	97	0	97	1	97	0	97	1	97
SOUTHBOUND	→ Left-Through			0							0				0				0	
BOL	Through		590	1	332	10	600	337	121	723	1	404	10	733	1	409	0	733	1	409
I ₹ I	← Through-Right  → Right		74	0	74	0	74	74	9	84	0	84	0	84	0	84	0	84	0	84
000	Left-Through-Right			0							0				0				0	
0,	↓ Left-Right			0							0				0				0	
I	ے Left	I	121	2	67	0	121	67	18	141	2	78	0	141	2	78	0	141	2	78
2	→ Left-Through			0							0				0				0	
l g	→ Through  → Through-Right		1412	3 0	471	0	1412	471	43	1483	3 0	494	0	1483	3 0	494	0	1483	3 0	494
EASTBOUND	Right		446	1	327	0	446	327	155	610	1	451	0	610	1	451	0	610	1	451
EA	Left-Through-Right			0							0				0				0	
	-			0							0				0				0	
	√ Left	I	68	1	68	8	76	76	43	112	1	112	8	120	1	120	0	120	1	120
WESTBOUND			4005	0	400		4005	400		4077	0	450		4077	0	450		4077	0	450
BOL	← Through ← Through-Right		1265	3 0	422	0	1265	422	84	1374	3 0	458	0	1374	3 0	458	0	1374	3 0	458
ST	Right Left-Through-Right		73	1	26	0	73	26	2	76	1	28	0	76	1	28	0	76	1	28
×	,			0 0							0 0				0				0	
			Non	th-South:	570	No	rth-South:	575		Nor	th-South:	722		Nor	th-South:	727		Nor	th-South:	727
	CRITICAL VOL	LUMES		ast-West:	539	_	East-West:	547			ast-West:	606			ast-West:	614			ast-West:	614
ļ				SUM:	1109		SUM:	1122			SUM:	1328			SUM:				SUM:	1341
	VOLUME/CAPACITY (V/C) I				0.807			0.816				0.966				0.975				0.975
V/C	C LESS ATSAC/ATCS ADJUST				0.707			0.716				0.866				0.875				0.875
	LEVEL OF SERVICE	(LOS): ARKS:			С			С				D				D				D

Version: 1i Beta; 8/4/2011

### PROJECT IMPACT

Change in v/c due to project: 0.009  $\Delta v/c$  af Significant impacted? NO Fu

 $\triangle v/c$  after mitigation: 0.009 Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	National	Boulevard			Yea	r of Count	2016	Amb	ient Grov	wth: (%):	1	Condu	cted by:	R	RA.	Date:		1/24/2017	7
7	East-West Street:	Venice B	oulevard			Proje	ction Year	2018		Pe	ak Hour:	PM	Revie	wed by:	R	RA.	Project:		RA491	
-		Phases			4			4				4				4				4
1	posed Ø'ing: N/S-1, E/W-2 or		NB 0	SB	0	NB	0 SE	0 3 0	NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
Right	Turns: FREE-1, NRTOR-2 or		EB 0	WB	0	EB	0 W	3 0	EB	0	WB	0	EB	0	WB	0	EB	0	WB	0
	ATSAC-1 or ATSAC+A				2			2				2				2				2
	Override (	Бараспу	EXISTI	NG CONDIT		EXIST	NG PLUS PI		FUTUR	E CONDITI	ON W/O PR		FUTUE	RE CONDIT	ION W/ PR	U	FUTURE	W/ PROJE	CT W/ MIT	
	MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Project	Total	No. of	Lane	Added	Total	No. of	Lane
			Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
₽	↑ Left		201	1 0	201	0	201	201	164	369	1 0	369	0	369	1 0	369	0	369	1 0	369
5	← Left-Through ↑ Through		609	1	352	11	620	362	127	748	1	442	11	759	1	452	0	759	1	452
Ř	Through-Right			1							1				1				1	
NORTHBOUND	Right		94	0	94	9	103	103	39	135	0	135	9	144	0	144	0	144	0	144
¥	Left-Through-Right Left-Right			0 0							0 0				0				0	
	Lon ragin																			
₽	Left		141	1 0	141	0	141	141	0	144	1	144	0	144	1 0	144	0	144	1 0	144
5	Left-Through Through		779	1	418	4	783	420	99	894	0 1	479	4	898	1	481	0	898	1	481
Ĕ	Through-Right			1							1				1				1	
SOUTHBOUND	→ Right  → Left-Through-Right		56	0 0	56	0	56	56	7	64	0 0	64	0	64	0	64	0	64	0	64
S	↓ Left-Right			0							0				0				0	
	1																			
Ω			165	2 0	91	0	165	91	33	201	2 0	111	0	201	2	111	0	201	2 0	111
N N	→ Through		1554	3	518	0	1554	518	90	1675	3	558	0	1675	3	558	0	1675	3	558
TBC	Through-Right		0.40	0 1	040	•	0.40	040		4.5-3	0	070		457	0	070		45-	0	070
EASTBOUND	Right  Left-Through-Right		310	0	210	0	310	210	141	457	1 0	273	0	457	0	273	0	457	1 0	273
	- Left-Right			0							0				0				0	
	√ Left		90	1	90	3	93	93	41	133	1	133	3	136	1	136	0	136	1	136
ð			30	0	30		33	33		100	0	133	3	130	Ó	130		130	0	130
WESTBOUND	← Through ← Through-Right		1337	3	446	0	1337	446	84	1448	3	483	0	1448	3	483	0	1448	3	483
STB	Through-Right Right		59	0 1	0	0	59	0	4	64	0 1	0	0	64	U 1	0	0	64	0 1	0
WE	Left-Through-Right		00	0	J				·	01	0	J		O r	0	J		0 1	0	
	├ Left-Right		A1	0 th Couth	619	A/-	rth-South:	621		A1	0	848		A1.c	0 th Carret	850		Me	0 th Couth	850
	CRITICAL VO	DLUMES		th-South: ast-West:	608		rtn-Soutn: East-West:	611			th-South: ast-West:	691			th-South: ast-West:	694			th-South: ast-West:	694
				SUM:	1227		SUM:	1232			SUM:	1539			SUM:				SUM:	1544
	VOLUME/CAPACITY (V/C)				0.892			0.896				1.119				1.123				1.123
V/C	C LESS ATSAC/ATCS ADJUS				0.792			0.796				1.019				1.023				1.023
	LEVEL OF SERVICE	· ,			С			С				F				F				F
	REI	MARKS:																		

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project: 0.004
Significant impacted? NO

 $\Delta v/c$  after mitigation: 0.004 Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	La Ciene	ega Bouleva	rd		Yea	r of Count	2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
8	East-West Street:		Boulevard				ction Year				ak Hour:	AM		wed by:		RA	Project:		RA491	
		of Phases			4			4				4				4	,			4
Орј	posed Ø'ing: N/S-1, E/W-2 or	r Both-3?	ND O	66	0		0 0	0	ME	0	66	0	NE	0	66	0	ME	0	65	0
Right	Turns: FREE-1, NRTOR-2 or	r OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SI		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	ATSAC-1 or ATSAC+	ATCS-2?		2	2			2			2	2				2				2
	Override	Capacity			0			0				0				0				0
	MOVEMENT		EXISTI	NG CONDIT			ING PLUS P				ON W/O PR			RE CONDIT				W/ PROJE		
	IVIO VEIVIEN I		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
_	↑ Left		172	1	172	0	172	172	0	175	1	175	0	175	1	175	0	175	1	175
	← Left-Through			0							0				0				0	
gr	Through		1633	2	563	1	1634	564	61	1727	2	596	1	1728	2	597	0	1728	2	597
NORTHBOUND	↑ Through-Right		57	1 0	57	0	57	57	4	62	1 0	62	0	62	1 0	62	0	62	1 0	62
l S	← Left-Through-Right		<b>0</b> 7	0	0,		01	01	-	02	0	02		02	0	02		02	0	OZ.
	← Left-Right			0							0				0				0	
	Left		110	1	140		110	440	0	120	1	420	0	120	1	120	0	120	1	420
9	→ Leπ ↓ Left-Through		118	1 0	118	0	118	118	0	120	0	120	0	120	0	120	0	120	1 0	120
l o	Through		1160	2	467	2	1162	468	87	1270	2	519	2	1272	2	520	0	1272	2	520
SOUTHBOUND	Through-Right		046	1	0.46		0.46	040		000	1	000		000	1	000		000	1	000
5			242	0 0	242	0	242	242	41	288	0 0	288	0	288	0	288	0	288	0 0	288
Ö	Left-Right			0							0				Ö				0	
	1 1-6			_			6 <b>7</b> 4	4=4		600										
₽			274	2 0	151	0	274	151	22	302	2 0	166	0	302	2	166	0	302	2	166
	→ Through		1187	3	396	2	1189	396	33	1244	3	415	2	1246	3	415	0	1246	3	415
∏ IBC	Through-Right		40-	0			40=		_	100	0			100	0		_	100	0	40
EASTBOUND	Right  Left-Through-Right		127	1 0	41	0	127	41	0	130	1 0	43	0	130	1	43	0	130	1 0	43
"	→ Left-Right			0							0				0				0	
					•	_				,			_	,			_	,		
۵			179	1 0	179	0	179	179	11	194	1 0	194	0	194	1	194	0	194	1 0	194
WESTBOUND	← Through		1234	3	411	8	1242	414	72	1331	3	444	8	1339	3	446	0	1339	3	446
∏ IBΩ	Through-Right			0							0				0				0	
ĘS.	Right Left-Through-Right		85	1 0	26	0	85	26	0	87	1 0	27	0	87	1	27	0	87	1 0	27
\$	Left-Right			0							0				0				0	
	· · ·		_	th-South:	681		rth-South:	682			th-South:	716			th-South:	717			th-South:	717
	CRITICAL V	OLUMES	Ea	ast-West: SUM:	575 1256	1	East-West: SUM:	575 1257		E	ast-West: SUM:	610 1326		E	ast-West: SUM:			E	ast-West: SUM:	612 1329
	VOLUME/CAPACITY (V/C	) RATIO:	<del> </del>	SUIVI:	0.913		SUIVI:	0.914			SUIVI:	0.964			SUIVI:	0.967			SUIVI:	0.967
V/C	C LESS ATSAC/ATCS ADJUS	,			0.913			0.914 <b>0.814</b>				0.964 <b>0.864</b>				0.967 <b>0.867</b>				0.967 <b>0.867</b>
"	LEVEL OF SERVICE				0.813 D			0.814 D				0.864 D				0.867 D				0.867 D
<u> </u>		MARKS:	<u> </u>		U			ע				U				U				ע

Version: 1i Beta; 8/4/2011

### PROJECT IMPACT

Change in v/c due to project: 0.003  $\Delta v/c$  after mitigation: 0.003 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



Right Turns: FREE-1, NRTOR-2 or OLA-3?   EB 0   WB 0   EB 0   EB 0   WB 0	RA 4 0 SB 0 WB 2 0	Project:		RA491	4
Opposed Ø'ing: N/S-1, E/W-2 or Both-3?  Right Turns: FREE-1, NRTOR-2 or OLA-3?  B  O  NB	SB WB 2	NB			4
Right Turns: FREE-1, NRTOR-2 or OLA-3?   EB 0   WB 0   EB 0	<i>WB</i> 0 2				0
	2		0	SB WB	0
ATSAC-1 or ATSAC+ATCS-2? 2 2	0			112-	2
Override Capacity 0 0					0
EXISTING CONDITION EXISTING PLUS PROJECT FUTURE CONDITION W/O PROJECT FUTURE CONDITION			E W/ PROJE		
	No. of Lane Lanes Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
Volume Lanes Volume Traffic Volume Volume Volume Lanes Vo	1 93	O	93	1	93
Q	0		33	0	93
Q	2 385	0	1067	2	385
및 Through-Right 1	1			1	
Lange of the control of the contro	0 89	0	89	0	89
Q ← Left-Through-Right 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0			0	
Letterugik					
□ Left 60 1 60 0 60 0 61 1 61 0 61	1 61	0	61	1	61
Comparison   Co	0 2 576		4.400	0 2	570
□	2 576	0	1493	1	576
Right 199 0 199 0 199 31 234 0 234 0 234	0 234	0	234	0	234
0 ← Left-Through-Right 0	0			0	
60 Left-Right 0	0			0	
Left 286 2 157 0 286 157 47 339 2 186 0 339	2 186	0	339	2	186
	0		000	0	100
3	3 505	0	1515	3	505
QN DOM For Through	0	0	155	0	100
	1 109	U	155	0	109
Left-Right 0	0			Ö	
☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐ ☐	1 180	0	180	1 0	180
Q	3 395	0	1185	3	395
© ↑ Through-Right 0	0			0	
<b>5 Right</b> 29 1 0 0 29 0 0 30 1 0 0 30 0 30 0 0 30 0 0 30 0 0 30 0 0 0 30 0 0 0 30 0 0 0 30 0 0 0 0 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0	0	30	1	0
Left-Through-Right  Left-Right  0  0  0	0			0	
North-South: 620 North-South: 621 North-South: 668 North-			Noi	rth-South:	669
	t-West: 685		E	ast-West:	685
SUM: 1257 SUM: 1261 SUM: 1350	<b>SUM</b> : 1354			SUM:	1354
VOLUME/CAPACITY (V/C) RATIO:         0.914         0.917         0.982	0.985				0.985
V/C LESS ATSAC/ATCS ADJUSTMENT: 0.814 0.817 0.882	0.885				0.885
LEVEL OF SERVICE (LOS): D D D	D				D

REMARKS:

Version: 1i Beta; 8/4/2011

### PROJECT IMPACT

Change in v/c due to project: 0.003  $\Delta v/c$  after mitigation: 0.003 Significant impacted? NO Fully mitigated? N/A

INT # 9

North/South Street: WASHINGTON BOULEVARD-IRVING PLACE

East/West Street: CULVER BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.09	27	137	0.197	N-S(1):	0.288 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.91	603	2,757	0.219 *	E-W(1):	0.268
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.338 *
	TH	3.00	1,623	4,800	0.338 *		
	LT	1.00	43	1,600	0.027	V/C:	0.626
Northbound	RT	1.00	87	1,600	0.028	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.00	110	1,600	0.069 *		
Eastbound	RT	0.00	0	0	0.000	ICU:	0.656
	TH	3.00	1,159	4,800	0.241		
	LT	0.00	0	0	0.000 *	LOS:	В
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT		Volume 18	Capacity 62	0.290	N-S(1):	0.344 *
Approach	Movement	Lanes			0.290 0.000		
Approach Southbound	Movement RT TH LT	Lanes 0.04	18	62	0.290	N-S(1):	0.344 * 0.000 0.274 *
Approach	Movement RT TH LT RT	Lanes 0.04 0.00	18 0 911 0	62 0	0.290 0.000 0.323 * 0.000	N-S(1): N-S(2):	0.344 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 0.04 0.00 1.96	18 0 911	62 0 2,824	0.290 0.000 0.323 *	N-S(1): N-S(2): E-W(1):	0.344 * 0.000 0.274 *
Approach Southbound	Movement RT TH LT RT	0.04 0.00 1.96 0.00	18 0 911 0	62 0 2,824 0	0.290 0.000 0.323 * 0.000	N-S(1): N-S(2): E-W(1):	0.344 * 0.000 0.274 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.04 0.00 1.96 0.00 3.00	18 0 911 0 1,293	62 0 2,824 0 4,800	0.290 0.000 0.323 * 0.000 0.269	N-S(1): N-S(2): E-W(1): E-W(2):	0.344 * 0.000 0.274 * 0.269
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00	18 0 911 0 1,293 33	62 0 2,824 0 4,800 1,600 1,600 0	0.290 0.000 0.323 * 0.000 0.269 0.021 * 0.018 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.344 * 0.000 0.274 * 0.269
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT RT	Lanes 0.04 0.00 1.96 0.00 3.00 1.00	18 0 911 0 1,293 33 61	62 0 2,824 0 4,800 1,600	0.290 0.000 0.323 * 0.000 0.269 0.021 * 0.018	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.344 * 0.000 0.274 * 0.269 0.618 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00	18 0 911 0 1,293 33 61 0	62 0 2,824 0 4,800 1,600 1,600 0	0.290 0.000 0.323 * 0.000 0.269 0.021 * 0.018 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.344 * 0.000 0.274 * 0.269 0.618 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00	18 0 911 0 1,293 33 61 0	62 0 2,824 0 4,800 1,600 1,600 0 1,600	0.290 0.000 0.323 * 0.000 0.269 0.021 * 0.018 0.000 0.021 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.344 * 0.000 0.274 * 0.269  0.618 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00 0.00	18 0 911 0 1,293 33 61 0 34	62 0 2,824 0 4,800 1,600 0 1,600 0	0.290 0.000 0.323 * 0.000 0.269 0.021 * 0.018 0.000 0.021 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.344 * 0.000 0.274 * 0.269  0.618 0.100 -0.070

^{* =} Critical Movement

INT #9

North/South Street: WASHINGTON BOULEVARD-IRVING PLACE

East/West Street: CULVER BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

**AM PEAK HOUR** 

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

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Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.09	27	137	0.197	N-S(1):	0.288 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.91	603	2,757	0.219 *	E-W(1):	0.271
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.339 *
	TH	3.00	1,625	4,800	0.339 *		
	LT	1.00	43	1,600	0.027	V/C:	0.627
Northbound	RT	1.00	87	1,600	0.028	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.00	110	1,600	0.069 *		
Eastbound	RT	0.00	0	0	0.000	ICU:	0.657
		2.00	1,170	4,800	0.244		
	TH	3.00	1,170	7,000	<b>v.</b>		
	TH LT	0.00	0	0	0.000 *	LOS:	В
			•	· ·		LOS:	В
Peak Period:		0.00	•	· ·		LOS:	В
Peak Period: Approach	LT	0.00	•	· ·		LOS:	
	PM PEAK F	0.00 <b>IOUR</b>	0	0	0.000 *		
Approach	PM PEAK F	0.00 HOUR Lanes	0 Volume	0 Capacity	0.000 * V/C	ICU ANA	LYSIS
Approach	PM PEAK F Movement RT	0.00 HOUR Lanes 0.04	Volume 18	0 Capacity 62	0.000 * V/C 0.290	ICU ANA N-S(1):	LYSIS 0.344 *
Approach	PM PEAK F Movement RT TH	0.00 HOUR Lanes 0.04 0.00	Volume 18 0	Capacity 62 0	0.000 *  V/C  0.290  0.000	ICU ANA N-S(1): N-S(2):	LYSIS 0.344 * 0.000
Approach Southbound	PM PEAK H Movement RT TH LT	0.00 HOUR Lanes 0.04 0.00 1.96	0 Volume 18 0 911	0 Capacity 62 0 2,824	0.000 *  V/C  0.290  0.000  0.323 *	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.344 * 0.000 0.275 *
Approach Southbound	PM PEAK F  Movement  RT  TH  LT  RT	0.00  HOUR  Lanes 0.04 0.00 1.96 0.00	Volume  18 0 911 0	0 Capacity 62 0 2,824	0.000 *  V/C  0.290  0.000  0.323 *  0.000	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.344 * 0.000 0.275 *
Approach Southbound	PM PEAK F Movement RT TH LT RT TH	0.00  HOUR  Lanes 0.04 0.00 1.96 0.00 3.00	Volume  18 0 911 0 1,305	0 Capacity 62 0 2,824 0 4,800	0.000 *  V/C  0.290 0.000 0.323 * 0.000 0.272	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):	LYSIS 0.344 * 0.000 0.275 * 0.272
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT	0.00  HOUR  Lanes 0.04 0.00 1.96 0.00 3.00 1.00	Volume  18 0 911 0 1,305 33	Capacity 62 0 2,824 0 4,800 1,600	0.000 *  V/C  0.290 0.000 0.323 *  0.000 0.272 0.021 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):	LYSIS 0.344 * 0.000 0.275 * 0.272
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT	0.00  HOUR  Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00	Volume  18 0 911 0 1,305 33 61	Capacity 62 0 2,824 0 4,800 1,600 1,600	0.000 *  V/C  0.290 0.000 0.323 *  0.000 0.272 0.021 * 0.018	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time:	LYSIS 0.344 * 0.000 0.275 * 0.272 0.619 0.100
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT	0.00  HOUR  Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00	0 Volume 18 0 911 0 1,305 33 61 0	0 Capacity 62 0 2,824 0 4,800 1,600 1,600 0	0.000 *  V/C  0.290 0.000 0.323 *  0.000 0.272 0.021 *  0.018 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time:	LYSIS 0.344 * 0.000 0.275 * 0.272 0.619 0.100
Approach Southbound Westbound Northbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT	0.00  HOUR  Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00	Volume  18 0 911 0 1,305 33 61 0 34	Capacity 62 0 2,824 0 4,800 1,600 0 1,600	0.000 *  V/C  0.290 0.000 0.323 *  0.000 0.272 0.021 *  0.018 0.000 0.021 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.344 * 0.000 0.275 * 0.272  0.619 0.100 -0.070

Traffic signals in Culver City have advanced traffic signal synchronization equivalent to ATSAC.

Peak Period:

^{* =} Critical Movement

**INT#9** 

North/South Street: WASHINGTON BOULEVARD-IRVING PLACE

East/West Street: CULVER BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

AM PEAK HOUR

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AW PEAK F	IUUK					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.09	28	138	0.203	N-S(1):	0.296 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.91	623	2,756	0.226 *	E-W(1):	0.323
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.390 *
	TH	3.00	1,870	4,800	0.390 *		
	LT	1.00	44	1,600	0.028	V/C:	0.686
Northbound	RT	1.00	91	1,600	0.029	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.00	112	1,600	0.070 *		
Eastbound	RT	0.00	0	0	0.000	ICU:	0.716
	TH	3.00	1,416	4,800	0.295		
	LT	0.00	0	0	0.000 *	LOS:	С
Peak Period:	PM PEAK H	IOUR					
Peak Period: Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT		Volume 18	Capacity 60	0.300	ICU ANA N-S(1):	LYSIS 0.356 *
Approach	Movement	Lanes					
Approach	Movement RT	Lanes 0.04	18	60	0.300	N-S(1):	0.356 *
Approach	Movement RT TH	Lanes 0.04 0.00	18 0	60 0	0.300 0.000	N-S(1): N-S(2):	0.356 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 0.04 0.00 1.96	18 0 943	60 0 2,826	0.300 0.000 0.334 *	N-S(1): N-S(2): E-W(1):	0.356 * 0.000 0.327
Approach Southbound	Movement RT TH LT RT	0.04 0.00 1.96 0.00	18 0 943 0	60 0 2,826 0	0.300 0.000 0.334 * 0.000	N-S(1): N-S(2): E-W(1):	0.356 * 0.000 0.327 0.328 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.04 0.00 1.96 0.00 3.00	18 0 943 0 1,574	60 0 2,826 0 4,800	0.300 0.000 0.334 * 0.000 0.328 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.356 * 0.000 0.327 0.328 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00	18 0 943 0 1,574 34	60 0 2,826 0 4,800 1,600	0.300 0.000 0.334 * 0.000 0.328 * 0.021	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.356 * 0.000 0.327 0.328 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00	18 0 943 0 1,574 34 65 0 35	60 0 2,826 0 4,800 1,600	0.300 0.000 0.334 * 0.000 0.328 * 0.021 0.019	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.356 * 0.000 0.327 0.328 * 0.684 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00	18 0 943 0 1,574 34 65 0	60 0 2,826 0 4,800 1,600 1,600 0	0.300 0.000 0.334 * 0.000 0.328 * 0.021 0.019 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.356 * 0.000 0.327 0.328 * 0.684 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT TH LT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00	18 0 943 0 1,574 34 65 0 35	60 0 2,826 0 4,800 1,600 1,600 0 1,600	0.300 0.000 0.334 * 0.000 0.328 * 0.021 0.019 0.000 0.022 * 0.000 0.306	N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.356 * 0.000 0.327 0.328 * 0.684 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00 0.00	18 0 943 0 1,574 34 65 0 35	60 0 2,826 0 4,800 1,600 0 1,600 0	0.300 0.000 0.334 * 0.000 0.328 * 0.021 0.019 0.000 0.022 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.356 * 0.000 0.327 0.328 * 0.684 0.100 -0.070

Traffic signals in Culver City have advanced traffic signal synchronization equivalent to ATSAC.

Peak Period:

^{* =} Critical Movement

INT # 9

North/South Street: WASHINGTON BOULEVARD-IRVING PLACE

East/West Street: CULVER BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR				
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS
Southbound	RT	0.09	28	138	0.203	N-S(1): 0.296 *
	TH	0.00	0	0	0.000	N-S(2): 0.000
	LT	1.91	623	2,756	0.226 *	E-W(1): 0.325
Westbound	RT	0.00	0	0	0.000	E-W(2): 0.390 *
	TH	3.00	1,872	4,800	0.390 *	
	LT	1.00	44	1,600	0.028	V/C: 0.686
Northbound	RT	1.00	91	1,600	0.029	Lost Time: 0.100
	TH	0.00	0	0	0.000	ATSAC: -0.070
	LT	1.00	112	1,600	0.070 *	
Eastbound	RT	0.00	0	0	0.000	ICU: 0.716
	TH	3.00	1,427	4,800	0.297	
	LT	0.00	0	0	0.000 *	LOS: C
Peak Period:	PM PEAK H	IOUR				
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS
	Movement RT	Lanes 0.04	18	60	0.300	N-S(1): 0.356 *
Approach	Movement RT TH	0.04 0.00	18 0	60 0	0.300 0.000	N-S(1): 0.356 * N-S(2): 0.000
Approach Southbound	Movement RT TH LT	0.04 0.00 1.96	18 0 943	60 0 2,826	0.300 0.000 0.334 *	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328
Approach	Movement RT TH LT RT	0.04 0.00 1.96 0.00	18 0 943 0	60 0 2,826	0.300 0.000 0.334 * 0.000	N-S(1): 0.356 * N-S(2): 0.000
Approach Southbound	Movement RT TH LT RT TH	0.04 0.00 1.96 0.00 3.00	18 0 943	60 0 2,826 0 4,800	0.300 0.000 0.334 * 0.000 0.330 *	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *
Approach Southbound	Movement RT TH LT RT	0.04 0.00 1.96 0.00	18 0 943 0	60 0 2,826	0.300 0.000 0.334 * 0.000	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328
Approach Southbound	Movement RT TH LT RT RT TH	0.04 0.00 1.96 0.00 3.00	18 0 943 0 1,586	60 0 2,826 0 4,800	0.300 0.000 0.334 * 0.000 0.330 *	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00	18 0 943 0 1,586 34	60 0 2,826 0 4,800 1,600	0.300 0.000 0.334 * 0.000 0.330 * 0.021	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *  V/C: 0.686
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	0.04 0.00 1.96 0.00 3.00 1.00	18 0 943 0 1,586 34 65	60 0 2,826 0 4,800 1,600	0.300 0.000 0.334 * 0.000 0.330 * 0.021 0.019	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *  V/C: 0.686 Lost Time: 0.100 ATSAC: -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00	18 0 943 0 1,586 34 65 0	60 0 2,826 0 4,800 1,600 1,600	0.300 0.000 0.334 * 0.000 0.330 * 0.021 0.019 0.000	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *  V/C: 0.686 Lost Time: 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00	18 0 943 0 1,586 34 65 0	60 0 2,826 0 4,800 1,600 1,600 0 1,600	0.300 0.000 0.334 * 0.000 0.330 * 0.021 0.019 0.000 0.022 *	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *  V/C: 0.686 Lost Time: 0.100 ATSAC: -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT RT TH LT RT TH LT RT	Lanes 0.04 0.00 1.96 0.00 3.00 1.00 1.00 0.00 1.00 0.00	18 0 943 0 1,586 34 65 0 35	60 0 2,826 0 4,800 1,600 0 1,600 0	0.300 0.000 0.334 * 0.000 0.330 * 0.021 0.019 0.000 0.022 *	N-S(1): 0.356 * N-S(2): 0.000 E-W(1): 0.328 E-W(2): 0.330 *  V/C: 0.686 Lost Time: 0.100 ATSAC: -0.070

^{* =} Critical Movement

INT # 10

North/South Street: MAIN STREET

East/West Street: CULVER BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSI	S
Southbound	RT	1.00	212	1,600	0.000	N-S(1): 0.0	56 *
	TH	0.00	0	0	0.000	N-S(2): 0.0	00
	LT	1.00	89	1,600	0.056 *	E-W(1): 0.3	37
Westbound	RT	1.00	126	1,600	0.023	E-W(2): 0.5	98 *
	TH	2.00	1,394	3,200	0.436 *		
	LT	0.00	0	0	0.000	V/C: 0.6	54
Northbound	RT	0.00	0	0	0.000	Lost Time: 0.1	00
	TH	0.00	0	0	0.000 *	ATSAC: -0.0	70
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	0	0	0.000	ICU: 0.6	84
	TH	3.00	1,619	4,800	0.337		
	LT	1.00	259	1,600	0.162 *	LOS: B	}
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSI	
	Movement RT	Lanes 1.00	209	1,600	0.043	N-S(1): 0.1	43 *
Approach	Movement RT TH	1.00 0.00	209 0	1,600 0	0.043 0.000	N-S(1): 0.1- N-S(2): 0.0-	43 * 43
Approach Southbound	Movement RT TH LT	1.00 0.00 1.00	209 0 229	1,600 0 1,600	0.043 0.000 0.143 *	N-S(1): 0.1 N-S(2): 0.0 E-W(1): 0.3	43 * 43 75
Approach	Movement RT TH LT RT	1.00 0.00 1.00 1.00	209 0	1,600 0 1,600 1,600	0.043 0.000 0.143 * 0.000	N-S(1): 0.14 N-S(2): 0.04 E-W(1): 0.3	43 * 43
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 0.00 1.00 1.00 2.00	209 0 229	1,600 0 1,600 1,600 3,200	0.043 0.000 0.143 * 0.000 0.341 *	N-S(1): 0.1 N-S(2): 0.0 E-W(1): 0.3 E-W(2): 0.4	43 * 43 75 29 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	1.00 0.00 1.00 1.00	209 0 229 92 1,091 1	1,600 0 1,600 1,600	0.043 0.000 0.143 * 0.000 0.341 * 0.001	N-S(1): 0.1- N-S(2): 0.0- E-W(1): 0.3 E-W(2): 0.4- V/C: 0.5	43 * 43 75 29 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 0.00 1.00 1.00 2.00	209 0 229 92	1,600 0 1,600 1,600 3,200	0.043 0.000 0.143 * 0.000 0.341 *	N-S(1): 0.1 N-S(2): 0.0 E-W(1): 0.3 E-W(2): 0.4	43 * 43 75 29 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	1.00 0.00 1.00 1.00 2.00 0.00	209 0 229 92 1,091 1	1,600 0 1,600 1,600 3,200 1,600 0	0.043 0.000 0.143 * 0.000 0.341 * 0.001	N-S(1): 0.1- N-S(2): 0.0- E-W(1): 0.3 E-W(2): 0.4- V/C: 0.5	43 * 43 75 29 * 72 00
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00	209 0 229 92 1,091 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.143 * 0.000 0.341 * 0.001 0.000	N-S(1): 0.1 N-S(2): 0.0 E-W(1): 0.3 E-W(2): 0.4 V/C: 0.5 Lost Time: 0.1 ATSAC: -0.0	43 * 43 75 29 * 72 00 70
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	209 0 229 92 1,091 1 0	1,600 0 1,600 1,600 3,200 1,600 0	0.043 0.000 0.143 * 0.000 0.341 * 0.001 0.000 0.000 *	N-S(1): 0.1- N-S(2): 0.0- E-W(1): 0.3 E-W(2): 0.4- V/C: 0.5 Lost Time: 0.1	43 * 43 75 29 * 72 00 70
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	209 0 229 92 1,091 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.143 * 0.000 0.341 * 0.001 0.000 0.000 * 0.000	N-S(1): 0.1 N-S(2): 0.0 E-W(1): 0.3 E-W(2): 0.4 V/C: 0.5 Lost Time: 0.1 ATSAC: -0.0	43 * 43 75 29 * 72 00 70
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	209 0 229 92 1,091 1 0 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.143 * 0.000 0.341 * 0.001 0.000 0.000 * 0.000	N-S(1): 0.1 N-S(2): 0.0 E-W(1): 0.3 E-W(2): 0.4 V/C: 0.5 Lost Time: 0.1 ATSAC: -0.0	43 * 43 75 29 * 72 00 70 02

^{* =} Critical Movement

**INT # 10** 

North/South Street: MAIN STREET

East/West Street: CULVER BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
Southbound	RT	1.00	212	1,600	0.000	N-S(1):	0.056 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.00	89	1,600	0.056 *	E-W(1):	0.340
Westbound	RT	1.00	126	1,600	0.023	E-W(2):	0.598 *
	TH	2.00	1,396	3,200	0.436 *		
	LT	0.00	0	0	0.000	V/C:	0.654
Northbound	RT	0.00	0	0	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000 *	ATSAC:	-0.070
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	0	0	0.000	ICU:	0.684
	TH	3.00	1,630	4,800	0.340		
		4.00	250	1,600	0.162 *	LOS:	В
	LT	1.00	259	1,600	0.102	LO3.	ט
			259	1,000	0.102		В
Peak Period:	PM PEAK H			,			
Approach	PM PEAK H	IOUR Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
	PM PEAK F Movement RT	IOUR Lanes 1.00		,	V/C 0.043	ICU ANAI N-S(1):	LYSIS 0.143 *
Approach	PM PEAK H Movement RT TH	Lanes 1.00 0.00	Volume 209 0	Capacity 1,600 0	V/C 0.043 0.000	ICU ANAI N-S(1): N-S(2):	LYSIS 0.143 * 0.043
Approach Southbound	PM PEAK H Movement RT TH LT	Lanes 1.00 0.00 1.00	Volume 209 0 229	Capacity 1,600 0 1,600	V/C 0.043 0.000 0.143 *	ICU ANAI N-S(1): N-S(2): E-W(1):	UYSIS 0.143 * 0.043 0.376
Approach	PM PEAK H Movement RT TH	Lanes 1.00 0.00	Volume 209 0	Capacity 1,600 0	V/C 0.043 0.000	ICU ANAI N-S(1): N-S(2):	LYSIS 0.143 * 0.043
Approach Southbound	PM PEAK H Movement RT TH LT	Lanes 1.00 0.00 1.00	Volume 209 0 229	Capacity 1,600 0 1,600	V/C 0.043 0.000 0.143 *	ICU ANAI N-S(1): N-S(2): E-W(1):	UYSIS 0.143 * 0.043 0.376
Approach Southbound	PM PEAK F  Movement  RT  TH  LT  RT	Lanes 1.00 0.00 1.00 1.00	Volume 209 0 229 92	Capacity 1,600 0 1,600 1,600	V/C 0.043 0.000 0.143 * 0.000	ICU ANAI N-S(1): N-S(2): E-W(1):	UYSIS 0.143 * 0.043 0.376
Approach Southbound	PM PEAK F  Movement  RT  TH  LT  RT  TH	Lanes 1.00 0.00 1.00 1.00 2.00	Volume 209 0 229 92	Capacity 1,600 0 1,600 1,600 3,200	V/C 0.043 0.000 0.143 * 0.000 0.345 *	ICU ANAI N-S(1): N-S(2): E-W(1): E-W(2):	UYSIS 0.143 * 0.043 0.376 0.433 *
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00	Volume 209 0 229 92 1,103 1	Capacity 1,600 0 1,600 1,600 3,200 1,600	V/C 0.043 0.000 0.143 * 0.000 0.345 * 0.001	ICU ANAI N-S(1): N-S(2): E-W(1): E-W(2): V/C:	UYSIS 0.143 * 0.043 0.376 0.433 * 0.576
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  TH  LT  RT  TH  LT  RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00	Volume 209 0 229 92 1,103 1 0	Capacity 1,600 0 1,600 1,600 3,200 1,600 0	V/C 0.043 0.000 0.143 * 0.000 0.345 * 0.001 0.000	ICU ANAI N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.143 * 0.043 0.376 0.433 * 0.576 0.100
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  TH  LT  TH  LT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	Volume 209 0 229 92 1,103 1 0 0	Capacity 1,600 0 1,600 1,600 3,200 1,600 0	V/C 0.043 0.000 0.143 * 0.000 0.345 * 0.001 0.000 0.000 *	ICU ANAI N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.143 * 0.043 0.376 0.433 * 0.576 0.100
Approach Southbound Westbound Northbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	Volume 209 0 229 92 1,103 1 0 0	Capacity 1,600 0 1,600 1,600 3,200 1,600 0 0	V/C 0.043 0.000 0.143 * 0.000 0.345 * 0.001 0.000 0.000 * 0.000	ICU ANAI N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.143 * 0.043 0.376 0.433 * 0.576 0.100 -0.070

^{* =} Critical Movement

INT # 10

North/South Street: MAIN STREET

East/West Street: CULVER BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	216	1,600	0.000	N-S(1):	0.080 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.00	128	1,600	0.080 *	E-W(1):	0.395
Westbound	RT	1.00	132	1,600	0.003	E-W(2):	0.676 *
	TH	2.00	1,636	3,200	0.511 *		
	LT	0.00	0	0	0.000	V/C:	0.756
Northbound	RT	0.00	0	0	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000 *	ATSAC:	-0.070
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	0	0	0.000	ICU:	0.786
	TH	3.00	1,895	4,800	0.395		
	LT	1.00	264	1,600	0.165 *	LOS:	С
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.00	213	1,600	0.043	N-S(1):	0.168 *
Approach	Movement RT TH	Lanes 1.00 0.00	213 0	1,600 0	0.043 0.000	N-S(1): N-S(2):	0.168 * 0.043
Approach Southbound	Movement RT TH LT	Lanes 1.00 0.00 1.00	213 0 269	1,600 0 1,600	0.043 0.000 0.168 *	N-S(1): N-S(2): E-W(1):	0.168 * 0.043 0.435
Approach	Movement RT TH LT RT	Lanes 1.00 0.00 1.00	213 0 269 106	1,600 0 1,600 1,600	0.043 0.000 0.168 * 0.000	N-S(1): N-S(2):	0.168 * 0.043
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 0.00 1.00 1.00 2.00	213 0 269	1,600 0 1,600 1,600 3,200	0.043 0.000 0.168 * 0.000 0.428 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.168 * 0.043 0.435 0.518 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00	213 0 269 106 1,368 1	1,600 0 1,600 1,600	0.043 0.000 0.168 * 0.000 0.428 * 0.001	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.168 * 0.043 0.435 0.518 *
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00	213 0 269 106 1,368 1	1,600 0 1,600 1,600 3,200	0.043 0.000 0.168 * 0.000 0.428 * 0.001 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.168 * 0.043 0.435 0.518 * 0.686 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT RT TH LT TH LT RT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,368 1 0	1,600 0 1,600 1,600 3,200 1,600 0	0.043 0.000 0.168 * 0.000 0.428 * 0.001 0.000 0.000 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.168 * 0.043 0.435 0.518 *
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,368 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.168 * 0.000 0.428 * 0.001 0.000 0.000 * 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.168 * 0.043 0.435 0.518 * 0.686 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,368 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0	0.043 0.000 0.168 * 0.000 0.428 * 0.001 0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.168 * 0.043 0.435 0.518 * 0.686 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,368 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.168 * 0.000 0.428 * 0.001 0.000 0.000 * 0.000 0.000 0.434	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.168 * 0.043 0.435 0.518 * 0.686 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,368 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.168 * 0.000 0.428 * 0.001 0.000 0.000 * 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.168 * 0.043 0.435 0.518 * 0.686 0.100 -0.070

^{* =} Critical Movement

**INT #10** 

North/South Street: MAIN STREET

East/West Street: CULVER BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR				
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS
Southbound	RT	1.00	216	1,600	0.000	N-S(1): 0.080 *
	TH	0.00	0	0	0.000	N-S(2): 0.000
	LT	1.00	128	1,600	0.080 *	E-W(1): 0.397
Westbound	RT	1.00	132	1,600	0.003	E-W(2): 0.677 *
	TH	2.00	1,638	3,200	0.512 *	
	LT	0.00	0	0	0.000	V/C: 0.757
Northbound	RT	0.00	0	0	0.000	Lost Time: 0.100
	TH	0.00	0	0	0.000 *	ATSAC: -0.070
	LT	0.00	0	0	0.000	
Eastbound	RT	0.00	0	0	0.000	ICU: 0.787
	TH	3.00	1,906	4,800	0.397	
	LT	1.00	264	1,600	0.165 *	LOS: C
Peak Period:	PM PEAK H	IOUR				
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS
	Movement RT	Lanes 1.00	213	1,600	0.043	N-S(1): 0.168 *
Approach	Movement RT TH	1.00 0.00	213 0	1,600 0	0.043 0.000	N-S(1): 0.168 * N-S(2): 0.043
Approach Southbound	Movement RT TH LT	1.00 0.00 1.00	213 0 269	1,600 0 1,600	0.043 0.000 0.168 *	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435
Approach	Movement RT TH LT RT	1.00 0.00 1.00 1.00	213 0 269 106	1,600 0 1,600 1,600	0.043 0.000 0.168 * 0.000	N-S(1): 0.168 * N-S(2): 0.043
Approach Southbound	Movement RT TH LT RT TH	1.00 0.00 1.00 1.00 2.00	213 0 269	1,600 0 1,600 1,600 3,200	0.043 0.000 0.168 * 0.000 0.432 *	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00	213 0 269 106 1,380 1	1,600 0 1,600 1,600	0.043 0.000 0.168 * 0.000 0.432 * 0.001	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	1.00 0.00 1.00 1.00 2.00	213 0 269 106 1,380 1	1,600 0 1,600 1,600 3,200 1,600	0.043 0.000 0.168 * 0.000 0.432 * 0.001 0.000	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690 Lost Time: 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00	213 0 269 106 1,380 1	1,600 0 1,600 1,600 3,200 1,600 0	0.043 0.000 0.168 * 0.000 0.432 * 0.001	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,380 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.168 * 0.000 0.432 * 0.001 0.000 0.000 * 0.000	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690 Lost Time: 0.100 ATSAC: -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,380 1 0	1,600 0 1,600 1,600 3,200 1,600 0	0.043 0.000 0.168 * 0.000 0.432 * 0.001 0.000 0.000 * 0.000	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690 Lost Time: 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,380 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.168 * 0.000 0.432 * 0.001 0.000 0.000 * 0.000 0.000 0.434	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690 Lost Time: 0.100 ATSAC: -0.070  ICU: 0.720
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.00 1.00 1.00 2.00 0.00 0.00 0.00	213 0 269 106 1,380 1 0 0	1,600 0 1,600 1,600 3,200 1,600 0 0	0.043 0.000 0.168 * 0.000 0.432 * 0.001 0.000 0.000 * 0.000	N-S(1): 0.168 * N-S(2): 0.043 E-W(1): 0.435 E-W(2): 0.522 *  V/C: 0.690 Lost Time: 0.100 ATSAC: -0.070

^{* =} Critical Movement

**INT #11** 

North/South Street: WASHINGTON BOULEVARD-CANFIELD AVENUE

East/West Street: CULVER BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	8	1,600	0.001 *	N-S(1):	0.385
	TH	0.00	0	0	0.000	N-S(2):	0.428 *
	LT	0.00	0	0	0.000	E-W(1):	0.239 *
Westbound	RT	0.00	1	0	0.000	E-W(2):	0.090
	TH	2.00	273	3,200	0.086		
	LT	1.00	30	1,600	0.019 *	V/C:	0.667
Northbound	RT	1.00	53	1,600	0.014	Lost Time:	0.100
	TH	0.03	17	44	0.385	ATSAC:	-0.070
	LT	1.97	1,214	2,840	0.427 *		
Eastbound	RT	2.00	1,046	3,200	0.135	ICU:	0.697
	TH	2.00	705	3,200	0.220 *		
	LT	1.00	7	1,600	0.004	LOS:	В
Deal Deals	DM DE ALC I	IOUD					
Peak Period:	PM PEAK F		\/ali maa	Consoit	V/C	ICILANIA	LVCIC
Approach	Movement	Lanes	Volume	Capacity		ICU ANA	
Southbound	RT Tu	1.00	25	1,600	0.001 *	N-S(1):	0.286
	TH	0.00	0	0	0.000	N-S(2):	0.319 *
M/s alle accessed	LT	0.00	0	0	0.000	E-W(1):	0.273 *
Westbound	RT	0.00	19	0	0.000	E-W(2):	0.127
	TH	2.00	344	3,200	0.113		. =
	LT	1.00	35	1,600	0.022 *	V/C:	0.592
Northbound	RT	1.00	99	1,600	0.040	Lost Time:	0.100
	TH	0.03	14	49	0.286	ATSAC:	-0.070
	LT	1.97	901	2,836	0.318 *		
Eastbound	RT	2.00	1,219	3,200	0.238	ICU:	0.622
	TH	2.00	804	3,200	0.251 *		
	LT	1.00	23	1,600	0.014	LOS:	В

^{* =} Critical Movement

**INT # 11** 

North/South Street: WASHINGTON BOULEVARD-CANFIELD AVENUE

East/West Street: CULVER BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR				
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS
Southbound	RT	1.00	8	1,600	0.001 *	N-S(1): 0.385
	TH	0.00	0	0	0.000	N-S(2): 0.429 *
	LT	0.00	0	0	0.000	E-W(1): 0.239 *
Westbound	RT	0.00	1	0	0.000	E-W(2): 0.090
	TH	2.00	273	3,200	0.086	
	LT	1.00	30	1,600	0.019 *	V/C: 0.668
Northbound	RT	1.00	53	1,600	0.014	Lost Time: 0.100
	TH	0.03	17	44	0.385	ATSAC: -0.070
	LT	1.97	1,216	2,840	0.428 *	
Eastbound	RT	2.00	1,057	3,200	0.138	ICU: 0.698
	TH	2.00	705	3,200	0.220 *	
	LT	1.00	7	1,600	0.004	LOS: B
Peak Period:	PM PEAK H	IOUR				
Peak Period: Approach	PM PEAK H	IOUR Lanes	Volume	Capacity	V/C	ICU ANALYSIS
			Volume 25	Capacity 1,600	V/C 0.001 *	ICU ANALYSIS N-S(1): 0.290
Approach	Movement	Lanes				
Approach	Movement RT	Lanes 1.00	25	1,600	0.001 *	N-S(1): 0.290
Approach	Movement RT TH	Lanes 1.00 0.00	25 0	1,600 0	0.001 * 0.000	N-S(1): 0.290 N-S(2): 0.323 *
Approach Southbound	Movement RT TH LT	Lanes 1.00 0.00 0.00	25 0 0	1,600 0 0	0.001 * 0.000 0.000	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 *
Approach Southbound	Movement RT TH LT RT	Lanes 1.00 0.00 0.00 0.00	25 0 0 19	1,600 0 0	0.001 * 0.000 0.000 0.000	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 1.00 0.00 0.00 0.00 2.00	25 0 0 19 344	1,600 0 0 0 3,200	0.001 * 0.000 0.000 0.000 0.113	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 * E-W(2): 0.127
Approach Southbound Westbound	Movement RT TH LT RT TH LT LT TH LT	Lanes 1.00 0.00 0.00 0.00 2.00 1.00	25 0 0 19 344 35	1,600 0 0 0 3,200 1,600	0.001 * 0.000 0.000 0.000 0.113 0.022 *	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 * E-W(2): 0.127
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.00 0.00 0.00 0.00 2.00 1.00	25 0 0 19 344 35 99	1,600 0 0 0 3,200 1,600 1,600	0.001 * 0.000 0.000 0.000 0.113 0.022 * 0.040	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 * E-W(2): 0.127 V/C: 0.596 Lost Time: 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT RT TH LT TH LT	Lanes 1.00 0.00 0.00 0.00 2.00 1.00 1.00 0.03	25 0 0 19 344 35 99	1,600 0 0 0 3,200 1,600 48	0.001 * 0.000 0.000 0.000 0.113 0.022 * 0.040 0.290	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 * E-W(2): 0.127 V/C: 0.596 Lost Time: 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT LT	Lanes 1.00 0.00 0.00 0.00 2.00 1.00 1.00 0.03 1.97	25 0 0 19 344 35 99 14	1,600 0 0 0 3,200 1,600 1,600 48 2,837	0.001 * 0.000 0.000 0.000 0.113 0.022 * 0.040 0.290 0.322 *	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 * E-W(2): 0.127  V/C: 0.596 Lost Time: 0.100 ATSAC: -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT LT RT TH LT RT TH LT RT	Lanes 1.00 0.00 0.00 0.00 2.00 1.00 1.00 0.03 1.97 2.00	25 0 0 19 344 35 99 14 913	1,600 0 0 0 3,200 1,600 1,600 48 2,837 3,200	0.001 * 0.000 0.000 0.000 0.113 0.022 * 0.040 0.290 0.322 * 0.237	N-S(1): 0.290 N-S(2): 0.323 * E-W(1): 0.273 * E-W(2): 0.127  V/C: 0.596 Lost Time: 0.100 ATSAC: -0.070

^{* =} Critical Movement

**INT # 11** 

North/South Street: WASHINGTON BOULEVARD-CANFIELD AVENUE

East/West Street: CULVER BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Ν
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	8	1,600	0.001 *	N-S(1):	0.429
	TH	0.00	0	0	0.000	N-S(2):	0.478 *
	LT	0.00	0	0	0.000	E-W(1):	0.293 *
Westbound	RT	0.00	1	0	0.000	E-W(2):	0.123
	TH	2.00	379	3,200	0.119		
	LT	1.00	68	1,600	0.043 *	V/C:	0.771
Northbound	RT	1.00	57	1,600	0.000	Lost Time:	0.100
	TH	0.02	17	40	0.429	ATSAC:	-0.070
	LT	1.98	1,357	2,844	0.477 *		
Eastbound	RT	2.00	1,264	3,200	0.180	ICU:	0.801
	TH	2.00	801	3,200	0.250 *		
	LT	1.00	7	1,600	0.004	LOS:	D
Peak Period:	PM PEAK F						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
Southbound	RT	1.00	26	1,600	0.002 *	N-S(1):	0.352
	TH	0.00	0	0	0.000	N-S(2):	0.393 *
	I I T I					, ,	
	LT	0.00	0	0	0.000	E-W(1):	0.332 *
Westbound	RT	0.00	19	0	0.000	, ,	
Westbound	RT TH	0.00 2.00	19 424	0 3,200	0.000 0.138	E-W(1): E-W(2):	0.332 * 0.152
	RT TH LT	0.00	19 424 61	0 3,200 1,600	0.000 0.138 0.038 *	E-W(1): E-W(2): V/C:	0.332 * 0.152 0.725
Westbound  Northbound	RT TH LT RT	0.00 2.00 1.00 1.00	19 424 61 120	0 3,200 1,600 1,600	0.000 0.138 0.038 * 0.037	E-W(1): E-W(2): V/C: Lost Time:	0.332 * 0.152 0.725 0.100
	RT TH LT RT TH	0.00 2.00 1.00 1.00 0.02	19 424 61 120 14	0 3,200 1,600 1,600 40	0.000 0.138 0.038 * 0.037 0.352	E-W(1): E-W(2): V/C:	0.332 * 0.152 0.725
Northbound	RT TH LT RT TH LT	0.00 2.00 1.00 1.00	19 424 61 120	0 3,200 1,600 1,600 40 2,844	0.000 0.138 0.038 * 0.037 0.352 0.391 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.332 * 0.152
	RT TH LT RT TH	0.00 2.00 1.00 1.00 0.02	19 424 61 120 14	0 3,200 1,600 1,600 40	0.000 0.138 0.038 * 0.037 0.352 0.391 * 0.264	E-W(1): E-W(2): V/C: Lost Time:	0.332 * 0.152 0.725 0.100
Northbound	RT TH LT RT TH LT	0.00 2.00 1.00 1.00 0.02 1.98	19 424 61 120 14 1,113	0 3,200 1,600 1,600 40 2,844	0.000 0.138 0.038 * 0.037 0.352 0.391 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.332 * 0.152

^{* =} Critical Movement

**INT #11** 

North/South Street: WASHINGTON BOULEVARD-CANFIELD AVENUE

East/West Street: CULVER BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

AM PEAK F	IOUR					
Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
RT	1.00	8	1,600	0.001 *	N-S(1):	0.430
TH	0.00	0	0	0.000	N-S(2):	0.479 *
LT	0.00	0	0	0.000	E-W(1):	0.293 *
RT	0.00	1	0	0.000	E-W(2):	0.123
TH	2.00	379	3,200	0.119		
LT	1.00	68	1,600	0.043 *	V/C:	0.772
RT	1.00	57	1,600	0.000	Lost Time:	0.100
TH	0.02	17	40	0.430	ATSAC:	-0.070
LT	1.98	1,359	2,844	0.478 *		
RT	2.00	1,275	3,200	0.183	ICU:	0.802
TH	2.00	801	3,200	0.250 *		
LT	1.00	7	1,600	0.004	LOS:	D
<b>PM PEAK H</b>	IOUR					
Movement	Lanes	Volume	Capacity	V/C		
RT	1.00	26	1,600	0.002 *	N-S(1):	0.356
TH	0.00	0	0	0.000	N-S(2):	0.397 *
LT	0.00	0	0	0.000	E-W(1):	0.332 *
RT	0.00	19	0	0.000	E \///2\.	0.152
	0.00	10	U	0.000	<b>⊏-</b> VV(∠).	0.132
TH	2.00	424	3,200	0.000 0.138	E-VV(2).	0.132
			-		E-vv(2): V/C:	0.729
TH	2.00	424	3,200	0.138	,	
TH LT	2.00 1.00	424 61	3,200 1,600	0.138 0.038 *	V/C:	0.729
TH LT RT	2.00 1.00 1.00	424 61 120	3,200 1,600 1,600	0.138 0.038 * 0.037	V/C: Lost Time:	0.729 0.100
TH LT RT TH	2.00 1.00 1.00 0.02	424 61 120 14	3,200 1,600 1,600 39	0.138 0.038 * 0.037 0.356	V/C: Lost Time:	0.729 0.100
TH LT RT TH LT	2.00 1.00 1.00 0.02 1.98	424 61 120 14 1,125	3,200 1,600 1,600 39 2,845	0.138 0.038 * 0.037 0.356 0.395 *	V/C: Lost Time: ATSAC:	0.729 0.100 -0.070
	RT TH LT	RT 1.00 TH 0.00 LT 0.00 RT 0.00 TH 2.00 LT 1.00 RT 1.00 TH 0.02 LT 1.98 RT 2.00 TH 2.00 LT 1.00  PM PEAK HOUR  Movement Lanes RT 1.00 TH 0.00 LT 0.00	RT       1.00       8         TH       0.00       0         LT       0.00       0         RT       0.00       1         TH       2.00       379         LT       1.00       68         RT       1.00       57         TH       0.02       17         LT       1.98       1,359         RT       2.00       801         LT       1.00       7          PM PEAK HOUR         Movement       Lanes       Volume         RT       1.00       26         TH       0.00       0         LT       0.00       0         LT       0.00       0	RT         1.00         8         1,600           TH         0.00         0         0           LT         0.00         0         0           RT         0.00         1         0           TH         2.00         379         3,200           LT         1.00         68         1,600           RT         1.00         57         1,600           TH         0.02         17         40           LT         1.98         1,359         2,844           RT         2.00         1,275         3,200           TH         2.00         801         3,200           LT         1.00         7         1,600           PM PEAK HOUR           Movement         Lanes         Volume         Capacity           RT         1.00         26         1,600           TH         0.00         0         0           LT         0.00         0         0	RT         1.00         8         1,600         0.001 *           TH         0.00         0         0.000         0.000           LT         0.00         0         0.000         0.000           RT         0.00         1         0         0.000           TH         2.00         379         3,200         0.119           LT         1.00         68         1,600         0.043 *           RT         1.00         57         1,600         0.000           TH         0.02         17         40         0.430           LT         1.98         1,359         2,844         0.478 *           RT         2.00         1,275         3,200         0.183           TH         2.00         801         3,200         0.250 *           LT         1.00         7         1,600         0.004    PM PEAK HOUR  Movement Lanes Volume Capacity V/C  RT  1.00         0         0.002 *           TH         0.00         0         0.000         0.000           LT         0.00         0         0.000	RT         1.00         8         1,600         0.001 *         N-S(1):           TH         0.00         0         0.000         N-S(2):           LT         0.00         0         0.000         E-W(1):           RT         0.00         1         0         0.000         E-W(2):           TH         2.00         379         3,200         0.119         U.         U.         E-W(2):           RT         1.00         68         1,600         0.043 *         V/C:         Lost Time:         TH         0.02         17         40         0.430         ATSAC:         LT         1.98         1,359         2,844         0.478 *         ICU:         TH         2.00         801         3,200         0.183         ICU:         ICU:         TH         2.00         801         3,200         0.250 *         LT         LT         1.00         7         1,600         0.004         LOS:           PM PEAK HOUR           Movement         Lanes         Volume         Capacity         V/C         ICU ANA           RT         1.00         26         1,600         0.002 *         N-S(1):           TH         0.00         <

^{* =} Critical Movement

**INT #12** 

North/South Street: INCE BOULEVARD

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Υ
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK I	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	5	1,600	0.003	N-S(1):	0.451 *
	TH	0.17	88	280	0.315	N-S(2):	0.000
	LT	1.83	919	2,628	0.350 *	E-W(1):	0.377 *
Westbound	RT	2.00	1,197	3,200	0.374 *	E-W(2):	0.000
	TH	0.00	0	0	0.000		
	LT	1.00	58	1,600	0.036	V/C:	0.828
Northbound	RT	1.00	111	1,600	0.033	Lost Time:	0.100
	TH	1.00	162	1,600	0.101 *	ATSAC:	-0.070
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	1	0	0.000	ICU:	0.858
	TH	1.00	3	1,600	0.003 *		
	LT	0.00	0	0	0.000	LOS:	D
Peak Period:	PM PEAK H		) / a la coma a	0	\//O	1011 4114	1.1/010
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
Southbound	RT	1.00	5	1,600	0.003	N-S(1):	0.514 *
	TH	0.13	86	208	0.414	N-S(2):	0.000
NA (I	LT	1.87	1,238	2,693	0.460 *	E-W(1):	0.269 *
Westbound	RT	2.00	838	3,200	0.262 *	E-W(2):	0.000
	TH	0.00	0	0	0.000	\ // O	. =
	LT	1.00	94	1,600	0.059	V/C:	0.783
Northbound	RT	1.00	78	1,600	0.000	Lost Time:	0.100
				4 000	0.0=4:	4.7040	
	TH	1.00	87	1,600	0.054 *	ATSAC:	-0.070
	TH LT	1.00 0.00	0	0	0.000		
Eastbound	TH LT RT	1.00 0.00 0.00	0	0	0.000 0.000	ATSAC:	-0.070 0.813
Eastbound	TH LT	1.00 0.00	0	0	0.000		

^{* =} Critical Movement

**INT # 12** 

North/South Street: INCE BOULEVARD

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

**AM PEAK HOUR** 

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Υ
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

r can r crioa.	7 (10) 1 =7 (1 )						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	5	1,600	0.003	N-S(1):	0.454 *
	TH	0.17	88	277	0.318	N-S(2):	0.000
	LT	1.83	930	2,631	0.353 *	E-W(1):	0.378 *
Westbound	RT	2.00	1,199	3,200	0.375 *	E-W(2):	0.000
	TH	0.00	0	0	0.000		
	LT	1.00	58	1,600	0.036	V/C:	0.832
Northbound	RT	1.00	111	1,600	0.033	Lost Time:	0.100
	TH	1.00	162	1,600	0.101 *	ATSAC:	-0.070
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	1	0	0.000	ICU:	0.862
		1.00	3	1,600	0.003 *		
	TH	1.00		.,000			
	LT	0.00	0	0	0.000	LOS:	D
Peak Period:	PM PEAK F	0.00 HOUR	0	0	0.000		
Approach	PM PEAK F Movement	0.00 HOUR Lanes	0 Volume	0 Capacity	0.000 V/C	ICU ANA	LYSIS
Peak Period: Approach Southbound	PM PEAK F Movement RT	0.00 HOUR Lanes 1.00	Volume 5	Capacity 1,600	0.000 V/C 0.003	ICU ANA N-S(1):	LYSIS 0.515 *
Approach	PM PEAK F  Movement  RT  TH	0.00 HOUR Lanes 1.00 0.13	0 Volume 5 86	0 Capacity 1,600 207	0.000 V/C 0.003 0.415	ICU ANA N-S(1): N-S(2):	LYSIS 0.515 * 0.000
Approach Southbound	PM PEAK F  Movement  RT  TH  LT	0.00  HOUR  Lanes 1.00 0.13 1.87	0 Volume 5 86 1,242	0 Capacity 1,600 207 2,693	0.000 V/C 0.003 0.415 0.461 *	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.515 * 0.000 0.273 *
Approach	PM PEAK F  Movement  RT  TH  LT  RT	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00	0 Volume 5 86	0 Capacity 1,600 207	0.000 V/C 0.003 0.415 0.461 * 0.266 *	ICU ANA N-S(1): N-S(2):	LYSIS 0.515 * 0.000
Approach Southbound	PM PEAK F  Movement  RT  TH  LT  RT  RT  TH	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00 0.00	0 Volume 5 86 1,242 850 0	Capacity 1,600 207 2,693 3,200 0	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):	LYSIS 0.515 * 0.000 0.273 * 0.000
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  TH  LT  TH  LT  TH	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00	0 Volume 5 86 1,242 850 0 94	Capacity 1,600 207 2,693 3,200	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000 0.059	ICU ANA N-S(1): N-S(2): E-W(1):	UYSIS 0.515 * 0.000 0.273 * 0.000 0.788
Approach Southbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00 0.00 1.00 1.00	0 Volume 5 86 1,242 850 0 94 78	Capacity 1,600 207 2,693 3,200 0 1,600 1,600	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000 0.059 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):	LYSIS 0.515 * 0.000 0.273 * 0.000
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  TH  LT  TH  LT  TH	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00 0.00 1.00	0 Volume 5 86 1,242 850 0 94	Capacity 1,600 207 2,693 3,200 0 1,600	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000 0.059	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2): V/C:	UYSIS 0.515 * 0.000 0.273 * 0.000 0.788
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00 0.00 1.00 1.00	0 Volume 5 86 1,242 850 0 94 78	Capacity 1,600 207 2,693 3,200 0 1,600 1,600	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000 0.059 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	UYSIS 0.515 * 0.000 0.273 * 0.000 0.788 0.100 -0.070
Approach Southbound Westbound	PM PEAK F  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  RT  TH  LT  RT  RT  RT  TH  RT  RT  RT  RT  RT  R	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00 0.00 1.00 1.00 1.00	0 Volume 5 86 1,242 850 0 94 78 87	Capacity 1,600 207 2,693 3,200 0 1,600 1,600 1,600	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000 0.059 0.000 0.054 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	UYSIS 0.515 * 0.000 0.273 * 0.000 0.788 0.100
Approach Southbound Westbound Northbound	PM PEAK F  Movement  RT  TH  LT	0.00  HOUR  Lanes 1.00 0.13 1.87 2.00 0.00 1.00 1.00 1.00 0.00	0 Volume 5 86 1,242 850 0 94 78 87 0	Capacity 1,600 207 2,693 3,200 0 1,600 1,600 1,600 0	0.000 V/C 0.003 0.415 0.461 * 0.266 * 0.000 0.059 0.000 0.054 * 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.515 * 0.000 0.273 * 0.000 0.788 0.100 -0.070

Traffic signals in Culver City have advanced traffic signal synchronization equivalent to ATSAC.

Peak Period:

^{* =} Critical Movement

**INT # 12** 

North/South Street: INCE BOULEVARD

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Υ
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	60	1,600	0.038	N-S(1):	0.542 *
	TH	0.29	179	463	0.387	N-S(2):	0.000
	LT	1.71	1,058	2,463	0.430 *	E-W(1):	0.442 *
Westbound	RT	2.00	1,327	3,200	0.415 *	E-W(2):	0.000
	TH	0.00	0	0	0.000		
	LT	1.00	119	1,600	0.074	V/C:	0.984
Northbound	RT	1.00	117	1,600	0.000	Lost Time:	0.100
	TH	1.00	179	1,600	0.112 *	ATSAC:	-0.070
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	1	0	0.000	ICU:	1.014
	TH	1.00	42	1,600	0.027 *		
	LT	0.00	0	0	0.000	LOS:	F
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.00	69	1,600	0.043	N-S(1):	0.627 *
Approach	Movement RT TH	1.00 0.15	69 115	1,600 244	0.043 0.471	N-S(1): N-S(2):	0.627 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 1.00 0.15 1.85	69 115 1,391	1,600 244 2,660	0.043 0.471 0.523 *	N-S(1): N-S(2): E-W(1):	0.627 * 0.000 0.371 *
Approach	Movement RT TH LT RT	1.00 0.15 1.85 2.00	69 115 1,391 991	1,600 244 2,660 3,200	0.043 0.471 0.523 * 0.310 *	N-S(1): N-S(2):	0.627 * 0.000
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 0.15 1.85 2.00 0.00	69 115 1,391 991 0	1,600 244 2,660 3,200 0	0.043 0.471 0.523 * 0.310 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2):	0.627 * 0.000 0.371 * 0.000
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00	69 115 1,391 991 0 114	1,600 244 2,660 3,200 0 1,600	0.043 0.471 0.523 * 0.310 * 0.000 0.071	N-S(1): N-S(2): E-W(1):	0.627 * 0.000 0.371 * 0.000
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00	69 115 1,391 991 0 114 103	1,600 244 2,660 3,200 0 1,600	0.043 0.471 0.523 * 0.310 * 0.000 0.071 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.627 * 0.000 0.371 * 0.000 0.998 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00	69 115 1,391 991 0 114 103 166	1,600 244 2,660 3,200 0 1,600 1,600 1,600	0.043 0.471 0.523 * 0.310 * 0.000 0.071 0.000 0.104 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.627 * 0.000 0.371 * 0.000
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00 0.00	69 115 1,391 991 0 114 103	1,600 244 2,660 3,200 0 1,600 1,600 0	0.043 0.471 0.523 * 0.310 * 0.000 0.071 0.000 0.104 * 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.627 * 0.000 0.371 * 0.000 0.998 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00 0.00 0.00	69 115 1,391 991 0 114 103 166 0	1,600 244 2,660 3,200 0 1,600 1,600 0	0.043 0.471 0.523 * 0.310 * 0.000 0.071 0.000 0.104 * 0.000 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.627 * 0.000 0.371 * 0.000 0.998 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00 0.00	69 115 1,391 991 0 114 103 166 0	1,600 244 2,660 3,200 0 1,600 1,600 0	0.043 0.471 0.523 * 0.310 * 0.000 0.071 0.000 0.104 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.627 * 0.000 0.371 * 0.000 0.998 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00 0.00 0.00	69 115 1,391 991 0 114 103 166 0	1,600 244 2,660 3,200 0 1,600 1,600 0	0.043 0.471 0.523 * 0.310 * 0.000 0.071 0.000 0.104 * 0.000 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.627 * 0.000 0.371 * 0.000 0.998 0.100 -0.070

^{* =} Critical Movement

**INT # 12** 

North/South Street: INCE BOULEVARD

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Y
Left-Turn Lane:	1600 vph	E-W Split Phase :	Υ
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS	)
Southbound	RT	1.00	60	1,600	0.038	N-S(1): 0.54	5 *
	TH	0.29	179	459	0.390	N-S(2): 0.00	0
	LT	1.71	1,069	2,467	0.433 *	E-W(1): 0.44	2 *
Westbound	RT	2.00	1,329	3,200	0.415 *	E-W(2): 0.00	0
	TH	0.00	0	0	0.000		
	LT	1.00	119	1,600	0.074	V/C: 0.98	7
Northbound	RT	1.00	117	1,600	0.000	Lost Time: 0.10	0
	TH	1.00	179	1,600	0.112 *	ATSAC: -0.07	0
	LT	0.00	0	0	0.000		
Eastbound	RT	0.00	1	0	0.000	ICU: 1.01	7
	TH	1.00	42	1,600	0.027 *		
	LT	0.00	0	0	0.000	LOS: F	
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANALYSIS	
	Movement RT	Lanes 1.00	69	1,600	0.043	N-S(1): 0.62	8 *
Approach	Movement	Lanes			0.043 0.472	N-S(1): 0.62 N-S(2): 0.00	8 * 0
Approach Southbound	Movement RT TH LT	Lanes 1.00 0.15 1.85	69	1,600 244 2,661	0.043 0.472 0.524 *	N-S(1): 0.62	8 * 0
Approach	Movement RT TH	1.00 0.15	69 115	1,600 244	0.043 0.472	N-S(1): 0.62 N-S(2): 0.00	8 * 0 4 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 0.15 1.85 2.00 0.00	69 115 1,395	1,600 244 2,661 3,200 0	0.043 0.472 0.524 * 0.313 * 0.000	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00	8 * 0 4 * 0
Approach Southbound	Movement RT TH LT RT	1.00 0.15 1.85 2.00	69 115 1,395 1,003	1,600 244 2,661 3,200	0.043 0.472 0.524 * 0.313 *	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37	8 * 0 4 * 0
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 0.15 1.85 2.00 0.00	69 115 1,395 1,003 0	1,600 244 2,661 3,200 0	0.043 0.472 0.524 * 0.313 * 0.000	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00	8 * 0 4 * 0
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00	69 115 1,395 1,003 0 114	1,600 244 2,661 3,200 0 1,600	0.043 0.472 0.524 * 0.313 * 0.000 0.071	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00	8 * 0 4 * 0
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00	69 115 1,395 1,003 0 114 103	1,600 244 2,661 3,200 0 1,600 1,600 1,600 0	0.043 0.472 0.524 * 0.313 * 0.000 0.071 0.000 0.104 * 0.000	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00  V/C: 1.00 Lost Time: 0.10 ATSAC: -0.07	8 * 0 4 * 0 2 0
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00	69 115 1,395 1,003 0 114 103 166	1,600 244 2,661 3,200 0 1,600 1,600 0 0	0.043 0.472 0.524 * 0.313 * 0.000 0.071 0.000 0.104 *	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00 V/C: 1.00 Lost Time: 0.10	8 * 0 4 * 0 2 0
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT TH LT TH	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00 0.00	69 115 1,395 1,003 0 114 103 166 0	1,600 244 2,661 3,200 0 1,600 1,600 1,600 0	0.043 0.472 0.524 * 0.313 * 0.000 0.071 0.000 0.104 * 0.000	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00  V/C: 1.00 Lost Time: 0.10 ATSAC: -0.07	8 * 0 4 * 0 2 0
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 0.15 1.85 2.00 0.00 1.00 1.00 0.00 0.00	69 115 1,395 1,003 0 114 103 166 0	1,600 244 2,661 3,200 0 1,600 1,600 0 0	0.043 0.472 0.524 * 0.313 * 0.000 0.071 0.000 0.104 * 0.000 0.000	N-S(1): 0.62 N-S(2): 0.00 E-W(1): 0.37 E-W(2): 0.00  V/C: 1.00 Lost Time: 0.10 ATSAC: -0.07	8 * 0 4 * 0 2 0

^{* =} Critical Movement

**INT #13** 

North/South Street: ROBERTSON BOULEVARD-HIGUERA STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	86	1,600	0.054	N-S(1):	0.284 *
	TH	1.00	238	1,600	0.149	N-S(2):	0.203
	LT	1.00	101	1,600	0.063 *	E-W(1):	0.270
Westbound	RT	0.00	142	0	0.000	E-W(2):	0.396 *
	TH	2.00	1,041	3,200	0.370 *		
	LT	1.00	78	1,600	0.049	V/C:	0.680
Northbound	RT	1.00	124	1,600	0.029	Lost Time:	0.100
	TH	1.00	354	1,600	0.221 *	ATSAC:	-0.070
	LT	1.00	86	1,600	0.054		
Eastbound	RT	0.00	65	0	0.000	ICU:	0.710
	TH	2.00	642	3,200	0.221		
	LT	1.00	42	1,600	0.026 *	LOS:	С
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.00	72	1,600	0.045	N-S(1):	0.224 *
Approach	Movement RT TH	Lanes 1.00 1.00	72 235	1,600 1,600	0.045 0.147	N-S(1): N-S(2):	0.224 * 0.170
Approach Southbound	Movement RT TH LT	Lanes 1.00 1.00 1.00	72 235 124	1,600 1,600 1,600	0.045 0.147 0.078 *	N-S(1): N-S(2): E-W(1):	0.224 * 0.170 0.395 *
Approach	Movement RT TH LT RT	Lanes 1.00 1.00 1.00 0.00	72 235 124 202	1,600 1,600 1,600 0	0.045 0.147 0.078 * 0.000	N-S(1): N-S(2):	0.224 * 0.170
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 1.00 1.00 0.00 2.00	72 235 124 202 651	1,600 1,600 1,600 0 3,200	0.045 0.147 0.078 * 0.000 0.267	N-S(1): N-S(2): E-W(1): E-W(2):	0.224 * 0.170 0.395 * 0.388
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00	72 235 124 202 651 82	1,600 1,600 1,600 0 3,200 1,600	0.045 0.147 0.078 * 0.000 0.267 0.051 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.224 * 0.170 0.395 * 0.388
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00	72 235 124 202 651 82 88	1,600 1,600 1,600 0 3,200 1,600	0.045 0.147 0.078 * 0.000 0.267 0.051 * 0.004	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.224 * 0.170 0.395 * 0.388 0.619 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT RT TH LT TH LT RT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 124 202 651 82 88 234	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.045 0.147 0.078 * 0.000 0.267 0.051 * 0.004 0.146 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.224 * 0.170 0.395 * 0.388
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 124 202 651 82 88 234 36	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.045 0.147 0.078 * 0.000 0.267 0.051 * 0.004 0.146 * 0.023	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.224 * 0.170 0.395 * 0.388  0.619 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 124 202 651 82 88 234 36	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.045 0.147 0.078 * 0.000 0.267 0.051 * 0.004 0.146 * 0.023 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.224 * 0.170 0.395 * 0.388 0.619 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 124 202 651 82 88 234 36	1,600 1,600 0 3,200 1,600 1,600 1,600 0 3,200	0.045 0.147 0.078 * 0.000 0.267 0.051 * 0.004 0.146 * 0.023 0.000 0.344 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.224 * 0.170 0.395 * 0.388  0.619 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 124 202 651 82 88 234 36	1,600 1,600 0 3,200 1,600 1,600 1,600 0	0.045 0.147 0.078 * 0.000 0.267 0.051 * 0.004 0.146 * 0.023 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.224 * 0.170 0.395 * 0.388  0.619 0.100 -0.070

^{* =} Critical Movement

**INT #13** 

North/South Street: ROBERTSON BOULEVARD-HIGUERA STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANAL	_YSIS
Southbound	RT	1.00	86	1,600	0.054	N-S(1):	0.297 *
	TH	1.00	238	1,600	0.149	N-S(2):	0.203
	LT	1.00	122	1,600	0.076 *	E-W(1):	0.273
Westbound	RT	0.00	147	0	0.000	E-W(2):	0.398 *
	TH	2.00	1,043	3,200	0.372 *		
	LT	1.00	78	1,600	0.049	V/C:	0.695
Northbound	RT	1.00	126	1,600	0.030	Lost Time:	0.100
	TH	1.00	354	1,600	0.221 *	ATSAC:	-0.070
	LT	1.00	86	1,600	0.054		
Eastbound	RT	0.00	65	0	0.000	ICU:	0.725
	TH	2.00	653	3,200	0.224		
	LT	1.00	42	1,600	0.026 *	LOS:	С
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANAL	
	Movement RT	Lanes 1.00	72	1,600	0.045	N-S(1):	0.229 *
Approach	Movement RT TH	1.00 1.00	72 235	1,600 1,600	0.045 0.147	N-S(1): N-S(2):	0.229 * 0.170
Approach Southbound	Movement RT TH LT	1.00 1.00 1.00	72 235 132	1,600 1,600 1,600	0.045 0.147 0.083 *	N-S(1): N-S(2): E-W(1):	0.229 * 0.170 0.398
Approach	Movement RT TH	1.00 1.00	72 235	1,600 1,600	0.045 0.147 0.083 * 0.000	N-S(1): N-S(2):	0.229 * 0.170
Approach Southbound	Movement RT TH LT	1.00 1.00 1.00	72 235 132	1,600 1,600 1,600	0.045 0.147 0.083 *	N-S(1): N-S(2): E-W(1):	0.229 * 0.170 0.398
Approach Southbound	Movement RT TH LT RT	1.00 1.00 1.00 0.00	72 235 132 225	1,600 1,600 1,600 0	0.045 0.147 0.083 * 0.000	N-S(1): N-S(2): E-W(1):	0.229 * 0.170 0.398
Approach Southbound	Movement RT TH LT RT TH	1.00 1.00 1.00 0.00 2.00	72 235 132 225 663	1,600 1,600 1,600 0 3,200	0.045 0.147 0.083 * 0.000 0.278 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.229 * 0.170 0.398 0.399 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00	72 235 132 225 663 84	1,600 1,600 1,600 0 3,200 1,600	0.045 0.147 0.083 * 0.000 0.278 * 0.053	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.229 * 0.170 0.398 0.399 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00	72 235 132 225 663 84 89 234 36	1,600 1,600 1,600 0 3,200 1,600	0.045 0.147 0.083 * 0.000 0.278 * 0.053 0.003	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.229 * 0.170 0.398 0.399 * 0.628 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 132 225 663 84 89 234	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.045 0.147 0.083 * 0.000 0.278 * 0.053 0.003 0.146 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.229 * 0.170 0.398 0.399 * 0.628 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 132 225 663 84 89 234 36	1,600 1,600 0 3,200 1,600 1,600 1,600 1,600	0.045 0.147 0.083 * 0.000 0.278 * 0.053 0.003 0.146 * 0.023	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.229 * 0.170 0.398 0.399 * 0.628 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	72 235 132 225 663 84 89 234 36	1,600 1,600 0 3,200 1,600 1,600 1,600 0	0.045 0.147 0.083 * 0.000 0.278 * 0.053 0.003 0.146 * 0.023 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.229 * 0.170 0.398 0.399 * 0.628 0.100 -0.070

^{* =} Critical Movement

**INT #13** 

North/South Street: ROBERTSON BOULEVARD-HIGUERA STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	153	1,600	0.096	N-S(1):	0.323 *
	TH	1.00	268	1,600	0.168	N-S(2):	0.226
	LT	1.00	136	1,600	0.085 *	E-W(1):	0.317
Westbound	RT	0.00	154	0	0.000	E-W(2):	0.463 *
	TH	2.00	1,227	3,200	0.432 *		
	LT	1.00	81	1,600	0.051	V/C:	0.786
Northbound	RT	1.00	128	1,600	0.029	Lost Time:	0.100
	TH	1.00	380	1,600	0.238 *	ATSAC:	-0.070
	LT	1.00	92	1,600	0.058		
Eastbound	RT	0.00	73	0	0.000	ICU:	0.816
	TH	2.00	777	3,200	0.266		
	LT	1.00	49	1,600	0.031 *	LOS:	D
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT		Volume 125	1,600	0.078	ICU ANA N-S(1):	0.269 *
Approach	Movement	Lanes					
Approach Southbound	Movement RT	Lanes 1.00	125	1,600	0.078 0.163 0.106 *	N-S(1):	0.269 * 0.189 0.458
Approach	Movement RT TH LT RT	1.00 1.00	125 260	1,600 1,600	0.078 0.163 0.106 * 0.000	N-S(1): N-S(2):	0.269 * 0.189
Approach Southbound	Movement RT TH LT	1.00 1.00 1.00	125 260 170	1,600 1,600 1,600	0.078 0.163 0.106 *	N-S(1): N-S(2): E-W(1):	0.269 * 0.189 0.458
Approach Southbound	Movement RT TH LT RT	1.00 1.00 1.00 0.00	125 260 170 249	1,600 1,600 1,600 0	0.078 0.163 0.106 * 0.000	N-S(1): N-S(2): E-W(1):	0.269 * 0.189 0.458
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 1.00 1.00 0.00 2.00	125 260 170 249 840	1,600 1,600 1,600 0 3,200	0.078 0.163 0.106 * 0.000 0.340 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.269 * 0.189 0.458 0.486 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00	125 260 170 249 840 87	1,600 1,600 1,600 0 3,200 1,600	0.078 0.163 0.106 * 0.000 0.340 * 0.054	N-S(1): N-S(2): E-W(1): E-W(2):	0.269 * 0.189 0.458 0.486 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00	125 260 170 249 840 87 94 260 41	1,600 1,600 1,600 0 3,200 1,600	0.078 0.163 0.106 * 0.000 0.340 * 0.054 0.004	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.269 * 0.189 0.458 0.486 * 0.755 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 170 249 840 87 94 260	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.078 0.163 0.106 * 0.000 0.340 * 0.054 0.004 0.163 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.269 * 0.189 0.458 0.486 * 0.755 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 170 249 840 87 94 260 41	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.078 0.163 0.106 * 0.000 0.340 * 0.054 0.004 0.163 * 0.026	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.269 * 0.189 0.458 0.486 * 0.755 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 170 249 840 87 94 260 41	1,600 1,600 0 3,200 1,600 1,600 1,600 0	0.078 0.163 0.106 * 0.000 0.340 * 0.054 0.004 0.163 * 0.026 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.269 * 0.189 0.458 0.486 * 0.755 0.100 -0.070

^{* =} Critical Movement

**INT #13** 

North/South Street: ROBERTSON BOULEVARD-HIGUERA STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	153	1,600	0.096	N-S(1):	0.336 *
	TH	1.00	268	1,600	0.168	N-S(2):	0.226
	LT	1.00	157	1,600	0.098 *	E-W(1):	0.320
Westbound	RT	0.00	159	0	0.000	E-W(2):	0.465 *
	TH	2.00	1,229	3,200	0.434 *		
	LT	1.00	81	1,600	0.051	V/C:	0.801
Northbound	RT	1.00	130	1,600	0.031	Lost Time:	0.100
	TH	1.00	380	1,600	0.238 *	ATSAC:	-0.070
	LT	1.00	92	1,600	0.058		
Eastbound	RT	0.00	73	0	0.000	ICU:	0.831
	TH	2.00	788	3,200	0.269		
	LT	1.00	49	1,600	0.031 *	LOS:	D
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.00	125	1,600	0.078	N-S(1):	0.274 *
Approach	Movement RT TH	1.00 1.00	125 260	1,600 1,600	0.078 0.163	N-S(1): N-S(2):	0.274 * 0.189
Approach Southbound	Movement RT TH LT	1.00 1.00 1.00	125 260 178	1,600 1,600 1,600	0.078 0.163 0.111 *	N-S(1): N-S(2): E-W(1):	0.274 * 0.189 0.462
Approach	Movement RT TH LT RT	1.00 1.00 1.00 0.00	125 260 178 272	1,600 1,600 1,600 0	0.078 0.163 0.111 * 0.000	N-S(1): N-S(2):	0.274 * 0.189
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.00 1.00 1.00 0.00 2.00	125 260 178 272 852	1,600 1,600 1,600 0 3,200	0.078 0.163 0.111 * 0.000 0.351 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.274 * 0.189 0.462 0.497 *
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00	125 260 178 272 852 89	1,600 1,600 1,600 0 3,200 1,600	0.078 0.163 0.111 * 0.000 0.351 * 0.056	N-S(1): N-S(2): E-W(1):	0.274 * 0.189 0.462 0.497 *
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00	125 260 178 272 852 89	1,600 1,600 1,600 0 3,200 1,600	0.078 0.163 0.111 * 0.000 0.351 * 0.056 0.004	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.274 * 0.189 0.462 0.497 * 0.771 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00	125 260 178 272 852 89	1,600 1,600 1,600 0 3,200 1,600	0.078 0.163 0.111 * 0.000 0.351 * 0.056	N-S(1): N-S(2): E-W(1): E-W(2):	0.274 * 0.189 0.462 0.497 *
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 178 272 852 89 95 260 41	1,600 1,600 1,600 0 3,200 1,600	0.078 0.163 0.111 * 0.000 0.351 * 0.056 0.004 0.163 * 0.026	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.274 * 0.189 0.462 0.497 * 0.771 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 178 272 852 89 95 260 41	1,600 1,600 1,600 0 3,200 1,600 1,600 1,600	0.078 0.163 0.111 * 0.000 0.351 * 0.056 0.004 0.163 * 0.026 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.274 * 0.189 0.462 0.497 * 0.771 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT TH LT TH	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 178 272 852 89 95 260 41	1,600 1,600 0 3,200 1,600 1,600 1,600 1,600	0.078 0.163 0.111 * 0.000 0.351 * 0.056 0.004 0.163 * 0.026 0.000 0.406	N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.274 * 0.189 0.462 0.497 * 0.771 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.00 1.00 1.00 0.00 2.00 1.00 1.00 1.00	125 260 178 272 852 89 95 260 41	1,600 1,600 0 3,200 1,600 1,600 1,600 0	0.078 0.163 0.111 * 0.000 0.351 * 0.056 0.004 0.163 * 0.026 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.274 * 0.189 0.462 0.497 * 0.771 0.100 -0.070

^{* =} Critical Movement

INT # 14

North/South Street: LANDMARK STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR							
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS		
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000		
	TH	0.00	0	0	0.000 *	N-S(2):	0.034 *		
	LT	0.00	0	0	0.000	E-W(1):	0.319		
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.378 *		
	TH	2.00	1,211	3,200	0.378 *				
	LT	1.00	63	1,600	0.039	V/C:	0.412		
Northbound	RT	1.00	47	1,600	0.000	Lost Time:	0.100		
	TH	0.00	0	0	0.000	ATSAC:	-0.070		
	LT	1.00	54	1,600	0.034 *				
Eastbound	RT	0.00	93	0	0.000	ICU:	0.442		
	TH	2.00	804	3,200	0.280				
	LT	0.00	0	0	0.000 *	LOS:	Α		
Peak Period:	PM PEAK H	IOUR							
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA			
	Movement RT	Lanes 0.00	Volume 0	Capacity 0	0.000	N-S(1):	0.017 *		
Approach	Movement RT TH	0.00 0.00		0	0.000 0.000	N-S(1): N-S(2):	0.017 * 0.014		
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 0.000 *	N-S(1): N-S(2): E-W(1):	0.017 * 0.014 0.397 *		
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 0.000 * 0.000	N-S(1): N-S(2):	0.017 * 0.014		
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 935	0 0 0 0 0 3,200	0.000 0.000 0.000 * 0.000 0.292	N-S(1): N-S(2): E-W(1):	0.017 * 0.014 0.397 * 0.292		
Approach Southbound	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0 0 935 6	0 0 0	0.000 0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.017 * 0.014 0.397 *		
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 935	0 0 0 0 0 3,200	0.000 0.000 0.000 * 0.000 0.292	N-S(1): N-S(2): E-W(1): E-W(2):	0.017 * 0.014 0.397 * 0.292		
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 935 6	0 0 0 0 3,200 1,600	0.000 0.000 0.000 * 0.000 0.292 0.004 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.017 * 0.014 0.397 * 0.292		
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 935 6 33 0	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 * 0.000 0.292 0.004 * 0.017 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.017 * 0.014 0.397 * 0.292  0.414 0.100 -0.070		
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 1.00 0.00	0 0 0 0 935 6 33	0 0 0 0 3,200 1,600 1,600	0.000 0.000 * 0.000 * 0.000 0.292 0.004 * 0.017 * 0.000 0.014	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.017 * 0.014 0.397 * 0.292 0.414 0.100		
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.00 1.00 0.00	0 0 0 935 6 33 0	0 0 0 0 3,200 1,600 1,600 0 1,600	0.000 0.000 0.000 * 0.000 0.292 0.004 * 0.017 * 0.000 0.014	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.017 * 0.014 0.397 * 0.292  0.414 0.100 -0.070		
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.00 1.00 0.00	0 0 0 935 6 33 0 23	0 0 0 0 3,200 1,600 1,600 0 1,600	0.000 0.000 * 0.000 * 0.000 0.292 0.004 * 0.017 * 0.000 0.014	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.017 * 0.014 0.397 * 0.292  0.414 0.100 -0.070		

^{* =} Critical Movement

INT # 14

North/South Street: LANDMARK STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.034 *
	LT	0.00	0	0	0.000	E-W(1):	0.323
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.394 *
	TH	2.00	1,260	3,200	0.394 *		
	LT	1.00	63	1,600	0.039	V/C:	0.428
Northbound	RT	1.00	47	1,600	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.00	54	1,600	0.034 *		
Eastbound	RT	0.00	93	0	0.000	ICU:	0.458
	TH	2.00	815	3,200	0.284		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK F			_			
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	0	0.000	N-S(1):	0.017 *
Approach	Movement RT TH	Lanes 0.00 0.00	0 0	0	0.000 0.000	N-S(1): N-S(2):	0.017 * 0.014
Approach Southbound	Movement RT TH LT	Lanes 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 0.000 *	N-S(1): N-S(2): E-W(1):	0.017 * 0.014 0.414 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 0.000 * 0.000	N-S(1): N-S(2):	0.017 * 0.014
Approach Southbound	Movement RT TH LT	Lanes 0.00 0.00 0.00 0.00 0.00 2.00	0 0 0	0 0 0 0 0 3,200	0.000 0.000 0.000 * 0.000 0.298	N-S(1): N-S(2): E-W(1):	0.017 * 0.014 0.414 * 0.298
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 955 6	0 0 0 0 3,200 1,600	0.000 0.000 0.000 * 0.000 0.298 0.004 *	N-S(1): N-S(2): E-W(1):	0.017 * 0.014 0.414 * 0.298
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 0.00 0.00 0.00 0.00 2.00	0 0 0 0 955	0 0 0 0 0 3,200	0.000 0.000 0.000 * 0.000 0.298	N-S(1): N-S(2): E-W(1): E-W(2):	0.017 * 0.014 0.414 * 0.298
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 955 6	0 0 0 0 3,200 1,600	0.000 0.000 0.000 * 0.000 0.298 0.004 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.017 * 0.014 0.414 * 0.298
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 955 6 33	0 0 0 0 3,200 1,600	0.000 0.000 0.000 * 0.000 0.298 0.004 * 0.017 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:	0.017 * 0.014 0.414 * 0.298 0.431 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 1.00 0.00	0 0 0 0 955 6 33 0	0 0 0 0 3,200 1,600 1,600	0.000 0.000 * 0.000 * 0.000 0.298 0.004 * 0.017 * 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:	0.017 * 0.014 0.414 * 0.298 0.431 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.00 1.00 0.00	0 0 0 955 6 33 0	0 0 0 3,200 1,600 1,600 0 1,600	0.000 0.000 * 0.000 * 0.000 0.298 0.004 * 0.017 * 0.000 0.014	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.017 * 0.014 0.414 * 0.298  0.431 0.100 -0.070

^{* =} Critical Movement

INT # 14

North/South Street: LANDMARK STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

LT   1.00   63   1,600   0.039 *	Peak Period:	AM PEAK H	IOUR					
TH	Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
LT   0.00   0   0   0.000   E-W(1):	Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
Westbound         RT         0.00         0         0         0.000         E-W(2):           TH         2.00         1,401         3,200         0.438 *         LT         V/C:           Northbound         RT         1.00         60         1,600         0.000         Lost Time:           TH         0.00         0         0         0.000         ATSAC:           LT         1.00         63         1,600         0.039 *           Eastbound         RT         0.00         123         0         0.000         ICU:           TH         2.00         950         3,200         0.335         LT         LOS:           Peak Period:         PM PEAK HOUR           Approach         Movement         Lanes         Volume         Capacity         V/C         ICU ANAL           Southbound         RT         0.00         0         0         0.000         N-S(1):           TH         0.00         0         0         0.000         R-S(2):           LT         0.00         0         0         0.000         E-W(1):		TH	0.00	0	0	0.000 *	N-S(2):	0.039 *
TH		LT	0.00	0	0	0.000	E-W(1):	0.402
LT   1.00   107   1,600   0.067   V/C:	Westbound	RT	0.00	0	0	0.000	E-W(2):	0.438 *
Northbound		TH	2.00	1,401	3,200	0.438 *		
TH		LT	1.00	107	1,600	0.067	V/C:	0.477
LT   1.00   63   1,600   0.039 *	Northbound	RT	1.00	60	1,600	0.000	Lost Time:	0.100
RT		TH	0.00	0	0	0.000	ATSAC:	-0.070
TH   2.00   950   3,200   0.335   LT   0.00   0   0   0   0.000 *   LOS:		LT	1.00	63	1,600	0.039 *		
Peak Period:         PM PEAK HOUR           Approach         Movement         Lanes         Volume         Capacity         V/C         ICU ANAL           Southbound         RT         0.00         0         0         0.000         N-S(1):           TH         0.00         0         0         0.000         N-S(2):           LT         0.00         0         0         0.000         E-W(1):	Eastbound	RT	0.00	123	0	0.000	ICU:	0.507
Peak Period:         PM PEAK HOUR           Approach         Movement         Lanes         Volume         Capacity         V/C         ICU ANAL           Southbound         RT         0.00         0         0         0.000         N-S(1):           TH         0.00         0         0         0.000         N-S(2):           LT         0.00         0         0         0.000         E-W(1):		TH	2.00	950	3,200	0.335		
Approach         Movement         Lanes         Volume         Capacity         V/C         ICU ANAL           Southbound         RT         0.00         0         0         0.000         N-S(1):           TH         0.00         0         0         0.000 *         N-S(2):           LT         0.00         0         0         0.000         E-W(1):		LT	0.00	0	0	0.000 *	LOS:	Α
Approach         Movement         Lanes         Volume         Capacity         V/C         ICU ANAL           Southbound         RT         0.00         0         0         0.000         N-S(1):           TH         0.00         0         0         0.000 *         N-S(2):           LT         0.00         0         0         0.000         E-W(1):								
Southbound         RT         0.00         0         0         0.000         N-S(1):           TH         0.00         0         0         0.000 *         N-S(2):           LT         0.00         0         0         0.000         E-W(1):								
TH 0.00 0 0 0.000 * N-S(2): LT 0.00 0 0 0.000 E-W(1):					. ,			
LT 0.00 0 0 0.000 E-W(1):	Southbound			_	0		` ,	0.018
					_		` ,	0.039 *
							` '	0.505 *
	Westbound	RT	0.00	0	0	0.000	E-W(2):	0.355
TH 2.00 1,136 3,200 0.355					,			
LT 1.00 66 1,600 0.041 * V/C:			1.00		,	0.041 *	V/C:	0.544
Northbound	Northbound	RT	1.00	94	1,600	0.018	Lost Time:	0.100
TH 0.00 0 0.000 ATSAC:		TH	0.00	0	0	0.000	ATSAC:	-0.070
LT 1.00 63 1,600 0.039 *					1,600			
Fastbound RT 0.00 46 0 0.000 ICH:	Eastbound	RT	0.00	46	0	0.000	ICU:	0.574
Labelle   10   0.00   10   0.000   100.			2.00	1 440	3 200	0.464 *		
TH 2.00 1,440 3,200 0.464 *		I H	2.00	1,440	3,200	0.404		

^{* =} Critical Movement

INT # 14

North/South Street: LANDMARK STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.039 *
	LT	0.00	0	0	0.000	E-W(1):	0.406
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.453 *
	TH	2.00	1,450	3,200	0.453 *		
	LT	1.00	107	1,600	0.067	V/C:	0.492
Northbound	RT	1.00	60	1,600	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.00	63	1,600	0.039 *		
Eastbound	RT	0.00	123	0	0.000	ICU:	0.522
	TH	2.00	961	3,200	0.339		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.018
	TH	0.00	0	0	$\wedge$ $\wedge \wedge \wedge \wedge$ *	NI C/O\.	$\wedge \wedge \wedge \wedge \wedge \star$
				-	0.000 *	N-S(2):	0.039 *
	LT	0.00	0	0	0.000	E-W(1):	0.523 *
Westbound	RT	0.00	0	0	0.000 0.000	, ,	
Westbound	RT TH	0.00 2.00	0 1,156	0 0 3,200	0.000 0.000 0.361	E-W(1):	0.523 * 0.361
	RT TH LT	0.00 2.00 1.00	0 1,156 66	0 0 3,200 1,600	0.000 0.000 0.361 0.041 *	E-W(1): E-W(2): V/C:	0.523 * 0.361 0.562
Westbound  Northbound	RT TH LT RT	0.00 2.00 1.00 1.00	0 1,156 66 94	0 0 3,200	0.000 0.000 0.361 0.041 *	E-W(1): E-W(2): V/C: Lost Time:	0.523 * 0.361 0.562 0.100
	RT TH LT	0.00 2.00 1.00	0 1,156 66 94 0	0 0 3,200 1,600 1,600 0	0.000 0.000 0.361 0.041 * 0.018 0.000	E-W(1): E-W(2): V/C:	0.523 * 0.361 0.562
Northbound	RT TH LT RT TH LT	0.00 2.00 1.00 1.00	0 1,156 66 94 0 63	0 0 3,200 1,600 1,600 0 1,600	0.000 0.000 0.361 0.041 * 0.018 0.000 0.039 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.523 * 0.361 0.562 0.100 -0.070
	RT TH LT RT TH LT	0.00 2.00 1.00 1.00 0.00	0 1,156 66 94 0 63 46	0 0 3,200 1,600 1,600 0 1,600	0.000 0.000 0.361 0.041 * 0.018 0.000 0.039 * 0.000	E-W(1): E-W(2): V/C: Lost Time:	0.523 * 0.361 0.562 0.100
Northbound	RT TH LT RT TH LT	0.00 2.00 1.00 1.00 0.00 1.00	0 1,156 66 94 0 63	0 0 3,200 1,600 1,600 0 1,600	0.000 0.000 0.361 0.041 * 0.018 0.000 0.039 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.523 * 0.361 0.562 0.100 -0.070

^{* =} Critical Movement

**INT #15** 

North/South Street: NATIONAL BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	82	0	0.000	N-S(1):	0.268
	TH	2.00	684	3,200	0.239 *	N-S(2):	0.312 *
	LT	2.00	82	2,880	0.028	E-W(1):	0.286
Westbound	RT	0.00	181	0	0.000	E-W(2):	0.328 *
	TH	3.00	1,213	4,800	0.290 *		
	LT	1.00	162	1,600	0.101	V/C:	0.640
Northbound	RT	0.00	36	0	0.000	Lost Time:	0.100
	TH	2.00	733	3,200	0.240	ATSAC:	-0.070
	LT	2.00	211	2,880	0.073 *		
Eastbound	RT	1.00	140	1,600	0.022	ICU:	0.670
	TH	2.00	592	3,200	0.185		
	LT	1.00	61	1,600	0.038 *	LOS:	В
Peak Period:	PM PEAK H	IOUD					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	I VSIS
Southbound	RT	0.00	52	0	0.000	N-S(1):	0.339
Codtribodina	TH	2.00	937	3,200	0.309 *	N-S(2):	0.382 *
	LT	2.00	240	2,880	0.083	E-W(1):	0.404 *
Westbound	RT	0.00	104	0	0.000	E-W(2):	0.238
	TH	3.00	783	4,800	0.185	, ,	
	LT	1.00	126	1,600	0.079 *	V/C:	0.786
Northbound	RT	0.00	80	0	0.000	Lost Time:	0.100
	TH	2.00	740	3,200	0.256	ATSAC:	-0.070
	LT	2.00	209	2,880	0.073 *		
Eastbound	RT	1.00	200	1,600	0.060	ICU:	0.816
	TH	2.00	1,039	3,200	0.325 *		
	LT	1.00	85	1,600	0.053	LOS:	D
	LI	1.00		1,000	0.000	L00.	

^{* =} Critical Movement

**INT #15** 

North/South Street: NATIONAL BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	100	0	0.000	N-S(1):	0.268
	TH	2.00	684	3,200	0.245 *	N-S(2):	0.324 *
	LT	2.00	82	2,880	0.028	E-W(1):	0.287
Westbound	RT	0.00	181	0	0.000	E-W(2):	0.335 *
	TH	3.00	1,228	4,800	0.294 *		
	LT	1.00	162	1,600	0.101	V/C:	0.659
Northbound	RT	0.00	36	0	0.000	Lost Time:	0.100
	TH	2.00	733	3,200	0.240	ATSAC:	-0.070
	LT	2.00	227	2,880	0.079 *		
Eastbound	RT	1.00	144	1,600	0.019	ICU:	0.689
	TH	2.00	595	3,200	0.186		
	LT	1.00	65	1,600	0.041 *	LOS:	В
		10115					
Peak Period:	PM PEAK F		\/ali vaa	O a m a aith i	V/C	ICI I ANIA	1 1/010
Approach	Movement	Lanes	Volume	Capacity		ICU ANA	
Southbound	RT	0.00	59	0	0.000	N-S(1):	0.339
	TH	2.00	937	3,200	0.311 *	N-S(2):	0.386 *
Ma ath a cad	LT	2.00	240	2,880	0.083	E-W(1):	0.409 *
Westbound	RT	0.00	104	0	0.000	E-W(2):	0.252
	TH	3.00	789	4,800	0.186	\//O	0.705
N. a.i.	LT	1.00	126	1,600	0.079 *	V/C:	0.795
Northbound	RT	0.00	80	0	0.000	Lost Time:	0.100
	TH	2.00	740	3,200	0.256	ATSAC:	-0.070
	LT	2.00	216	2,880	0.075 *		
Eastbound	RT	1.00	218	1,600	0.069	ICU:	0.825
	TH	2.00	1,055	3,200	0.330 *		
	LT	1.00	105	1,600	0.066	LOS:	D

^{* =} Critical Movement

**INT #15** 

North/South Street: NATIONAL BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	107	0	0.000	N-S(1):	0.348
	TH	2.00	853	3,200	0.300 *	N-S(2):	0.415 *
	LT	2.00	168	2,880	0.058	E-W(1):	0.316
Westbound	RT	0.00	203	0	0.000	E-W(2):	0.372 *
	TH	3.00	1,345	4,800	0.323 *		
	LT	1.00	173	1,600	0.108	V/C:	0.787
Northbound	RT	0.00	84	0	0.000	Lost Time:	0.100
	TH	2.00	844	3,200	0.290	ATSAC:	-0.070
	LT	2.00	331	2,880	0.115 *		
Eastbound	RT	1.00	207	1,600	0.026	ICU:	0.817
	TH	2.00	666	3,200	0.208		
	LT	4 00	78	1,600	0.049 *	LOS:	D
	LI	1.00	70	1,000	0.049	LUS.	U
Peak Period:	PM PEAK H		70	1,600	0.049	LU3.	<u>U</u>
Peak Period: Approach			Volume	Capacity	V/C	ICU ANA	
	PM PEAK H	IOUR		·			
Approach	PM PEAK H	IOUR Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Approach	PM PEAK H Movement RT	IOUR Lanes 0.00	Volume 80	Capacity 0	V/C 0.000	ICU ANA N-S(1):	LYSIS 0.429
Approach	PM PEAK H Movement RT TH	Lanes 0.00 2.00	Volume 80 1,108	Capacity 0 3,200	V/C 0.000 0.371 *	ICU ANA N-S(1): N-S(2):	LYSIS 0.429 0.487 *
Approach Southbound	PM PEAK H Movement RT TH LT	Lanes 0.00 2.00 2.00	Volume 80 1,108 331	Capacity 0 3,200 2,880	V/C 0.000 0.371 * 0.115	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.429 0.487 * 0.465 *
Approach Southbound	PM PEAK H Movement RT TH LT RT	Lanes 0.00 2.00 2.00 0.00	Volume 80 1,108 331 160	Capacity 0 3,200 2,880 0	V/C 0.000 0.371 * 0.115 0.000	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.429 0.487 * 0.465 *
Approach Southbound	PM PEAK H  Movement  RT  TH  LT  RT  RT	Lanes 0.00 2.00 2.00 0.00 3.00	Volume 80 1,108 331 160 915	Capacity 0 3,200 2,880 0 4,800	V/C 0.000 0.371 * 0.115 0.000 0.224	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):	0.429 0.487 * 0.465 * 0.304
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00	Volume 80 1,108 331 160 915 167	Capacity 0 3,200 2,880 0 4,800 1,600	V/C 0.000 0.371 * 0.115 0.000 0.224 0.104 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.429 0.487 * 0.465 * 0.304
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00	Volume 80 1,108 331 160 915 167 108	Capacity 0 3,200 2,880 0 4,800 1,600	V/C 0.000 0.371 * 0.115 0.000 0.224 0.104 * 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time:	0.429 0.487 * 0.465 * 0.304 0.952 0.100
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  TH  LT  TH  LT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00 2.00	Volume 80 1,108 331 160 915 167 108 896	Capacity 0 3,200 2,880 0 4,800 1,600 0 3,200	V/C 0.000 0.371 * 0.115 0.000 0.224 0.104 * 0.000 0.314	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time:	0.429 0.487 * 0.465 * 0.304 0.952 0.100
Approach Southbound Westbound Northbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  TH  LT  RT  TH  LT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00 2.00 2.00	Volume 80 1,108 331 160 915 167 108 896 335	Capacity  0 3,200 2,880 0 4,800 1,600 0 3,200 2,880	V/C 0.000 0.371 * 0.115 0.000 0.224 0.104 * 0.000 0.314 0.116 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.429 0.487 * 0.465 * 0.304 0.952 0.100 -0.070

^{* =} Critical Movement

**INT #15** 

North/South Street: NATIONAL BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Book Books I	AM DE ALC I	IOLID					
Peak Period:	AM PEAK H		\/ali ves s	O = = = it :	V/C	IOLL ANIA	1.7/010
Approach	Movement	Lanes	Volume	Capacity	_	ICU ANA	
Southbound	RT	0.00	125	0	0.000	N-S(1):	0.348
	TH	2.00	853	3,200	0.306 *	N-S(2):	0.426 *
	LT	2.00	168	2,880	0.058	E-W(1):	0.317
Westbound	RT	0.00	203	0	0.000	E-W(2):	0.377 *
	TH	3.00	1,360	4,800	0.326 *		
	LT	1.00	173	1,600	0.108	V/C:	0.803
Northbound	RT	0.00	84	0	0.000	Lost Time:	0.100
	TH	2.00	844	3,200	0.290	ATSAC:	-0.070
	LT	2.00	347	2,880	0.120 *		
Eastbound	RT	1.00	211	1,600	0.023	ICU:	0.833
	TH	2.00	669	3,200	0.209		
	LT	1.00	82	1,600	0.051 *	LOS:	D
Peak Period:	PM PEAK H	IOUR					
Peak Period: Approach	PM PEAK H	IOUR Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
			Volume 87	Capacity 0	V/C 0.000	ICU ANA N-S(1):	LYSIS 0.429
Approach	Movement	Lanes					
Approach	Movement RT	Lanes 0.00	87	0	0.000	N-S(1):	0.429
Approach	Movement RT TH	Lanes 0.00 2.00	87 1,108	0 3,200	0.000 0.373 *	N-S(1): N-S(2):	0.429 0.492 *
Approach Southbound	Movement RT TH LT	Lanes 0.00 2.00 2.00	87 1,108 331	0 3,200 2,880	0.000 0.373 * 0.115	N-S(1): N-S(2): E-W(1):	0.429 0.492 * 0.470 *
Approach Southbound	Movement RT TH LT RT	Lanes 0.00 2.00 2.00 0.00	87 1,108 331 160	0 3,200 2,880 0	0.000 0.373 * 0.115 0.000	N-S(1): N-S(2): E-W(1):	0.429 0.492 * 0.470 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 2.00 2.00 0.00 3.00	87 1,108 331 160 921	0 3,200 2,880 0 4,800	0.000 0.373 * 0.115 0.000 0.225	N-S(1): N-S(2): E-W(1): E-W(2):	0.429 0.492 * 0.470 * 0.318
Approach Southbound Westbound	Movement RT TH LT RT RT TH LT TH	Lanes 0.00 2.00 2.00 0.00 3.00 1.00	87 1,108 331 160 921 167	0 3,200 2,880 0 4,800 1,600	0.000 0.373 * 0.115 0.000 0.225 0.104 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.429 0.492 * 0.470 * 0.318
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00	87 1,108 331 160 921 167 108	0 3,200 2,880 0 4,800 1,600	0.000 0.373 * 0.115 0.000 0.225 0.104 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.429 0.492 * 0.470 * 0.318 0.962 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00 2.00	87 1,108 331 160 921 167 108 896	0 3,200 2,880 0 4,800 1,600 0 3,200	0.000 0.373 * 0.115 0.000 0.225 0.104 * 0.000 0.314	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.429 0.492 * 0.470 * 0.318 0.962 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT TH LT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00 2.00 2.00	87 1,108 331 160 921 167 108 896 342	0 3,200 2,880 0 4,800 1,600 0 3,200 2,880	0.000 0.373 * 0.115 0.000 0.225 0.104 * 0.000 0.314 0.119 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.429 0.492 * 0.470 * 0.318 0.962 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 2.00 2.00 0.00 3.00 1.00 0.00 2.00 2.00 1.00	87 1,108 331 160 921 167 108 896 342 309	0 3,200 2,880 0 4,800 1,600 0 3,200 2,880 1,600	0.000 0.373 * 0.115 0.000 0.225 0.104 * 0.000 0.314 0.119 * 0.086	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.429 0.492 * 0.470 * 0.318 0.962 0.100 -0.070

^{* =} Critical Movement

**INT #16** 

North/South Street: HELMS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Ν
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANAL	_YSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.015
	TH	0.00	0	0	0.000 *	N-S(2):	0.071 *
	LT	0.00	0	0	0.000	E-W(1):	0.240
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.439 *
	TH	2.00	1,404	3,200	0.439 *		
	LT	1.00	11	1,600	0.007	V/C:	0.510
Northbound	RT	0.12	14	196	0.015	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.88	100	1,404	0.071 *		
Eastbound	RT	0.00	23	0	0.000	ICU:	0.540
	TH	2.00	723	3,200	0.233		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H					I IOII ANIAI	\ <u> </u>
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANAL	
	Movement RT	Lanes 0.00	0	0	0.000	N-S(1):	0.000
Approach	Movement RT TH	Lanes 0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.000 0.047 *
Approach Southbound	Movement RT TH LT	Lanes 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.000 0.047 * 0.433 *
Approach	Movement RT TH LT RT	Lanes 0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.000 0.047 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 0 899	0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.281	N-S(1): N-S(2): E-W(1): E-W(2):	0.000 0.047 * 0.433 * 0.281
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 899 22	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.281 0.014 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.000 0.047 * 0.433 * 0.281
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07	0 0 0 0 899 22 5	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.281 0.014 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.047 * 0.433 * 0.281 0.480 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00	0 0 0 0 899 22 5 0	0 0 0 0 3,200 1,600 107 0	0.000 0.000 * 0.000 0.000 0.281 0.014 * 0.000 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.000 0.047 * 0.433 * 0.281
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93	0 0 0 0 899 22 5 0 70	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.281 0.014 * 0.000 0.000 0.047 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.000 0.047 * 0.433 * 0.281 0.480 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93 0.00	0 0 0 0 899 22 5 0 70	0 0 0 0 3,200 1,600 107 0 1,493	0.000 0.000 * 0.000 0.000 0.281 0.014 * 0.000 0.000 0.047 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.047 * 0.433 * 0.281 0.480 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93	0 0 0 0 899 22 5 0 70	0 0 0 0 3,200 1,600 107 0 1,493	0.000 0.000 * 0.000 0.000 0.281 0.014 * 0.000 0.000 0.047 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.000 0.047 * 0.433 * 0.281 0.480 0.100 -0.070

^{* =} Critical Movement

**INT #16** 

North/South Street: HELMS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.015
	TH	0.00	0	0	0.000 *	N-S(2):	0.071 *
	LT	0.00	0	0	0.000	E-W(1):	0.241
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.443 *
	TH	2.00	1,419	3,200	0.443 *		
	LT	1.00	11	1,600	0.007	V/C:	0.514
Northbound	RT	0.12	14	196	0.015	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.88	100	1,404	0.071 *		
Eastbound	RT	0.00	23	0	0.000	ICU:	0.544
	TH	2.00	726	3,200	0.234		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	Capacity 0	0.000	N-S(1):	0.000
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.000 0.047 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.000 0.047 * 0.438 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.000 0.047 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.000 0.047 * 0.438 *
Approach Southbound	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2): E-W(1):	0.000 0.047 * 0.438 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 905	0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.283	N-S(1): N-S(2): E-W(1): E-W(2):	0.000 0.047 * 0.438 * 0.283
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 905 22	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.283 0.014 *	N-S(1): N-S(2): E-W(1): E-W(2):	0.000 0.047 * 0.438 * 0.283
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07	0 0 0 0 905 22 5	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.283 0.014 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.047 * 0.438 * 0.283 0.485 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00	0 0 0 0 905 22 5 0	0 0 0 0 3,200 1,600 107 0	0.000 0.000 * 0.000 0.000 0.283 0.014 * 0.000 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.047 * 0.438 * 0.283 0.485 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93	0 0 0 0 905 22 5 0 70	0 0 0 0 3,200 1,600 107 0 1,493	0.000 0.000 * 0.000 0.000 0.283 0.014 * 0.000 0.000 0.047 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.000 0.047 * 0.438 * 0.283 0.485 0.100 -0.070

^{* =} Critical Movement

**INT #16** 

North/South Street: HELMS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.016
	TH	0.00	0	0	0.000 *	N-S(2):	0.073 *
	LT	0.00	0	0	0.000	E-W(1):	0.276
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.497 *
	TH	2.00	1,591	3,200	0.497 *		
	LT	1.00	11	1,600	0.007	V/C:	0.570
Northbound	RT	0.12	14	193	0.016	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.88	102	1,407	0.073 *		
Eastbound	RT	0.00	23	0	0.000	ICU:	0.600
	TH	2.00	838	3,200	0.269		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	Capacity 0	0.000	N-S(1):	0.000
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.000 0.048 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.000 0.048 * 0.510 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.000 0.048 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 1,044	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.326	N-S(1): N-S(2): E-W(1): E-W(2):	0.000 0.048 * 0.510 * 0.326
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	0.00 0.00 0.00 0.00	0 0 0 0 1,044 22	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.326 0.014 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.000 0.048 * 0.510 * 0.326
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07	0 0 0 0 1,044	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.326 0.014 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2):	0.000 0.048 * 0.510 * 0.326
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 1,044 22	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.326 0.014 * 0.000 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.000 0.048 * 0.510 * 0.326
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07	0 0 0 1,044 22 5 0 71	0 0 0 0 3,200 1,600 105	0.000 0.000 * 0.000 0.000 0.326 0.014 * 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.000 0.048 * 0.510 * 0.326 0.558 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00	0 0 0 0 1,044 22 5	0 0 0 0 3,200 1,600 105 0	0.000 0.000 * 0.000 0.000 0.326 0.014 * 0.000 0.000 0.048 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.048 * 0.510 * 0.326 0.558 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93	0 0 0 1,044 22 5 0 71	0 0 0 0 3,200 1,600 105 0 1,495	0.000 0.000 * 0.000 0.000 0.326 0.014 * 0.000 0.000 0.048 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.000 0.048 * 0.510 * 0.326 0.558 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93 0.00	0 0 0 1,044 22 5 0 71	0 0 0 0 3,200 1,600 105 0 1,495	0.000 0.000 * 0.000 0.000 0.326 0.014 * 0.000 0.000 0.048 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.000 0.048 * 0.510 * 0.326 0.558 0.100 -0.070

^{* =} Critical Movement

**INT #16** 

North/South Street: HELMS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.016
	TH	0.00	0	0	0.000 *	N-S(2):	0.073 *
	LT	0.00	0	0	0.000	E-W(1):	0.277
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.502 *
	TH	2.00	1,606	3,200	0.502 *		
	LT	1.00	11	1,600	0.007	V/C:	0.575
Northbound	RT	0.12	14	193	0.016	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.88	102	1,407	0.073 *		
Eastbound	RT	0.00	23	0	0.000	ICU:	0.605
	TH	2.00	841	3,200	0.270		
	LT	0.00	0	0	0.000 *	LOS:	В
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	0	0.000	N-S(1):	0.000
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.000 0.048 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.000 0.048 * 0.515 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.000 0.048 *
Approach Southbound	Movement RT TH LT RT TH	0.00 0.00 0.00 0.00 0.00 2.00	0 0 0 0 1,050	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.328	N-S(1): N-S(2): E-W(1): E-W(2):	0.000 0.048 * 0.515 * 0.328
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 1,050 22	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.328 0.014 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.000 0.048 * 0.515 * 0.328
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07	0 0 0 0 1,050 22 5	0 0 0 0 3,200 1,600 105	0.000 0.000 * 0.000 0.000 0.328 0.014 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.048 * 0.515 * 0.328 0.563 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00	0 0 0 0 1,050 22 5 0	0 0 0 0 3,200 1,600 105 0	0.000 0.000 * 0.000 0.000 0.328 0.014 * 0.000 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.000 0.048 * 0.515 * 0.328
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93	0 0 0 1,050 22 5 0 71	0 0 0 0 3,200 1,600 105 0 1,495	0.000 0.000 * 0.000 0.000 0.328 0.014 * 0.000 0.000 0.048 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.000 0.048 * 0.515 * 0.328 0.563 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93 0.00	0 0 0 1,050 22 5 0 71	0 0 0 0 3,200 1,600 105 0 1,495	0.000 0.000 * 0.000 0.000 0.328 0.014 * 0.000 0.000 0.048 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.000 0.048 * 0.515 * 0.328 0.563 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93 0.00 2.00	0 0 0 1,050 22 5 0 71	0 0 0 3,200 1,600 105 0 1,495 0 3,200	0.000 0.000 * 0.000 0.000 0.328 0.014 * 0.000 0.000 0.048 * 0.000 0.501 *	N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.000 0.048 * 0.515 * 0.328 0.563 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.07 0.00 0.93 0.00	0 0 0 1,050 22 5 0 71	0 0 0 0 3,200 1,600 105 0 1,495	0.000 0.000 * 0.000 0.000 0.328 0.014 * 0.000 0.000 0.048 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.000 0.048 * 0.515 * 0.328 0.563 0.100 -0.070

^{* =} Critical Movement

INT # 17

North/South Street: LA CIENEGA AVENUE - MCMANUS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.93	134	3,092	0.038	N-S(1):	0.103 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.07	74	1,537	0.048 *	E-W(1):	0.222
Westbound	RT	0.00	28	0	0.000	E-W(2):	0.440 *
	TH	2.00	1,351	3,200	0.431 *		
	LT	1.00	14	1,600	0.009	V/C:	0.543
Northbound	RT	0.24	21	382	0.018	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.76	67	1,218	0.055 *		
Eastbound	RT	0.00	10	0	0.000	ICU:	0.573
	TH	2.00	670	3,200	0.213		
	LT	1.00	15	1,600	0.009 *	LOS:	Α
I Book Boriodi	DMDEAKL						
Peak Period:	PM PEAK F		Volume	Canacity	V/C	ICH ANA	I VSIS
Approach	Movement	Lanes	Volume 92	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.49	92	2,387	0.030	N-S(1):	0.104 *
Approach	Movement RT TH	Lanes 1.49 0.00	92 0	2,387 0	0.030 0.000	N-S(1): N-S(2):	0.104 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 1.49 0.00 1.51	92 0 93	2,387	0.030 0.000 0.043 *	N-S(1): N-S(2): E-W(1):	0.104 * 0.000 0.387 *
Approach	Movement RT TH LT RT	Lanes 1.49 0.00 1.51 0.00	92 0 93 31	2,387 0 2,172 0	0.030 0.000 0.043 * 0.000	N-S(1): N-S(2):	0.104 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 1.49 0.00 1.51	92 0 93	2,387 0 2,172	0.030 0.000 0.043 *	N-S(1): N-S(2): E-W(1):	0.104 * 0.000 0.387 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 1.49 0.00 1.51 0.00 2.00	92 0 93 31 711	2,387 0 2,172 0 3,200	0.030 0.000 0.043 * 0.000 0.232	N-S(1): N-S(2): E-W(1): E-W(2):	0.104 * 0.000 0.387 * 0.245
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.49 0.00 1.51 0.00 2.00 1.00	92 0 93 31 711 10	2,387 0 2,172 0 3,200 1,600	0.030 0.000 0.043 * 0.000 0.232 0.006 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.104 * 0.000 0.387 * 0.245
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21	92 0 93 31 711 10 21	2,387 0 2,172 0 3,200 1,600 343	0.030 0.000 0.043 * 0.000 0.232 0.006 * 0.032	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.104 * 0.000 0.387 * 0.245  0.491 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21 0.00	92 0 93 31 711 10 21 0	2,387 0 2,172 0 3,200 1,600 343 0	0.030 0.000 0.043 * 0.000 0.232 0.006 * 0.032 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.104 * 0.000 0.387 * 0.245  0.491 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21 0.00 0.79	92 0 93 31 711 10 21 0 77	2,387 0 2,172 0 3,200 1,600 343 0 1,257	0.030 0.000 0.043 * 0.000 0.232 0.006 * 0.032 0.000 0.061 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.104 * 0.000 0.387 * 0.245  0.491 0.100 -0.070

^{* =} Critical Movement

INT # 17

North/South Street: LA CIENEGA AVENUE - MCMANUS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.94	136	3,109	0.039	N-S(1):	0.104 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.06	74	1,522	0.049 *	E-W(1):	0.222
Westbound	RT	0.00	28	0	0.000	E-W(2):	0.444 *
	TH	2.00	1,363	3,200	0.435 *		
	LT	1.00	14	1,600	0.009	V/C:	0.548
Northbound	RT	0.24	21	382	0.018	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.76	67	1,218	0.055 *		
Eastbound	RT	0.00	10	0	0.000	ICU:	0.578
	TH	2.00	673	3,200	0.213		
	LT	1.00	15	1,600	0.009 *	LOS:	Α
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.50	93	2,400	0.030	N-S(1):	0.104 *
Approach	Movement RT TH	1.50 0.00	93 0	2,400 0	0.030 0.000	N-S(1): N-S(2):	0.104 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 1.50 0.00 1.50	93 0 93	2,400 0 2,160	0.030 0.000 0.043 *	N-S(1): N-S(2): E-W(1):	0.104 * 0.000 0.392 *
Approach	Movement RT TH LT RT	1.50 0.00 1.50 0.00	93 0 93 31	2,400 0 2,160 0	0.030 0.000 0.043 * 0.000	N-S(1): N-S(2):	0.104 * 0.000
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 1.50 0.00 1.50 0.00 2.00	93 0 93 31 716	2,400 0 2,160 0 3,200	0.030 0.000 0.043 * 0.000 0.233	N-S(1): N-S(2): E-W(1):	0.104 * 0.000 0.392 * 0.246
Approach Southbound	Movement RT TH LT RT	1.50 0.00 1.50 0.00	93 0 93 31	2,400 0 2,160 0	0.030 0.000 0.043 * 0.000	N-S(1): N-S(2): E-W(1):	0.104 * 0.000 0.392 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 1.50 0.00 1.50 0.00 2.00	93 0 93 31 716	2,400 0 2,160 0 3,200	0.030 0.000 0.043 * 0.000 0.233	N-S(1): N-S(2): E-W(1): E-W(2):	0.104 * 0.000 0.392 * 0.246
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 1.50 0.00 1.50 0.00 2.00 1.00	93 0 93 31 716 10	2,400 0 2,160 0 3,200 1,600	0.030 0.000 0.043 * 0.000 0.233 0.006 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.104 * 0.000 0.392 * 0.246
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.50 0.00 1.50 0.00 2.00 1.00 0.21	93 0 93 31 716 10 21 0	2,400 0 2,160 0 3,200 1,600 343	0.030 0.000 0.043 * 0.000 0.233 0.006 * 0.032	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.104 * 0.000 0.392 * 0.246  0.496 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.50 0.00 1.50 0.00 2.00 1.00 0.21 0.00	93 0 93 31 716 10 21 0	2,400 0 2,160 0 3,200 1,600 343 0	0.030 0.000 0.043 * 0.000 0.233 0.006 * 0.032 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.104 * 0.000 0.392 * 0.246 0.496 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.50 0.00 1.50 0.00 2.00 1.00 0.21 0.00 0.79	93 0 93 31 716 10 21 0	2,400 0 2,160 0 3,200 1,600 343 0 1,257	0.030 0.000 0.043 * 0.000 0.233 0.006 * 0.032 0.000 0.061 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.104 * 0.000 0.392 * 0.246  0.496 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 1.50 0.00 1.50 0.00 2.00 1.00 0.21 0.00 0.79 0.00	93 0 93 31 716 10 21 0 77 20	2,400 0 2,160 0 3,200 1,600 343 0 1,257	0.030 0.000 0.043 * 0.000 0.233 0.006 * 0.032 0.000 0.061 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.104 * 0.000 0.392 * 0.246  0.496 0.100 -0.070

^{* =} Critical Movement

INT # 17

North/South Street: LA CIENEGA AVENUE - MCMANUS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.99	147	3,178	0.042	N-S(1):	0.107 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.01	75	1,459	0.051 *	E-W(1):	0.248
Westbound	RT	0.00	29	0	0.000	E-W(2):	0.491 *
	TH	2.00	1,514	3,200	0.482 *		
	LT	1.00	14	1,600	0.009	V/C:	0.598
Northbound	RT	0.24	21	378	0.019	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.76	68	1,222	0.056 *		
Eastbound	RT	0.00	10	0	0.000	ICU:	0.628
	TH	2.00	755	3,200	0.239		
	LT	1.00	15	1,600	0.009 *	LOS:	В
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 1.49	94	2,387	0.031	N-S(1):	0.107 *
Approach	Movement RT TH	1.49 0.00	94 0	2,387 0	0.031 0.000	N-S(1): N-S(2):	0.107 * 0.000
Approach Southbound	Movement RT TH LT	Lanes 1.49 0.00 1.51	94 0 95	2,387 0 2,171	0.031 0.000 0.044 *	N-S(1): N-S(2): E-W(1):	0.107 * 0.000 0.448 *
Approach	Movement RT TH LT RT	1.49 0.00 1.51 0.00	94 0 95 32	2,387 0 2,171 0	0.031 0.000 0.044 * 0.000	N-S(1): N-S(2):	0.107 * 0.000
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.49 0.00 1.51 0.00 2.00	94 0 95 32 835	2,387 0 2,171 0 3,200	0.031 0.000 0.044 * 0.000 0.271	N-S(1): N-S(2): E-W(1): E-W(2):	0.107 * 0.000 0.448 * 0.284
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT	Lanes 1.49 0.00 1.51 0.00 2.00 1.00	94 0 95 32 835 10	2,387 0 2,171 0 3,200 1,600	0.031 0.000 0.044 * 0.000 0.271 0.006 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.107 * 0.000 0.448 * 0.284
Approach Southbound	Movement RT TH LT RT TH	Lanes 1.49 0.00 1.51 0.00 2.00	94 0 95 32 835	2,387 0 2,171 0 3,200	0.031 0.000 0.044 * 0.000 0.271	N-S(1): N-S(2): E-W(1): E-W(2):	0.107 * 0.000 0.448 * 0.284
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT	Lanes 1.49 0.00 1.51 0.00 2.00 1.00	94 0 95 32 835 10	2,387 0 2,171 0 3,200 1,600 336 0	0.031 0.000 0.044 * 0.000 0.271 0.006 * 0.033 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.107 * 0.000 0.448 * 0.284
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21	94 0 95 32 835 10 21 0	2,387 0 2,171 0 3,200 1,600 336	0.031 0.000 0.044 * 0.000 0.271 0.006 * 0.033 0.000 0.063 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.107 * 0.000 0.448 * 0.284  0.555 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21 0.00	94 0 95 32 835 10 21	2,387 0 2,171 0 3,200 1,600 336 0	0.031 0.000 0.044 * 0.000 0.271 0.006 * 0.033 0.000 0.063 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.107 * 0.000 0.448 * 0.284 0.555 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21 0.00 0.79	94 0 95 32 835 10 21 0	2,387 0 2,171 0 3,200 1,600 336 0 1,264	0.031 0.000 0.044 * 0.000 0.271 0.006 * 0.033 0.000 0.063 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.107 * 0.000 0.448 * 0.284  0.555 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT RT TH LT RT RT TH LT RT TH LT RT	Lanes 1.49 0.00 1.51 0.00 2.00 1.00 0.21 0.00 0.79 0.00	94 0 95 32 835 10 21 0 79	2,387 0 2,171 0 3,200 1,600 336 0 1,264	0.031 0.000 0.044 * 0.000 0.271 0.006 * 0.033 0.000 0.063 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.107 * 0.000 0.448 * 0.284  0.555 0.100 -0.070

^{* =} Critical Movement

INT # 17

North/South Street: LA CIENEGA AVENUE - MCMANUS AVENUE

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	2.00	149	3,193	0.042	N-S(1):	0.108 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.00	75	1,446	0.052 *	E-W(1):	0.249
Westbound	RT	0.00	29	0	0.000	E-W(2):	0.495 *
	TH	2.00	1,526	3,200	0.486 *		
	LT	1.00	14	1,600	0.009	V/C:	0.603
Northbound	RT	0.24	21	378	0.019	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.76	68	1,222	0.056 *		
Eastbound	RT	0.00	10	0	0.000	ICU:	0.633
	TH	2.00	758	3,200	0.240		
	LT	1.00	15	1,600	0.009 *	LOS:	В
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
Southbound	RT	1.50	95	2,400	0.031	N-S(1):	0.107 *
	TH	0.00	0	0	0 000		0 000
			-	ŭ	0.000	N-S(2):	0.000
	LT	1.50	95	2,160	0.044 *	E-W(1):	0.453 *
Westbound	RT	1.50 0.00	95 32	2,160 0	0.044 * 0.000	, ,	
Westbound	RT TH	1.50 0.00 2.00	95 32 840	2,160 0 3,200	0.044 * 0.000 0.273	E-W(1):	0.453 * 0.286
	RT TH LT	1.50 0.00 2.00 1.00	95 32 840 10	2,160 0 3,200 1,600	0.044 * 0.000 0.273 0.006 *	E-W(1): E-W(2): V/C:	0.453 * 0.286 0.560
Westbound  Northbound	RT TH LT RT	1.50 0.00 2.00 1.00 0.21	95 32 840 10 21	2,160 0 3,200	0.044 * 0.000 0.273 0.006 * 0.033	E-W(1): E-W(2): V/C: Lost Time:	0.453 * 0.286 0.560 0.100
	RT TH LT	1.50 0.00 2.00 1.00	95 32 840 10 21 0	2,160 0 3,200 1,600 336 0	0.044 * 0.000 0.273 0.006 * 0.033 0.000	E-W(1): E-W(2): V/C:	0.453 * 0.286 0.560
Northbound	RT TH LT RT TH LT	1.50 0.00 2.00 1.00 0.21 0.00 0.79	95 32 840 10 21 0 79	2,160 0 3,200 1,600 336 0 1,264	0.044 * 0.000 0.273 0.006 * 0.033 0.000 0.063 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.453 * 0.286 0.560 0.100 -0.070
	RT TH LT RT TH	1.50 0.00 2.00 1.00 0.21 0.00 0.79	95 32 840 10 21 0 79	2,160 0 3,200 1,600 336 0 1,264	0.044 * 0.000 0.273 0.006 * 0.033 0.000 0.063 * 0.000	E-W(1): E-W(2): V/C: Lost Time:	0.453 * 0.286 0.560 0.100
Northbound	RT TH LT RT TH LT	1.50 0.00 2.00 1.00 0.21 0.00 0.79	95 32 840 10 21 0 79	2,160 0 3,200 1,600 336 0 1,264	0.044 * 0.000 0.273 0.006 * 0.033 0.000 0.063 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.453 * 0.286 0.560 0.100 -0.070

^{* =} Critical Movement

**INT #18** 

North/South Street: LA CIENEGA BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	49	0	0.000	N-S(1):	0.404
	TH	3.00	1,042	4,800	0.227 *	N-S(2):	0.421 *
	LT	1.00	133	1,600	0.083	E-W(1):	0.281
Westbound	RT	1.00	320	1,600	0.117	E-W(2):	0.447 *
	TH	2.00	1,314	3,200	0.411 *		
	LT	1.00	69	1,600	0.043	V/C:	0.868
Northbound	RT	0.00	29	0	0.000	Lost Time:	0.100
	TH	3.00	1,514	4,800	0.321	ATSAC:	-0.070
	LT	1.00	310	1,600	0.194 *		
Eastbound	RT	1.00	122	1,600	0.000	ICU:	0.898
	TH	2.00	760	3,200	0.238		
	LT	1.00	57	1,600	0.036 *	LOS:	D
Dook Doriods	PM PEAK H	IOUD					
Peak Period: Approach	Movement	Lanes	Π	Capacity	V/C	ICU ANA	I VOIC
Southbound	RT	0.00	17	Оараспу	0.000	N-S(1):	0.388 *
Southbound	TH	3.00	1,284	4,800	0.000	N-S(1).	0.319
	LT	1.00	302	1,600	0.189 *	E-W(1):	0.422 *
Westbound	RT	1.00	142	1,600	0.000	E-W(1).	0.422
VVEStBOUTIO	TH	2.00	556	3,200	0.174	L-VV(Z).	0.212
	LT	1.00	69	1,600	0.043 *	V/C:	0.810
Northbound	RT	0.00	61	0	0.000	Lost Time:	0.100
	TH	3.00	896	4,800	0.199 *	ATSAC:	-0.070
	LT	1.00	77	1,600	0.048	,,	3.0.0
Eastbound	RT	1.00	119	1,600	0.026	ICU:	0.840
	TH	2.00	1,212	3,200	0.379 *	.56.	3.0.0
	LT	1.00	61	1,600	0.038	LOS:	D

^{* =} Critical Movement

**INT #18** 

North/South Street: LA CIENEGA BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	49	0	0.000	N-S(1):	0.404
	TH	3.00	1,042	4,800	0.227 *	N-S(2):	0.421 *
	LT	1.00	133	1,600	0.083	E-W(1):	0.281
Westbound	RT	1.00	320	1,600	0.117	E-W(2):	0.450 *
	TH	2.00	1,326	3,200	0.414 *		
	LT	1.00	69	1,600	0.043	V/C:	0.871
Northbound	RT	0.00	29	0	0.000	Lost Time:	0.100
	TH	3.00	1,514	4,800	0.321	ATSAC:	-0.070
	LT	1.00	310	1,600	0.194 *		
Eastbound	RT	1.00	122	1,600	0.000	ICU:	0.901
	TH	2.00	763	3,200	0.238		
	LT	1.00	58	1,600	0.036 *	LOS:	Ε
Peak Period:	PM PEAK F						
Approach	Movement	Lanes		Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	17	0	0.000	N-S(1):	0.388 *
Approach	Movement RT TH	Lanes 0.00 3.00	1,284	0 4,800	0.000 0.271	N-S(1): N-S(2):	0.388 * 0.319
Approach Southbound	Movement RT TH LT	Lanes 0.00 3.00 1.00	1,284 302	0 4,800 1,600	0.000 0.271 0.189 *	N-S(1): N-S(2): E-W(1):	0.388 * 0.319 0.426 *
Approach	Movement RT TH LT RT	0.00 3.00 1.00	1,284 302 142	0 4,800 1,600 1,600	0.000 0.271 0.189 * 0.000	N-S(1): N-S(2):	0.388 * 0.319
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 3.00 1.00 1.00 2.00	1,284 302 142 561	0 4,800 1,600 1,600 3,200	0.000 0.271 0.189 * 0.000 0.175	N-S(1): N-S(2): E-W(1): E-W(2):	0.388 * 0.319 0.426 * 0.215
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 3.00 1.00 1.00 2.00 1.00	1,284 302 142 561 69	0 4,800 1,600 1,600	0.000 0.271 0.189 * 0.000 0.175 0.043 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.388 * 0.319 0.426 * 0.215
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00	1,284 302 142 561 69 61	0 4,800 1,600 1,600 3,200 1,600	0.000 0.271 0.189 * 0.000 0.175 0.043 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.388 * 0.319 0.426 * 0.215  0.814 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00	1,284 302 142 561 69	0 4,800 1,600 1,600 3,200 1,600 0 4,800	0.000 0.271 0.189 * 0.000 0.175 0.043 * 0.000 0.199 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.388 * 0.319 0.426 * 0.215
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00 1.00	1,284 302 142 561 69 61 896 77	0 4,800 1,600 1,600 3,200 1,600 0 4,800 1,600	0.000 0.271 0.189 * 0.000 0.175 0.043 * 0.000 0.199 * 0.048	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.388 * 0.319 0.426 * 0.215  0.814 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00 1.00 1.00	1,284 302 142 561 69 61 896	0 4,800 1,600 1,600 3,200 1,600 0 4,800 1,600 1,600	0.000 0.271 0.189 * 0.000 0.175 0.043 * 0.000 0.199 * 0.048 0.026	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.388 * 0.319 0.426 * 0.215  0.814 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT TH LT TH LT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00 1.00 1.00 2.00	1,284 302 142 561 69 61 896 77	0 4,800 1,600 1,600 3,200 1,600 0 4,800 1,600 1,600 3,200	0.000 0.271 0.189 * 0.000 0.175 0.043 * 0.000 0.199 * 0.048	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.388 * 0.319 0.426 * 0.215  0.814 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00 1.00 1.00	1,284 302 142 561 69 61 896 77	0 4,800 1,600 1,600 3,200 1,600 0 4,800 1,600 1,600	0.000 0.271 0.189 * 0.000 0.175 0.043 * 0.000 0.199 * 0.048 0.026	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.388 * 0.319 0.426 * 0.215  0.814 0.100 -0.070

^{* =} Critical Movement

**INT #18** 

North/South Street: LA CIENEGA BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	59	0	0.000	N-S(1):	0.426
	TH	3.00	1,142	4,800	0.250 *	N-S(2):	0.448 *
	LT	1.00	136	1,600	0.085	E-W(1):	0.329
Westbound	RT	1.00	326	1,600	0.119	E-W(2):	0.497 *
	TH	2.00	1,467	3,200	0.458 *		
	LT	1.00	108	1,600	0.068	V/C:	0.945
Northbound	RT	0.00	30	0	0.000	Lost Time:	0.100
	TH	3.00	1,605	4,800	0.341	ATSAC:	-0.070
	LT	1.00	316	1,600	0.198 *		
Eastbound	RT	1.00	132	1,600	0.000	ICU:	0.975
	TH	2.00	836	3,200	0.261		
	LT	1.00	62	1,600	0.039 *	LOS:	Ε
Peak Period:	PM PEAK H						
Approach	Movement	Lanes		Capacity	V/C	ICU ANA	
Southbound	RT	0.00	26	0	0.000	N-S(1):	0.413 *
	TH	3.00	1,378	4,800	0.293	N-S(2):	0.342
	l LT l	1.00	308	1,600	0.193 *	E-W(1):	0.510 *
						` '	
Westbound	RT	1.00	145	1,600	0.000	E-W(2):	0.257
Westbound	RT TH	1.00 2.00	145 669	1,600 3,200	0.000 0.209	` '	0.257
	RT TH LT	1.00	145 669 126	1,600 3,200 1,600	0.000	` '	0.923
Westbound  Northbound	RT TH LT RT	1.00 2.00	145 669	1,600 3,200	0.000 0.209 0.079 * 0.000	E-W(2):	
	RT TH LT	1.00 2.00 1.00	145 669 126 62 995	1,600 3,200 1,600	0.000 0.209 0.079 *	E-W(2): V/C:	0.923
	RT TH LT RT	1.00 2.00 1.00 0.00	145 669 126 62	1,600 3,200 1,600 0	0.000 0.209 0.079 * 0.000	E-W(2):  V/C: Lost Time:	0.923 0.100
	RT TH LT RT TH	1.00 2.00 1.00 0.00 3.00	145 669 126 62 995	1,600 3,200 1,600 0 4,800	0.000 0.209 0.079 * 0.000 0.220 *	E-W(2):  V/C: Lost Time:	0.923 0.100
Northbound	RT TH LT RT TH LT	1.00 2.00 1.00 0.00 3.00 1.00	145 669 126 62 995 79	1,600 3,200 1,600 0 4,800 1,600	0.000 0.209 0.079 * 0.000 0.220 * 0.049	E-W(2):  V/C: Lost Time: ATSAC:	0.923 0.100 -0.070

^{* =} Critical Movement

**INT #18** 

North/South Street: LA CIENEGA BOULEVARD East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

	414 DE 417 I	10115					
Peak Period:	AM PEAK H		\/ali vaa	O a a a aite i	\//C	IOLL ANIA	1.7/010
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
Southbound	RT	0.00	59	0	0.000	N-S(1):	0.426
	TH	3.00	1,142	4,800	0.250 *	N-S(2):	0.448 *
	LT	1.00	136	1,600	0.085	E-W(1):	0.330
Westbound	RT	1.00	326	1,600	0.119	E-W(2):	0.501 *
	TH	2.00	1,479	3,200	0.462 *		
	LT	1.00	108	1,600	0.068	V/C:	0.949
Northbound	RT	0.00	30	0	0.000	Lost Time:	0.100
	TH	3.00	1,605	4,800	0.341	ATSAC:	-0.070
	LT	1.00	316	1,600	0.198 *		
Eastbound	RT	1.00	132	1,600	0.000	ICU:	0.979
	TH	2.00	839	3,200	0.262		
	LT	1.00	63	1,600	0.039 *	LOS:	E
Peak Period:	PM PEAK H	IOUR					
Peak Period: Approach	PM PEAK H	IOUR Lanes		Capacity	V/C	ICU ANA	LYSIS
			26	Capacity 0	V/C 0.000	ICU ANA N-S(1):	LYSIS 0.413 *
Approach	Movement	Lanes	26 1,378				
Approach	Movement RT	Lanes 0.00	_	0	0.000	N-S(1):	0.413 *
Approach	Movement RT TH	Lanes 0.00 3.00	1,378	0 4,800	0.000 0.293	N-S(1): N-S(2):	0.413 * 0.342
Approach Southbound	Movement RT TH LT	Lanes 0.00 3.00 1.00	1,378 308	0 4,800 1,600	0.000 0.293 0.193 *	N-S(1): N-S(2): E-W(1):	0.413 * 0.342 0.514 *
Approach Southbound	Movement RT TH LT RT	Lanes 0.00 3.00 1.00	1,378 308 145	0 4,800 1,600 1,600	0.000 0.293 0.193 * 0.000	N-S(1): N-S(2): E-W(1):	0.413 * 0.342 0.514 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 3.00 1.00 1.00 2.00	1,378 308 145 674	0 4,800 1,600 1,600 3,200	0.000 0.293 0.193 * 0.000 0.211	N-S(1): N-S(2): E-W(1): E-W(2):	0.413 * 0.342 0.514 * 0.260
Approach Southbound Westbound	Movement RT TH LT RT RT TH LT TH	Lanes 0.00 3.00 1.00 1.00 2.00 1.00	1,378 308 145 674 126	0 4,800 1,600 1,600 3,200 1,600	0.000 0.293 0.193 * 0.000 0.211 0.079 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.413 * 0.342 0.514 * 0.260
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00	1,378 308 145 674 126 62	0 4,800 1,600 1,600 3,200 1,600	0.000 0.293 0.193 * 0.000 0.211 0.079 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.413 * 0.342 0.514 * 0.260 0.927 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00	1,378 308 145 674 126 62 995	0 4,800 1,600 1,600 3,200 1,600 0 4,800	0.000 0.293 0.193 * 0.000 0.211 0.079 * 0.000 0.220 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.413 * 0.342 0.514 * 0.260 0.927 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT TH LT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00 1.00	1,378 308 145 674 126 62 995 79	0 4,800 1,600 1,600 3,200 1,600 0 4,800 1,600 1,600	0.000 0.293 0.193 * 0.000 0.211 0.079 * 0.000 0.220 * 0.049	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.413 * 0.342 0.514 * 0.260  0.927 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 3.00 1.00 1.00 2.00 1.00 0.00 3.00 1.00 1.00	1,378 308 145 674 126 62 995 79	0 4,800 1,600 1,600 3,200 1,600 0 4,800 1,600	0.000 0.293 0.193 * 0.000 0.211 0.079 * 0.000 0.220 * 0.049 0.036	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.413 * 0.342 0.514 * 0.260  0.927 0.100 -0.070

^{* =} Critical Movement

**INT #19** 

North/South Street: WESLEY STREET

East/West Street: NATIONAL BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.101
	TH	0.00	0	0	0.000 *	N-S(2):	0.139 *
	LT	0.00	0	0	0.000	E-W(1):	0.242
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.260 *
	TH	2.00	833	3,200	0.260 *		
	LT	1.00	22	1,600	0.014	V/C:	0.399
Northbound	RT	0.35	79	567	0.101	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.65	144	1,033	0.139 *		
Eastbound	RT	1.00	239	1,600	0.059	ICU:	0.429
	TH	2.00	729	3,200	0.228		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H						
Approach	Movement		_	Capacity	V/C	ICU ANA	
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.027
	TH	0.00	0				
				0	0.000 *	N-S(2):	0.061 *
	LT	0.00	0	0	0.000	E-W(1):	0.372 *
Westbound	RT	0.00	0	0	0.000 0.000		
Westbound	RT TH	0.00 2.00	0 0 930	0 0 3,200	0.000 0.000 0.291	E-W(1): E-W(2):	0.372 * 0.291
	RT TH LT	0.00 2.00 1.00	0 0 930 14	0 0 3,200 1,600	0.000 0.000 0.291 0.009 *	E-W(1): E-W(2): V/C:	0.372 * 0.291 0.433
Westbound  Northbound	RT TH LT RT	0.00 2.00 1.00 0.26	0 0 930	0 0 3,200	0.000 0.000 0.291 0.009 * 0.027	E-W(1): E-W(2): V/C: Lost Time:	0.372 * 0.291 0.433 0.100
	RT TH LT RT TH	0.00 2.00 1.00	0 0 930 14 25 0	0 0 3,200 1,600 408 0	0.000 0.000 0.291 0.009 * 0.027 0.000	E-W(1): E-W(2): V/C:	0.372 * 0.291 0.433
Northbound	RT TH LT RT TH LT	0.00 2.00 1.00 0.26 0.00 0.74	0 930 14 25 0 73	0 0 3,200 1,600 408 0 1,192	0.000 0.000 0.291 0.009 * 0.027 0.000 0.061 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.372 * 0.291
	RT TH LT RT TH LT	0.00 2.00 1.00 0.26 0.00	0 930 14 25 0 73	0 0 3,200 1,600 408 0 1,192 1,600	0.000 0.000 0.291 0.009 * 0.027 0.000 0.061 * 0.013	E-W(1): E-W(2): V/C: Lost Time:	0.372 * 0.291 0.433 0.100
Northbound	RT TH LT RT TH LT	0.00 2.00 1.00 0.26 0.00 0.74	0 930 14 25 0 73	0 0 3,200 1,600 408 0 1,192	0.000 0.000 0.291 0.009 * 0.027 0.000 0.061 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.372 * 0.291

^{* =} Critical Movement

**INT #19** 

North/South Street: WESLEY STREET

East/West Street: NATIONAL BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.101
	TH	0.00	0	0	0.000 *	N-S(2):	0.139 *
	LT	0.00	0	0	0.000	E-W(1):	0.243
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.265 *
	TH	2.00	849	3,200	0.265 *		
	LT	1.00	22	1,600	0.014	V/C:	0.404
Northbound	RT	0.35	79	567	0.101	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.65	144	1,033	0.139 *		
Eastbound	RT	1.00	239	1,600	0.059	ICU:	0.434
	TH	2.00	733	3,200	0.229		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H						
Approach	Movement	Lanes		Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	0	0.000	N-S(1):	0.027
Approach	Movement RT TH	0.00 0.00	0	0	0.000 0.000 *	N-S(1): N-S(2):	0.027 0.061 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.027 0.061 * 0.377 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.027 0.061 *
Approach Southbound	Movement RT TH LT RT TH	0.00 0.00 0.00 0.00 0.00 2.00	0 0 0 937	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.293	N-S(1): N-S(2): E-W(1): E-W(2):	0.027 0.061 * 0.377 * 0.293
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 937 14	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.293 0.009 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.027 0.061 * 0.377 * 0.293
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26	0 0 0 937	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.293 0.009 * 0.027	N-S(1): N-S(2): E-W(1): E-W(2):	0.027 0.061 * 0.377 * 0.293
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 937 14	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.293 0.009 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.027 0.061 * 0.377 * 0.293
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26	0 0 937 14 25 0 73	0 0 0 0 3,200 1,600 408 0 1,192	0.000 0.000 * 0.000 0.000 0.293 0.009 * 0.027	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.027 0.061 * 0.377 * 0.293 0.438 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26 0.00	0 0 0 937 14 25 0	0 0 0 0 3,200 1,600 408 0	0.000 0.000 * 0.000 0.000 0.293 0.009 * 0.027 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.027 0.061 * 0.377 * 0.293 0.438 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26 0.00 0.74	0 0 937 14 25 0 73	0 0 0 0 3,200 1,600 408 0 1,192	0.000 0.000 * 0.000 0.000 0.293 0.009 * 0.027 0.000 0.061 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.027 0.061 * 0.377 * 0.293 0.438 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26 0.00 0.74 1.00	0 0 937 14 25 0 73	0 0 0 0 3,200 1,600 408 0 1,192 1,600	0.000 0.000 * 0.000 0.000 0.293 0.009 * 0.027 0.000 0.061 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.027 0.061 * 0.377 * 0.293 0.438 0.100 -0.070

^{* =} Critical Movement

**INT # 19** 

North/South Street: WESLEY STREET

East/West Street: NATIONAL BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.104
	TH	0.00	0	0	0.000 *	N-S(2):	0.143 *
	LT	0.00	0	0	0.000	E-W(1):	0.317
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.347 *
	TH	2.00	1,109	3,200	0.347 *		
	LT	1.00	22	1,600	0.014	V/C:	0.490
Northbound	RT	0.36	81	568	0.104	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.64	147	1,032	0.143 *		
Eastbound	RT	1.00	245	1,600	0.061	ICU:	0.520
	TH	2.00	970	3,200	0.303		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK F		ľ				
Approach	Movement	Lanes	_	Capacity	V/C	ICU ANA	
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.029
	TH	0.00	0	0	0.000 *	N-S(2):	0.063 *
	LT	0.00	0	0	0.000	E-W(1):	0.465 *
Westbound	LT RT	0.00	0	0	0.000 0.000		
Westbound	LT RT TH	0.00 0.00 2.00	0 0 1,236	0 0 3,200	0.000 0.000 0.386	E-W(1): E-W(2):	0.465 * 0.386
	LT RT TH LT	0.00 0.00 2.00 1.00	0 0 1,236 14	0 0 3,200 1,600	0.000 0.000 0.386 0.009 *	E-W(1): E-W(2): V/C:	0.465 * 0.386 0.528
Westbound  Northbound	LT RT TH LT RT	0.00 0.00 2.00 1.00 0.26	0 0 1,236	0 0 3,200	0.000 0.000 0.386 0.009 *	E-W(1): E-W(2):	0.465 * 0.386
	LT RT TH LT	0.00 0.00 2.00 1.00	0 0 1,236 14	0 0 3,200 1,600	0.000 0.000 0.386 0.009 *	E-W(1): E-W(2): V/C:	0.465 * 0.386 0.528
	LT RT TH LT RT	0.00 0.00 2.00 1.00 0.26	0 0 1,236 14 26 0 75	0 0 3,200 1,600 412 0 1,188	0.000 0.000 0.386 0.009 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.465 * 0.386
	LT RT TH LT RT TH	0.00 0.00 2.00 1.00 0.26 0.00	0 0 1,236 14 26 0	0 0 3,200 1,600 412 0	0.000 0.000 0.386 0.009 * 0.029 0.000	E-W(1): E-W(2): V/C: Lost Time:	0.465 * 0.386 0.528 0.100
Northbound	LT RT TH LT RT TH LT	0.00 0.00 2.00 1.00 0.26 0.00 0.74	0 0 1,236 14 26 0 75	0 0 3,200 1,600 412 0 1,188	0.000 0.000 0.386 0.009 * 0.029 0.000 0.063 *	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.465 * 0.386
Northbound	LT RT TH LT RT TH LT	0.00 0.00 2.00 1.00 0.26 0.00 0.74	0 0 1,236 14 26 0 75	0 0 3,200 1,600 412 0 1,188 1,600	0.000 0.000 0.386 0.009 * 0.029 0.000 0.063 * 0.013	E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.465 * 0.386

^{* =} Critical Movement

**INT #19** 

North/South Street: WESLEY STREET

East/West Street: NATIONAL BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.104
	TH	0.00	0	0	0.000 *	N-S(2):	0.143 *
	LT	0.00	0	0	0.000	E-W(1):	0.318
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.352 *
	TH	2.00	1,125	3,200	0.352 *		
	LT	1.00	22	1,600	0.014	V/C:	0.495
Northbound	RT	0.36	81	568	0.104	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.64	147	1,032	0.143 *		
Eastbound	RT	1.00	245	1,600	0.061	ICU:	0.525
	TH	2.00	974	3,200	0.304		
	LT	0.00	0	0	0.000 *	LOS:	Α
Peak Period:	PM PEAK H	IOUR					
Peak Period: Approach	PM PEAK H	IOUR Lanes		Capacity	V/C	ICU ANA	LYSIS
			0	Capacity 0	V/C 0.000	ICU ANA N-S(1):	LYSIS 0.029
Approach	Movement	Lanes	0				
Approach	Movement RT	Lanes 0.00		0	0.000	N-S(1):	0.029
Approach	Movement RT TH	0.00 0.00	0	0 0	0.000 0.000 *	N-S(1): N-S(2):	0.029 0.063 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.029 0.063 * 0.471 *
Approach Southbound	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2): E-W(1):	0.029 0.063 * 0.471 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 1,243	0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.388	N-S(1): N-S(2): E-W(1): E-W(2):	0.029 0.063 * 0.471 * 0.388
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 1,243 14	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.388 0.009 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.029 0.063 * 0.471 * 0.388
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT RT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26	0 0 0 1,243 14 26	0 0 0 0 3,200 1,600 412	0.000 0.000 * 0.000 0.000 0.388 0.009 * 0.029	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.029 0.063 * 0.471 * 0.388 0.534 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26 0.00	0 0 0 1,243 14 26 0	0 0 0 0 3,200 1,600 412 0	0.000 0.000 * 0.000 0.000 0.388 0.009 * 0.029 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.029 0.063 * 0.471 * 0.388 0.534 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26 0.00 0.74	0 0 1,243 14 26 0 75	0 0 0 0 3,200 1,600 412 0 1,188	0.000 0.000 * 0.000 0.000 0.388 0.009 * 0.029 0.000 0.063 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.029 0.063 * 0.471 * 0.388 0.534 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.26 0.00 0.74 1.00	0 0 1,243 14 26 0 75	0 0 0 0 3,200 1,600 412 0 1,188 1,600	0.000 0.000 * 0.000 0.000 0.388 0.009 * 0.029 0.000 0.063 * 0.013	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.029 0.063 * 0.471 * 0.388 0.534 0.100 -0.070

^{* =} Critical Movement

**INT # 20** 

North/South Street: HAYDEN AVENUE

East/West Street: NATIONAL BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.115 *
	LT	0.00	0	0	0.000	E-W(1):	0.316 *
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.189
	TH	2.00	602	3,200	0.188		
	LT	1.00	185	1,600	0.116 *	V/C:	0.431
Northbound	RT	0.26	43	416	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.74	288	2,506	0.115 *		
Eastbound	RT	1.00	254	1,600	0.055	ICU:	0.461
	TH	2.00	640	3,200	0.200 *		
	LT	0.00	1	1,600	0.001	LOS:	Α
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	Volume 0	Capacity 0	0.000	N-S(1):	0.137
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.137 0.178 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.137 0.178 * 0.260 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.137 0.178 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 438	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.137	N-S(1): N-S(2): E-W(1):	0.137 0.178 * 0.260 * 0.137
Approach Southbound	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2): E-W(1):	0.137 0.178 * 0.260 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 438	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.137	N-S(1): N-S(2): E-W(1): E-W(2):	0.137 0.178 * 0.260 * 0.137
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 438 17	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.137 0.011 * 0.137 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.137 0.178 * 0.260 * 0.137
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46	0 0 0 0 438 17 119 0 393	0 0 0 0 3,200 1,600 744	0.000 0.000 * 0.000 0.000 0.137 0.011 * 0.137 0.000 0.178 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.137 0.178 * 0.260 * 0.137 0.438 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46 0.00	0 0 0 0 438 17 119 0	0 0 0 0 3,200 1,600 744 0	0.000 0.000 * 0.000 0.000 0.137 0.011 * 0.137 0.000 0.178 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.137 0.178 * 0.260 * 0.137 0.438 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46 0.00 1.54	0 0 0 0 438 17 119 0 393	0 0 0 0 3,200 1,600 744 0 2,211	0.000 0.000 * 0.000 0.000 0.137 0.011 * 0.137 0.000 0.178 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.137 0.178 * 0.260 * 0.137 0.438 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46 0.00 1.54 1.00	0 0 0 0 438 17 119 0 393 338	0 0 0 3,200 1,600 744 0 2,211 1,600	0.000 0.000 * 0.000 0.000 0.137 0.011 * 0.137 0.000 0.178 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.137 0.178 * 0.260 * 0.137 0.438 0.100 -0.070

^{* =} Critical Movement

**INT # 20** 

North/South Street: HAYDEN AVENUE

East/West Street: NATIONAL BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.116 *
	LT	0.00	0	0	0.000	E-W(1):	0.318 *
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.193
	TH	2.00	614	3,200	0.192		
	LT	1.00	185	1,600	0.116 *	V/C:	0.434
Northbound	RT	0.26	43	411	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.74	292	2,510	0.116 *		
Eastbound	RT	1.00	254	1,600	0.054	ICU:	0.464
	TH	2.00	644	3,200	0.202 *		
	LT	0.00	1	1,600	0.001	LOS:	Α
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	Capacity 0	0.000	N-S(1):	0.138
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.138 0.178 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.138 0.178 * 0.265 *
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.138 0.178 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 443	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.138	N-S(1): N-S(2): E-W(1):	0.138 0.178 * 0.265 * 0.138
Approach Southbound	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2): E-W(1):	0.138 0.178 * 0.265 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 443	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.138	N-S(1): N-S(2): E-W(1): E-W(2):	0.138 0.178 * 0.265 * 0.138
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 443 17	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.138 0.011 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.138 0.178 * 0.265 * 0.138
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46	0 0 0 0 443 17 119	0 0 0 0 3,200 1,600 741	0.000 0.000 * 0.000 0.000 0.138 0.011 * 0.138	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.138 0.178 * 0.265 * 0.138 0.443 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46 0.00	0 0 0 0 443 17 119 0	0 0 0 0 3,200 1,600 741 0	0.000 0.000 * 0.000 0.000 0.138 0.011 * 0.138 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.138 0.178 * 0.265 * 0.138 0.443 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46 0.00 1.54	0 0 0 0 443 17 119 0 395	0 0 0 0 3,200 1,600 741 0 2,213	0.000 0.000 * 0.000 0.000 0.138 0.011 * 0.138 0.000 0.178 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.138 0.178 * 0.265 * 0.138 0.443 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.46 0.00 1.54 1.00	0 0 0 0 443 17 119 0 395 338	0 0 0 3,200 1,600 741 0 2,213 1,600	0.000 0.000 * 0.000 0.000 0.138 0.011 * 0.138 0.000 0.178 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.138 0.178 * 0.265 * 0.138 0.443 0.100 -0.070

^{* =} Critical Movement

**INT # 20** 

North/South Street: HAYDEN AVENUE

East/West Street: NATIONAL BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.147 *
	LT	0.00	0	0	0.000	E-W(1):	0.399 *
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.257
	TH	2.00	818	3,200	0.256		
	LT	1.00	210	1,600	0.131 *	V/C:	0.546
Northbound	RT	0.34	72	546	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.66	350	2,389	0.147 *		
Eastbound	RT	1.00	282	1,600	0.044	ICU:	0.576
	TH	2.00	857	3,200	0.268 *		
	LT	0.00	1	1,600	0.001	LOS:	Α
Peak Period:	PM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	Volume 0	Capacity 0	0.000	N-S(1):	0.147
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.147 0.211 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.147 0.211 * 0.355 *
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.147 0.211 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 0 677	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.212	N-S(1): N-S(2): E-W(1):	0.147 0.211 * 0.355 * 0.212
Approach Southbound	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2): E-W(1):	0.147 0.211 * 0.355 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 0 677	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.212	N-S(1): N-S(2): E-W(1): E-W(2):	0.147 0.211 * 0.355 * 0.212
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 677 34	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.212 0.021 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.147 0.211 * 0.355 * 0.212
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.50	0 0 0 0 677 34 151	0 0 0 0 3,200 1,600 793	0.000 0.000 * 0.000 0.000 0.212 0.021 * 0.147	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.147 0.211 * 0.355 * 0.212 0.566 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.50 0.00	0 0 0 0 677 34 151	0 0 0 0 3,200 1,600 793 0	0.000 0.000 * 0.000 0.000 0.212 0.021 * 0.147 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.147 0.211 * 0.355 * 0.212 0.566 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.50 0.00 1.50	0 0 0 0 677 34 151 0 458	0 0 0 0 3,200 1,600 793 0 2,166	0.000 0.000 * 0.000 0.000 0.212 0.021 * 0.147 0.000 0.211 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.147 0.211 * 0.355 * 0.212 0.566 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.50 0.00 1.50 1.00	0 0 0 0 677 34 151 0 458 363	0 0 0 3,200 1,600 793 0 2,166 1,600	0.000 0.000 * 0.000 0.000 0.212 0.021 * 0.147 0.000 0.211 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.147 0.211 * 0.355 * 0.212 0.566 0.100 -0.070

^{* =} Critical Movement

**INT # 20** 

North/South Street: HAYDEN AVENUE

East/West Street: NATIONAL BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	N
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.148 *
	LT	0.00	0	0	0.000	E-W(1):	0.400 *
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.260
	TH	2.00	830	3,200	0.259		
	LT	1.00	210	1,600	0.131 *	V/C:	0.548
Northbound	RT	0.34	72	541	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	1.66	354	2,393	0.148 *		
Eastbound	RT	1.00	282	1,600	0.043	ICU:	0.578
	TH	2.00	861	3,200	0.269 *		
	LT	0.00	1	1,600	0.001	LOS:	Α
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	0	0	0.000	N-S(1):	0.148
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.148 0.212 *
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.148 0.212 * 0.361 *
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.148 0.212 *
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 682	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.213	N-S(1): N-S(2): E-W(1): E-W(2):	0.148 0.212 * 0.361 * 0.213
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 682 34	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.213 0.021 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.148 0.212 * 0.361 * 0.213
Approach Southbound	Movement RT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00	0 0 0 0 682	0 0 0 0 0 3,200	0.000 0.000 * 0.000 0.000 0.213	N-S(1): N-S(2): E-W(1): E-W(2):	0.148 0.212 * 0.361 * 0.213
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 682 34	0 0 0 0 3,200 1,600	0.000 0.000 * 0.000 0.000 0.213 0.021 * 0.148 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.148 0.212 * 0.361 * 0.213
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.49 0.00 1.51	0 0 0 0 682 34 151 0 460	0 0 0 0 3,200 1,600 791	0.000 0.000 * 0.000 0.000 0.213 0.021 * 0.148 0.000 0.212 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.148 0.212 * 0.361 * 0.213 0.573 0.100 -0.070
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.49 0.00	0 0 0 0 682 34 151	0 0 0 0 3,200 1,600 791 0	0.000 0.000 * 0.000 0.000 0.213 0.021 * 0.148 0.000 0.212 * 0.036	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.148 0.212 * 0.361 * 0.213 0.573 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.49 0.00 1.51	0 0 0 0 682 34 151 0 460	0 0 0 0 3,200 1,600 791 0 2,168	0.000 0.000 * 0.000 0.000 0.213 0.021 * 0.148 0.000 0.212 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.148 0.212 * 0.361 * 0.213 0.573 0.100 -0.070
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.49 0.00 1.51 1.00	0 0 0 0 682 34 151 0 460	0 0 0 0 3,200 1,600 791 0 2,168 1,600	0.000 0.000 * 0.000 0.000 0.213 0.021 * 0.148 0.000 0.212 * 0.036	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.148 0.212 * 0.361 * 0.213 0.573 0.100 -0.070

^{* =} Critical Movement



(Circular 212 Method)



I/S #:	North-South Street:	Jefferso	n Boulevard Boulevard		Year of Count: 2016		2016	Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:	te: 1/24/2017		,	
21	East-West Street:	National	Boulevard			Proje	ction Year	2018		Pea	ak Hour:	AM	Revie	wed by:	F	RA	Project:		RA491	
	posed Ø'ing: N/S-1, E/W-2 o Turns: FREE-1, NRTOR-2 o ATSAC-1 or ATSAC+	r OLA-3?	NB 0 EB 3	SB WB	4 2 3 2 2 0	NB EB	0 SI		NB EB	0	SB WB	4 2 3 2 2	NB EB	0 3	SB WB	4 2 3 2 2	NB EB	0 3	SB WB	4 2 3 2 2 0
	Override	Сараспу	EXISTI	NG CONDI		EXIST	ING PLUS P		FUTUR	E CONDITI	ON W/O PR		FUTUI	RE CONDIT	ION W/ PR	•	FUTURE	W/ PROJE	CT W/ MIT	
	MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
NORTHBOUND	Left Left-Through Through-Right Right Left-Through-Right Left-Right		326 712 24	1 0 2 0 1 0	326 356 23	0 0	326 712 24	326 356 23	31 42 76	364 768 100	1 0 2 0 1 0	364 384 94	0 0	364 768 100	1 0 2 0 1 0	<b>364</b> 384 94	0 0	364 768 100	1 0 2 0 1 0	364 384 94
SOUTHBOUND	Left  Left-Through  Through-Right  Right  Left-Through-Right  Left-Right		18 856 674	1 0 1 0 1 0	18 <b>856</b> 528	0 0 12	18 856 686	18 <b>856</b> 538	75 74 173	93 947 861	1 0 1 0 1 0	93 <b>947</b> 619	0 0 12	93 947 873	1 0 1 0 1 0	93 <b>947</b> 630	0 0 0	93 947 873	1 0 1 0 1 0	93 <b>947</b> 630
EASTBOUND	→ Left     → Left-Through     → Through     ↑ Through-Right     Right     ← Left-Through-Right     ← Left-Right		269 23 284	1 1 0 0 1 0	146 146 0	3 0 1	272 23 285	148 148 0	110 76 14	384 99 304	1 1 0 0 1 0	<b>242</b> 242 0	3 0 1	387 99 305	1 1 0 0 1 0	243 243 0	0 0	387 99 305	1 1 0 0 1 0	243 243 0
WESTBOUND	Left Left-Through Through-Right Right Left-Through-Right Left-Through-Right Left-Right		2 10 8	0 1 0 0 1 0	2 12 8	0 0 0	2 10 8	2 <b>12</b> 8	10 20 10	12 30 18	0 1 0 0 1 0	12 <b>42</b> 18	0 0	12 30 18	0 1 0 0 1 0	12 <b>42</b> 18	0 0 0	12 30 18	0 1 0 0 1 0	12 <b>42</b> 18
	CRITICAL V			th-South: ast-West: SUM:	1182 158 1340		rth-South: East-West: SUM:	1182 160 1342			th-South: ast-West: SUM:	1311 284 1595			th-South: ast-West: SUM:				th-South: ast-West: SUM:	1311 285 1596
V/0	VOLUME/CAPACITY (V/C C LESS ATSAC/ATCS ADJU: LEVEL OF SERVIC	STMENT:			0.975 0.875 D			0.976 <b>0.876</b> <b>D</b>				1.160 1.060 F				1.161 1.061 F				1.161 1.061 F

REMARKS:

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.001  $\Delta v/c$  after mitigation: 0.001 Significant impacted? NO Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Jefferso	n Boulevard	I		Year of Count: 2016			6 Ambient Growth: (%):		1	Conducted by:		y: RA		Date: 1/24/2017		7		
21	East-West Street:	National	Boulevard				ction Year				ak Hour:	PM		wed by:		RA	Project:		RA491	
		f Phases			4			4				3				3	,			3
Opp	oosed Ø'ing: N/S-1, E/W-2 or	Both-3?	ND O	66	2	N/C	0 0	2	ME	0	66	2	NE	0	66	2	ME	0	66	2
Right	Turns: FREE-1, NRTOR-2 or	OLA-3?	NB 0 EB 3	SB WB	2	NB EB	0 SE 3 W		NB EB	0 3	SB WB	3 2	NB EB	0	SB WB	3 2	NB EB	0	SB WB	3 2
	ATSAC-1 or ATSAC+	ATCS-2?		2	2			2			2	2				2			2	2
	Override	Capacity			0			0				0				0				0
	MOVEMENT		EXISTI	NG CONDI			ING PLUS P				ON W/O PR			RE CONDIT				W/ PROJE		
	INIO V EIVIEN I		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
	↑ Left		177	1	177	0	177	177	21	202	1	202	0	202	1	202	0	202	1	202
NORTHBOUND	Left-Through			0							0				0		-		0	
∥ જૂ	Through		994	2	497	0	994	497	68	1082	2	541	0	1082	2	541	0	1082	2	541
∥ ≝ I	Through-Right		6	0 1	3	0	6	3	14	20	0 1	0	0	20	0	0	0	20	0 1	0
OR R	<ul><li></li></ul>		U	0	3		U	3	14	20	0	U		20	0	U		20	0	U
2	Left-Right			0							0				0				0	
_	1				- -				4.5			4-		4-				1-		
9	<ul><li>↓ Left</li><li>↓ Left-Through</li></ul>		4	1 0	4	0	4	4	13	17	1 0	17	0	17	1	17	0	17	1 0	17
l lo	Through		402	1	402	0	402	402	63	473	1	473	0	473	1	473	0	473	1	473
Ě	← Through-Right			0							0				0				0	
SOUTHBOUND			201	1 0	0	5	206	0	159	364	1 0	7	5	369	1	5	0	369	1 0	5
S	↓ Left-Right			0							0				0				0	
					=															
			481	1 1	245	14	495	252	193	684	1 1	357	14	698	1	364	0	698	1	364
3	→ Leπ-Inrougn → Through		8	0	245	0	8	252	21	29	0	357	0	29	0	364	0	29	0	364
EASTBOUND	→ Through-Right			0							0	30.			Ö				0	
AST	Right		363	1	186	5	368	191	48	418	1	216	5	423	1	221	0	423	1	221
щ	★ Left-Through-Right     ★ Left-Right			0 0							0 0				0				0	
	t con regine																			
	✓ Left		6	0	6	0	6	6	66	72	0	72	0	72	0	72	0	72	0	72
WESTBOUND			14	1 0	20	0	14	20	69	83	1 0	155	0	83	1 0	155	0	83	1 0	155
98	Through-Right		17	0	20		דו	20	03	00	0	100		00	0	133		00	0	133
EST	Right		17	1	17	0	17	17	66	83	1	83	0	83	1	83	0	83	1	83
×	Left-Through-Right Left-Right			0 0							0 0				0				0	
	↓ Len-Night		Nor	th-South:	579	No	rth-South:	579		Nor	th-South:	675		Nor	th-South:	675		Nor	th-South:	675
	CRITICAL VO	OLUMES		ast-West:	265	1	East-West:	272		E	ast-West:	512		E	ast-West:	519			ast-West:	519
<u> </u>	VOLUME (OADAOITY (1/2)	) DATIC		SUM:		-	SUM:	851			SUM:	1187			SUM:				SUM:	1194
	VOLUME/CAPACITY (V/C)	•			0.614			0.619				0.833				0.838				0.838
V/C	LESS ATSAC/ATCS ADJUS				0.514			0.519				0.733				0.738				0.738
	LEVEL OF SERVIC	E (LOS): MARKS:			Α			Α				С				С				С

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in *v/c* due to project: 0.005
Significant impacted? NO

 $\Delta v/c$  after mitigation: 0.005 Fully mitigated? N/A

int21_Calcadb.xls



(Circular 212 Method)



I/S #:	North-South Street:	Jefferso	n Boulevard	<u> </u>		Year of Count: 2016 Projection Year: 2018			Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
22	East-West Street:	Higuera	Street-Rode	o Road						Pea	ak Hour:	AM		wed by:		RA	Project:		RA491	
	No. o posed Ø'ing: N/S-1, E/W-2 o	of Phases r Both-3?			3 0	-		3				3				3				3
Right	Turns: FREE-1, NRTOR-2 o	r OLA-3?	0 3 EB 0	SB WB	0	NB EB	3 SE 0 W		NB EB	3	SB WB	0	NB EB	3	SB WB	0	NB EB	3	SB WB	0
	ATSAC-1 or ATSAC+ Override	ATCS-2? Capacity		,, ₀	2 0		J 777	2			.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2			,,,,,	2		U		2
			EXISTI	NG CONDI	TION	EXIST	ING PLUS PI	ROJECT	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTUI	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
	MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
₽	↑ Left  Left-Through		120	1 0	120	0	120	120	10	132	1 0	132	0	132	1 0	132	0	132	1 0	132
NORTHBOUND	↑ Through ↑ Through-Right		745	0 2 0	373	0	745	373	86	846	2 0	423	0	846	2 0	423	0	846	2 0	423
ORTH	<ul><li></li></ul>		463	0 0	0	0	463	0	18	490	0 0	0	0	490	0	0	0	490	0	0
Z	Left-Right		<b>I</b>	0							0				0				0	
Q			138	1 0	138	1	139	139	20	161	1 0	161	1	162	1 0	162	0	162	1 0	162
-IBOU	↓ Through ←↓ Through-Right		834	2 0	417	0	834	417	66	917	2 0	459	0	917	2	459	0	917	2	459
SOUTHBOUND	Right Left-Through-Right Left-Right		54	1 0 0	37	0	54	37	14	69	1 0 0	51	0	69	1 0 0	51	0	69	1 0 0	51
	Left		35	1	35	0	35	35	0	36	1	36	0	36	1	36	0	36	1	36
QND	→ Left-Through → Through		146	0 2	73	0	146	73	11	160	0 2	80	0	160	0	80		160	0 2	80
EASTBOUND	→ Through-Right → Right		55	0	,3	0	55	0	7	63	0	0	0	63	0	0		63	0	0
EAS	Left-Through-Right		00	0	J		55	· ·	,	UU.	0	Ū		00	0	J		00	0	J
QN.	✓ Left ✓ Left-Through		896	0	493	0	896	493	42	956	2 0	526	0	956	0	526	0	956	0	526
WESTBOUND	← Through ← Through-Right ← Bight		649	1 0 1	649	0	653 366	<b>653</b> 297	27 72	689 445	1 0 1	689	0	693 445	0	<b>693</b> 364	0	693 445	1 0 1	<b>693</b> 364
WES	Right  Left-Through-Right  Left-Right		366	0	297	0	300	297	12	445	0 0	365	"	445	0	304		445	0	304
	CRITICAL V	OLUMES	_	th-South: ast-West: SUM:	537 684 1221		rth-South: East-West: SUM:	537 688 1225			th-South: ast-West: SUM:	591 725 1316			th-South: ast-West: SUM:	729			th-South: ast-West: SUM:	591 729 1320
	VOLUME/CAPACITY (V/C	) RATIO:			0.857			0.860				0.924				0.926				0.926
V/C	C LESS ATSAC/ATCS ADJU	STMENT:			0.757			0.760				0.824				0.826				0.826
	LEVEL OF SERVICE	CE (LOS):			С			С				D				D				D
	DE	MARKS:																		

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.002  $\Delta v/c$  after Significant impacted? NO Full

 $\Delta v/c$  after mitigation: 0.002 Fully mitigated? N/A



(Circular 212 Method)



I/S #:	North-South Street:	Jefferso	n Boulevard	I		Year of Count: 2016 Projection Year: 2018			Amb	ient Grov	vth: (%):	1	Condu	cted by:	F	RA	Date:		1/24/2017	7
22	East-West Street:	Higuera	Street-Rode	eo Road						Pe	ak Hour:	PM		wed by:		RA	Project:		RA491	
Ор	posed Ø'ing: N/S-1, E/W-2 or		NB 3	SB	3 0 0	NB	3 SE	3 0 3 0	NB	3	SB	3 0 0	NB	3	SB	3 0 0	NB	3	SB	3 0 0
Right	Turns: FREE-1, NRTOR-2 or	r OLA-3?	EB 0	WB	0	EB	0 W		EB	0	WB	0	EB	0	WB	0	EB	0	WB	0
	ATSAC-1 or ATSAC+ Override				2 0			2				2 0				2				2 0
			EXISTI	NG CONDI			ING PLUS PI				ON W/O PR			RE CONDIT				W/ PROJE		
	MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
₽	↑ Left  Left-Through		34	1 0	34	0	34	34	8	43	1 0	43	0	43	1 0	43	0	43	1 0	43
NORTHBOUND	↑ Through ↑ Through-Right		949	0 2 0	475	0	949	475	73	1041	2 0	521	0	1041	2	521	0	1041	2	521
RT	Right		804	0	0	0	804	0	44	864	0	0	0	864	0	0	0	864	0	0
ON.	Left-Through-Right Left-Right			0 0							0 0				0				0	
	↓ Left		164	1	164	5	169	169	84	251	1	251	5	256	1	256	0	256	1	256
SOUTHBOUND	Left-Through Through		583	0 2	292	0	583	292	91	686	0 2	343	0	686	0 2	343	0	686	0 2	343
里	Through-Right		40	0 1	00	0	40	00	44	50	0 1	4.4	0	50	0	4.4		50	0 1	44
Sour	<ul><li>✓ Right</li><li>→ Left-Through-Right</li><li>✓ Left-Right</li></ul>		46	0 0	32	U	46	32	11	58	0 0	44	0	58	0	44	0	58	0	44
	ے Left		28	1	28	0	28	28	0	29	1	29	0	29	1	29	0	29	1	29
9	→ Left-Through		20	0	20	0	20	20	0	29	0	29	U	29	0	29	"	29	0	29
EASTBOUND	→ Through  → Through-Right		629	2 0	315	0	629	315	13	655	2 0	328	0	655	2	328	0	655	2 0	328
EAST	Right Left-Through-Right		128	1 0	111	0	128	111	7	138	1 0	117	0	138	1	117	0	138	1 0 0	117
	-		l	0							0				0				U	
Q	<ul><li>✓ Left</li><li>✓ Left-Through</li></ul>		407	2 0	224	0	407	224	23	438	2 0	241	0	438	2	241	0	438	2	241
WESTBOUND	← Through ← Through-Right		181	1 0	181	2	183	183	22	207	1 0	207	2	209	1	209	0	209	1	209
WES	Right  Left-Through-Right  Left-Right		114	1 0 0	32	0	114	30	30	146	1 0 0	21	0	146	1 0 0	18	0	146	1 0 0	18
	CRITICAL V	OLUMES	_	th-South: ast-West: SUM:	639 539 1178	_	rth-South: East-West: SUM:	644 539 1183			th-South: ast-West: SUM:	772 569 1341			th-South: ast-West: SUM:				th-South: ast-West: SUM:	777 569 1346
	VOLUME/CAPACITY (V/C	) RATIO:		30M.	0.827		30M.	0.830			30	0.941			30.77.	0.945			JOH.	0.945
V/C	C LESS ATSAC/ATCS ADJUS	STMENT:			0.727			0.730				0.841				0.845				0.845
	LEVEL OF SERVICE	E (LOS):			C			C				D				D				D
<u></u>		MARKS:											ı							

2

Version: 1i Beta; 8/4/2011

## PROJECT IMPACT

Change in v/c due to project: 0.004  $\triangle v$ .

Significant impacted? NO

∆v/c after mitigation: 0.004
Fully mitigated? N/A

Intersection												
Intersection Delay, s/veh	55.2											
Intersection LOS	F											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	0	0	Λ	0	Λ	10	F02	700	0	0	0	
	U	U	U	U	U	19	582	789	0	0	U	U
Peak Hour Factor	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96
	~	•	0.96	ŭ	0.92	* *			•		0.96 2	0.96 2
Peak Hour Factor	~	•	0.96 2 0	ŭ	0.92 2 0	* *			•		0.96 2 0	0.96 2 0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	63.4	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3	
Vol Left, %	3%	0%	0%	0%	0%	
Vol Thru, %	97%	0%	100%	100%	0%	
Vol Right, %	0%	100%	0%	0%	100%	
Sign Control	Stop	Stop	Stop	Stop	Stop	
Traffic Vol by Lane	601	789	120	120	833	
LT Vol	19	0	0	0	0	
Through Vol	582	0	120	120	0	
RT Vol	0	789	0	0	833	
Lane Flow Rate	626	822	125	125	868	
Geometry Grp	8	8	7	7	7	
Degree of Util (X)	1	1	0.251	0.251	1	
Departure Headway (Hd)	6.929	6.21	7.218	7.218	4.79	
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	
Cap	532	592	501	501	764	
Service Time	4.626	3.916	4.918	4.918	2.49	
HCM Lane V/C Ratio	1.177	1.389	0.25	0.25	1.136	
HCM Control Delay	65.5	61.8	12.3	12.3	53.9	
HCM Lane LOS	F	F	В	В	F	
HCM 95th-tile Q	14	14.7	1	1	16.8	

Intersection					
Intersection Delay, s/veh					
Intersection LOS					
Movement	SBU	SBL	SBT	SBR	
Vol, veh/h	0	0	240	833	
Peak Hour Factor	0.92	0.96	0.96	0.96	
Heavy Vehicles, %	2	2	2	2	
Mvmt Flow	0	0	250	868	
Number of Lanes	0	0	2	1	
Approach			SB		
Opposing Approach					
Opposing Lanes			0		
Conflicting Approach Left			WB		
Conflicting Lanes Left Conflicting Approach Right			2		
Conflicting Lanes Right			0		
HCM Control Delay			44.6		
HCM LOS			Е		
Long					

Intersection												
Intersection Delay, s/veh	41.8											
Intersection LOS	Е											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	Λ	_	_									
VOI, VOIIII	0	0	0	0	0	38	474	567	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0 0.96	0 0.92	38 0.96	474 0.96	567 0.96	0 0.92	0 0.96	0 0.96	0.96
	_	•	·	•	0 0.92 2				_		•	0 0.96 2
Peak Hour Factor	_	•	·	•	0 0.92 2 0				_		•	0 0.96 2 0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	64	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3
Vol Left, %	7%	0%	0%	0%	0%
Vol Thru, %	93%	0%	100%	100%	0%
Vol Right, %	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	512	567	242	242	532
LT Vol	38	0	0	0	0
Through Vol	474	0	242	242	0
RT Vol	0	567	0	0	532
Lane Flow Rate	533	591	252	252	554
Geometry Grp	8	8	7	7	7
Degree of Util (X)	1	1	0.499	0.499	0.734
Departure Headway (Hd)	7.021	6.28	7.12	7.12	4.771
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes
Cap	517	579	502	502	759
Service Time	4.739	3.998	4.918	4.918	2.49
HCM Lane V/C Ratio	1.031	1.021	0.502	0.502	0.73
HCM Control Delay	66	62.2	16.9	16.9	19.5
HCM Lane LOS	F	F	С	С	С
HCM 95th-tile Q	13.8	14.6	2.7	2.7	6.6

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Intersection						
Intersection Delay, s/veh						
Intersection LOS						
Movement	SBU	SBL	SBT	SBR		
Vol, veh/h	0	0	484	532		
Peak Hour Factor	0.92	0.96	0.96	0.96		
Heavy Vehicles, %	2	2	2	2		
Mvmt Flow	0	0	504	554		
Number of Lanes	0	0	2	1		
Approach			SB			
Opposing Approach						
Opposing Lanes			0			
Conflicting Approach Left			WB			
Conflicting Lanes Left Conflicting Approach Right			2			
Conflicting Lanes Right			0			
HCM Control Delay			18.3			
HCM LOS			С			
Lano						Ī

Intersection												
Intersection Delay, s/veh	55.2											
Intersection LOS	F											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	0	0	0	0	0	19	584	789	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	0	0	0	20	608	822	0	0	0	0
Number of Lanes	0	0	0	0	0	0	1	1	0	0	0	0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	63.4	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3	
Vol Left, %	3%	0%	0%	0%	0%	
Vol Thru, %	97%	0%	100%	100%	0%	
Vol Right, %	0%	100%	0%	0%	100%	
Sign Control	Stop	Stop	Stop	Stop	Stop	
Traffic Vol by Lane	603	789	120	120	833	
LT Vol	19	0	0	0	0	
Through Vol	584	0	120	120	0	
RT Vol	0	789	0	0	833	
Lane Flow Rate	628	822	125	125	868	
Geometry Grp	8	8	7	7	7	
Degree of Util (X)	1	1	0.251	0.251	1	
Departure Headway (Hd)	6.929	6.21	7.218	7.218	4.79	
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	
Cap	528	592	501	501	764	
Service Time	4.626	3.916	4.918	4.918	2.49	
HCM Lane V/C Ratio	1.189	1.389	0.25	0.25	1.136	
HCM Control Delay	65.5	61.8	12.3	12.3	53.9	
HCM Lane LOS	F	F	В	В	F	
HCM 95th-tile Q	14	14.7	1	1	16.8	

ntersection					
Intersection Delay, s/veh					
Intersection LOS					
Movement	SBU	SBL	SBT	SBR	
Vol, veh/h	0	0	240	833	
Peak Hour Factor	0.92	0.96	0.96	0.96	
Heavy Vehicles, %	2	2	2	2	
Mvmt Flow	0	0	250	868	
Number of Lanes	0	0	2	1	
Approach			SB		
Opposing Approach					
Opposing Lanes			0		
Conflicting Approach Left			WB		
Conflicting Lanes Left			2		
Conflicting Approach Right					
Conflicting Lanes Right			0		
HCM Control Delay			44.6		
HCM LOS			Е		

Intersection												
Intersection Delay, s/veh	41.9											
Intersection LOS	Е											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	0	0	0	0	0	38	483	567	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	0	0	0	40	503	591	0	0	0	0
Number of Lanes	0	0	0	0	0	0	1	1	0	0	0	0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	64	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3	
Vol Left, %	7%	0%	0%	0%	0%	
Vol Thru, %	93%	0%	100%	100%	0%	
Vol Right, %	0%	100%	0%	0%	100%	
Sign Control	Stop	Stop	Stop	Stop	Stop	
Traffic Vol by Lane	521	567	242	242	532	
LT Vol	38	0	0	0	0	
Through Vol	483	0	242	242	0	
RT Vol	0	567	0	0	532	
Lane Flow Rate	543	591	252	252	554	
Geometry Grp	8	8	7	7	7	
Degree of Util (X)	1	1	0.5	0.5	0.734	
Departure Headway (Hd)	7.025	6.285	7.135	7.135	4.771	
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	
Сар	521	579	502	502	759	
Service Time	4.74	4	4.918	4.918	2.49	
HCM Lane V/C Ratio	1.042	1.021	0.502	0.502	0.73	
HCM Control Delay	66	62.2	16.9	16.9	19.5	
HCM Lane LOS	F	F	С	С	С	
HCM 95th-tile Q	13.8	14.6	2.8	2.8	6.6	

Interception Delay chick				
Intersection Delay, s/veh				
Intersection LOS				
Movement	SBU	SBL	SBT	SBR
Vol, veh/h	0	0	484	532
Peak Hour Factor	0.92	0.96	0.96	0.96
Heavy Vehicles, %	2	2	2	2
Mvmt Flow	0	0	504	554
Number of Lanes	0	0	2	1
Annroach			SB	
Approach			SD	
Opposing Approach				
Opposing Lanes			0	
Conflicting Approach Left			WB	
Conflicting Lanes Left			2	
Conflicting Approach Right				
Conflicting Lanes Right			0	
HCM Control Delay			18.3	
HCM LOS			С	

Intersection												
Intersection Delay, s/veh	54.4											
Intersection LOS	F											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	Λ	0	^	^	^	4.0	/ 10	0.14	_			
VOI, VCII/II	0	0	Ü	0	Ü	19	649	841	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0.96	0.92	0.96	0.96	841 0.96	0.92	0 0.96	0 0.96	0.96
		•	0.96 2	•	0.92				•		0 0.96 2	0.96 2
Peak Hour Factor		•	0.96 2 0	•	0 0.92 2 0				•		0 0.96 2 0	0.96 2 0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	64.3	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3
Vol Left, %	3%	0%	0%	0%	0%
Vol Thru, %	97%	0%	100%	100%	0%
Vol Right, %	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	668	841	183	183	850
LT Vol	19	0	0	0	0
Through Vol	649	0	183	183	0
RT Vol	0	841	0	0	850
Lane Flow Rate	696	876	190	190	885
Geometry Grp	8	8	7	7	7
Degree of Util (X)	1	1	0.381	0.381	1
Departure Headway (Hd)	7.056	6.348	7.218	7.218	4.79
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes
Cap	515	578	502	502	761
Service Time	4.79	4.082	4.918	4.918	2.49
HCM Lane V/C Ratio	1.351	1.516	0.378	0.378	1.163
HCM Control Delay	66.3	62.7	14.3	14.3	53.9
HCM Lane LOS	F	F	В	В	F
HCM 95th-tile Q	13.8	14.5	1.8	1.8	16.8

Intersection
Intersection Delay, s/veh
Intersection LOS
Movement SBU SBL SBT SBR
Vol, veh/h 0 0 365 850
Peak Hour Factor 0.92 0.96 0.96 0.96
Heavy Vehicles, % 2 2 2 2
Mvmt Flow 0 0 380 885
Number of Lanes 0 0 2 1
Approach SB
Opposing Approach
Opposing Lanes 0
Conflicting Approach Left WB
Conflicting Lanes Left 2
Conflicting Approach Right
Conflicting Lanes Right 0
HCM Control Delay 42
HCM LOS E
Lane

PM Peak Hour
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Intersection												
Intersection Delay, s/veh	44.7											
Intersection LOS	Е											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	0	0	0	0	0	39	639	664	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	0	0	0	41	666	692	0	0	0	0
Number of Lanes	0	0	0	0	0	0	1	1	0	0	0	0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	65	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3	
Vol Left, %	6%	0%	0%	0%	0%	
Vol Thru, %	94%	0%	100%	100%	0%	
Vol Right, %	0%	100%	0%	0%	100%	
Sign Control	Stop	Stop	Stop	Stop	Stop	
Traffic Vol by Lane	678	664	286	286	543	
LT Vol	39	0	0	0	0	
Through Vol	639	0	286	286	0	
RT Vol	0	664	0	0	543	
Lane Flow Rate	706	692	297	297	566	
Geometry Grp	8	8	7	7	7	
Degree of Util (X)	1	1	0.596	0.596	0.753	
Departure Headway (Hd)	7.199	6.467	7.218	7.218	4.79	
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	
Cap	509	567	503	503	758	
Service Time	4.899	4.167	4.918	4.918	2.49	
HCM Lane V/C Ratio	1.387	1.22	0.59	0.59	0.747	
HCM Control Delay	66.8	63.1	20	20	20.6	
HCM Lane LOS	F	F	С	С	С	
HCM 95th-tile Q	13.7	14.4	3.8	3.8	7	

PM Peak Hour

ntersection				
Intersection Delay, s/veh				
Intersection LOS				
Movement	SBU	SBL	SBT	SBR
Vol, veh/h	0	0	571	543
Peak Hour Factor	0.92	0.96	0.96	0.96
Heavy Vehicles, %	2	2	2	2
Mvmt Flow	0	0	595	566
Number of Lanes	0	0	2	1
Approach			SB	
Opposing Approach				
Opposing Lanes			0	
Conflicting Approach Left			WB	
Conflicting Lanes Left			2	
Conflicting Approach Right				
Conflicting Lanes Right			0	
HCM Control Delay			20.3	
HCM LOS			С	
Lane				

Intersection												
Intersection Delay, s/veh	54.4											
Intersection LOS	F											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	٥	^										
VOI, VCII/II	0	0	0	0	0	19	651	841	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0 0.96	0 0.92	19 0.96	651 0.96	841 0.96	0 0.92	0 0.96	0 0.96	0.96
	-	•	0 0.96 2	•	0 0.92 2			~	•		0 0.96 2	0 0.96 2
Peak Hour Factor	-	•	0 0.96 2 0	•	0 0.92 2 0			~	•		0 0.96 2 0	0 0.96 2 0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	64.3	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3
Vol Left, %	3%	0%	0%	0%	0%
Vol Thru, %	97%	0%	100%	100%	0%
Vol Right, %	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	670	841	183	183	850
LT Vol	19	0	0	0	0
Through Vol	651	0	183	183	0
RT Vol	0	841	0	0	850
Lane Flow Rate	698	876	190	190	885
Geometry Grp	8	8	7	7	7
Degree of Util (X)	1	1	0.381	0.381	1
Departure Headway (Hd)	7.056	6.348	7.218	7.218	4.79
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes
Cap	516	578	502	502	761
Service Time	4.79	4.082	4.918	4.918	2.49
HCM Lane V/C Ratio	1.353	1.516	0.378	0.378	1.163
HCM Control Delay	66.3	62.7	14.3	14.3	53.9
HCM Lane LOS	F	F	В	В	F
HCM 95th-tile Q	13.8	14.5	1.8	1.8	16.8

SBU	SBL	SBT	SBR
0	0	365	850
0.92	0.96	0.96	0.96
2	2	2	2
0	0	380	885
0	0	2	1
		SB	
		0	
		WB	
		2	
		0	
		42	
		Е	
	0 0.92 2 0	0 0 0.92 0.96 2 2 0 0	0 0 365 0.92 0.96 0.96 2 2 2 2 0 0 380 0 0 2  SB  0 WB 2

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Intersection												
Intersection Delay, s/veh	44.8											
Intersection LOS	E											
Movement	EBU	EBL	EBT	EBR	WBU	WBL	WBT	WBR	NBU	NBL	NBT	NBR
Vol, veh/h	0	0	0	0	0	39	648	664	0	0	0	0
Peak Hour Factor	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96	0.92	0.96	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	0	0	0	41	675	692	0	0	0	0
Number of Lanes	0	0	0	0	0	0	1	1	0	0	0	0

Approach	WB	
Opposing Approach		
Opposing Lanes	0	
Conflicting Approach Left		
Conflicting Lanes Left	0	
Conflicting Approach Right	SB	
Conflicting Lanes Right	3	
HCM Control Delay	65	
HCM LOS	F	

Lane	WBLn1	WBLn2	SBLn1	SBLn2	SBLn3
Vol Left, %	6%	0%	0%	0%	0%
Vol Thru, %	94%	0%	100%	100%	0%
Vol Right, %	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	687	664	286	286	543
LT Vol	39	0	0	0	0
Through Vol	648	0	286	286	0
RT Vol	0	664	0	0	543
Lane Flow Rate	716	692	297	297	566
Geometry Grp	8	8	7	7	7
Degree of Util (X)	1	1	0.596	0.596	0.753
Departure Headway (Hd)	7.199	6.467	7.218	7.218	4.79
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes
Cap	508	567	503	503	758
Service Time	4.899	4.167	4.918	4.918	2.49
HCM Lane V/C Ratio	1.409	1.22	0.59	0.59	0.747
HCM Control Delay	66.8	63.1	20	20	20.6
HCM Lane LOS	F	F	С	С	С
HCM 95th-tile Q	13.7	14.4	3.8	3.8	7

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Intersection Delay, s/veh					
Intersection LOS					
IIIICI SCCIIOII LOS					
Movement	SBU	SBL	SBT	SBR	
Vol, veh/h	0	0	571	543	
Peak Hour Factor	0.92	0.96	0.96	0.96	
Heavy Vehicles, %	2	2	2	2	
Mvmt Flow	0	0	595	566	
Number of Lanes	0	0	2	1	
A			CD		
Approach			SB		
Opposing Approach					
Opposing Lanes			0		
Conflicting Approach Left			WB		
Conflicting Lanes Left			2		
Conflicting Approach Right					
Conflicting Lanes Right			0		
HCM Control Delay			20.3		
HCM LOS			С		

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# **Level of Service Workheet**

(Circular 212 Method)



I/S #:	North-South Street:	Robertse	on Boulevar	·d		Yea	r of Count	2016	Amb	ient Grov	wth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	,
23	East-West Street:	I-10 WB	On-Ramp/R	obertson	BI	Proje	ction Year	2018		Pe	ak Hour:	AM	Revie	wed by:	R	RA	Project:		RA491	
1	posed Ø'ing: N/S-1, E/W-2 or		NB 0	SB	0 0 1	NB	0 SE	0 0 1	NB	0	SB	0 0 1	NB	0	SB	0 0 1	NB	0	SB	0 0 1
Right	Turns: FREE-1, NRTOR-2 or		EB 0	WB	1	EB	0 WE	3 1	EB	0	WB	1	EB	0	WB	1	EB	0	WB	1
	ATSAC-1 or ATSAC+. Override				1200			0 1200				0 1200				0 1200				0 1200
			EXISTI	NG CONDI			ING PLUS P	ROJECT			ON W/O PF			RE CONDIT				W/ PROJE		
	MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
₽	↑ Left		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	0
1	← Left-Through  ↑ Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
l BG	† Through-Right			0							0				0				0	-
NORTHBOUND	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	← Left-Through-Right  ← Left-Right			0 0							0 0				0				0 0	
	Leit-Right			U								1							0	
Δ	→ Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SOUTHBOUND			240	0 2	120	0	240	120	120	365	0 2	183	0	365	0 2	183	0	365	0 2	183
BO	→ Through  Through-Right		240	0	120	U	240	120	120	303	0	103	0	303	0	103	U	303	0	103
1 5	ب _ Right		833	1	0	0	833	0	0	850	1	0	0	850	1	0	0	850	1	0
SOI	Left-Through-Right			0							0				0				0	
	↓ Left-Right			0							0				0				U	
	ال Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
EASTBOUND	→ Left-Through			0						_	0				0			_	0	
30.	→ Through  → Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	0
STE	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
EA	Left-Through-Right			0							0				0				0	
	- ≺ Left-Right			0							0				0				0	
	√ Left		19	0	19	0	19	19	0	19	0	19	0	19	0	19	0	19	0	19
WESTBOUND				1		_					1		_		1		_		1	
301	← Through ← Through-Right		582	0 0	601	2	584	603	55	649	0 0	668	2	651	0	670	0	651	0	670
STE	Right		789	1	0	0	789	0	36	841	1	0	0	841	1	0	0	841	1	0
WE	Left-Through-Right			0							0				0				0	
			A/	0 th-South:	120	A/-	rth-South:	120		Ma:	0 th-South:	183		Ma-	th-South:	183		Ale:-	0 th-South:	183
	CRITICAL V	OLUMES		tn-Soutn: ast-West:	601		rtn-Soutn: East-West:	603			าก-Soutn: ast-West:	668			tn-Soutn: ast-West:				tn-Soutn: ast-West:	670
				SUM:	721		SUM:	723			SUM:	851			SUM:				SUM:	853
	VOLUME/CAPACITY (V/C	) RATIO:			0.601			0.603				0.709				0.711				0.711
V/0	C LESS ATSAC/ATCS ADJUS	STMENT:			0.601			0.603				0.709				0.711				0.711
	LEVEL OF SERVIC	E (LOS):	<u> </u>		В			В				С				С				С
REMARKS: Unsignalized intersection.																				

Version: 1i Beta; 8/4/2011

#### PROJECT IMPACT

Change in v/c due to project: 0.002  $\Delta v/c$  after mitigation: 0.002 Significant impacted? NO Fully mitigated? N/A



# **Level of Service Workheet**

(Circular 212 Method)



I/S #:	North-South Street:	Robertso	on Boulevar	ď		Yea	r of Count	2016	Amb	ient Grov	wth: (%):	1	Condu	cted by:	R	RA	Date:		1/24/2017	,
23	East-West Street:	I-10 WB	On-Ramp/R	obertson	BI	Proje	ction Year:	2018		Pea	ak Hour:	PM	Revie	ewed by:	R	RA	Project:		RA491	
	posed Ø'ing: N/S-1, E/W-2 or		NB 0	SB	0 0 1	NB	0 SB	0 0 1	NB	0	SB	0 0 1	NB	0	SB	0 0 1	NB	0	SB	0 0 1
Right	Turns: FREE-1, NRTOR-2 or	OLA-3?	EB 0	WB	1	EB	0 SE		EB	0	WB	1	EB	0	WB	1	EB	0	WB	1
	ATSAC-1 or ATSAC+				0 1200			0 1200				0 1200				0 1200				0 1200
	Override (	Сараспу	FXISTI	NG CONDIT		FXIST	ING PLUS P		FUTUR	E CONDITION	ON W/O PR		FUTUI	RE CONDIT	ION W/ PR		FUTURE	W/ PROJE	CT W/ MIT	
	MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Project	Total	No. of	Lane	Added	Total	No. of	Lane
			Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
D	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
S	← Left-Through ↑ Through		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	0
<u>8</u>	↑ Through-Right			0	ŭ	Ĭ	Ü	Ū		Ü	0	ŭ		Ū	0	J	Ů	Ü	0	O
NORTHBOUND	→ Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	Left-Through-Right			0							0				0				0	
	← Left-Right			0							0				0				0	
	→ Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Š	Left-Through		40.4	0			40.4	242			0		•		0		•		0	
BO			484	2 0	242	0	484	242	77	571	2 0	286	0	571	2 0	286	0	571	2	286
₹	بار Right		532	1	0	0	532	0	0	543	1	0	0	543	1	0	0	543	1	0
SOUTHBOUND	Left-Through-Right			0							0				0				0	
	↓ Left-Right		l	0							0				0				0	
	ے Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	→ Left-Through			0	_				_	_	0		_		0			_	0	
EASTBOUND	→ Through  → Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0 0	0
STE	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
EA	Left-Through-Right			0							0				0				0	
	- ≺ Left-Right		l	0							0				0				0	
	√ Left		38	0	38	0	38	38	0	39	0	39	0	39	0	39	0	39	0	39
WESTBOUND				1	F		400				1		_	0.10	1			0.40	1	
301	← Through ← Through-Right		474	0 0	512	9	483	521	155	639	0 0	678	9	648	0	687	0	648	0	687
ST	Right		567	1	0	0	567	0	86	664	1	0	0	664	1	0	0	664	1	0
WE	Left-Through-Right			0							0				0				0	
	├ Left-Right		Nor	th-South:	242	No	rth-South:	242		Nor	0 th-South:	286		Nor	th-South:	286		Non	0 th-South:	286
	CRITICAL VO	OLUMES		ast-West:	512		ast-West:	521			ast-West:	678			ast-West:	687			ast-West:	687
-				SUM:	754	ļ	SUM:	763			SUM:	964			SUM:	973	ļ		SUM:	973
	VOLUME/CAPACITY (V/C)				0.628			0.636				0.803				0.811				0.811
V/0	C LESS ATSAC/ATCS ADJUS				0.628			0.636				0.803				0.811				0.811
	LEVEL OF SERVIC				В			В				D				D				D
REMARKS: Unsignalized intersection.																				

Version: 1i Beta; 8/4/2011

#### PROJECT IMPACT

Change in v/c due to project: 0.008  $\Delta v/c$  after mitigation: 0.008 Significant impacted? NO Fully mitigated? N/A

Intersection									
Intersection Delay, s/veh	10.4								
Intersection LOS	В								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	4	0	0	0	0	247	11
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	4	0	0	0	0	257	11
Number of Lanes	0	0	1	0	0	0	0	1	1
Approach			EB					SB	

Approach	EB	SB
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	7.7	10.4
HCM LOS	А	В

Lane	EBLn1	SBLn1	SBLn2	
Vol Left, %	0%	100%	0%	
Vol Thru, %	100%	0%	0%	
Vol Right, %	0%	0%	100%	
Sign Control	Stop	Stop	Stop	
Traffic Vol by Lane	4	247	11	
LT Vol	0	247	0	
Through Vol	4	0	0	
RT Vol	0	0	11	
Lane Flow Rate	4	257	11	
Geometry Grp	2	7	7	
Degree of Util (X)	0.005	0.36	0.012	
Departure Headway (Hd)	4.648	5.042	3.842	
Convergence, Y/N	Yes	Yes	Yes	
Cap	775	718	937	
Service Time	2.648	2.744	1.544	
HCM Lane V/C Ratio	0.005	0.358	0.012	
HCM Control Delay	7.7	10.6	6.6	
HCM Lane LOS	А	В	Α	
HCM 95th-tile Q	0	1.6	0	

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Intersection									
Intersection Delay, s/veh	14.9								
Intersection LOS	В								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	66	0	0	0	0	431	62
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	69	0	0	0	0	449	65
Number of Lanes	0	0	1	0	0	0	0	1	1

Approach	EB	SB
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	8.8	15.7
HCM LOS	А	С

Lane	EBLn1	SBLn1	SBLn2	
Vol Left, %	0%	100%	0%	
Vol Thru, %	100%	0%	0%	
Vol Right, %	0%	0%	100%	
Sign Control	Stop	Stop	Stop	
Traffic Vol by Lane	66	431	62	
LT Vol	0	431	0	
Through Vol	66	0	0	
RT Vol	0	0	62	
Lane Flow Rate	69	449	65	
Geometry Grp	2	7	7	
Degree of Util (X)	0.1	0.643	0.071	
Departure Headway (Hd)	5.231	5.155	3.954	
Convergence, Y/N	Yes	Yes	Yes	
Cap	690	696	894	
Service Time	3.231	2.933	1.73	
HCM Lane V/C Ratio	0.1	0.645	0.073	
HCM Control Delay	8.8	16.9	7	
HCM Lane LOS	А	С	Α	
HCM 95th-tile Q	0.3	4.7	0.2	

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Intersection									
Intersection Delay, s/veh	10.4								
Intersection LOS	В								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	4	0	0	0	0	247	11
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	4	0	0	0	0	257	11
Number of Lanes	0	0	1	0	0	0	0	1	1
Approach			EB					SB	
Opposing Approach									
Opposing Lanes			0					0	
O (1' 1' A   1   C			0.0						

ripproderi	LD	35
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	7.7	10.4
HCM LOS	А	В

Lane	EBLn1	SBLn1	SBLn2	
Vol Left, %	0%	100%	0%	
Vol Thru, %	100%	0%	0%	
Vol Right, %	0%	0%	100%	
Sign Control	Stop	Stop	Stop	
Traffic Vol by Lane	4	247	11	
LT Vol	0	247	0	
Through Vol	4	0	0	
RT Vol	0	0	11	
Lane Flow Rate	4	257	11	
Geometry Grp	2	7	7	
Degree of Util (X)	0.005	0.36	0.012	
Departure Headway (Hd)	4.648	5.042	3.842	
Convergence, Y/N	Yes	Yes	Yes	
Cap	775	718	937	
Service Time	2.648	2.744	1.544	
HCM Lane V/C Ratio	0.005	0.358	0.012	
HCM Control Delay	7.7	10.6	6.6	
HCM Lane LOS	Α	В	Α	
HCM 95th-tile Q	0	1.6	0	

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Intersection									
Intersection Delay, s/veh	13.3								
Intersection LOS	В								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	4	0	0	0	0	372	11
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	4	0	0	0	0	388	11
Number of Lanes	0	0	1	0	0	0	0	1	1

Approach	EB	SB
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	8	13.4
HCM LOS	А	В

Lane	EBLn1	SBLn1	SBLn2	
Vol Left, %	0%	100%	0%	
Vol Thru, %	100%	0%	0%	
Vol Right, %	0%	0%	100%	
Sign Control	Stop	Stop	Stop	
Traffic Vol by Lane	4	372	11	
LT Vol	0	372	0	
Through Vol	4	0	0	
RT Vol	0	0	11	
Lane Flow Rate	4	388	11	
Geometry Grp	2	7	7	
Degree of Util (X)	0.006	0.543	0.012	
Departure Headway (Hd)	4.999	5.042	3.842	
Convergence, Y/N	Yes	Yes	Yes	
Cap	720	721	936	
Service Time	2.999	2.746	1.546	
HCM Lane V/C Ratio	0.006	0.538	0.012	
HCM Control Delay	8	13.6	6.6	
HCM Lane LOS	А	В	Α	
HCM 95th-tile Q	0	3.3	0	

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•									
Intersection									
Intersection Delay, s/veh	14.9								
Intersection LOS	В								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	66	0	0	0	0	431	62
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	69	0	0	0	0	449	65
Number of Lanes	0	0	1	0	0	0	0	1	1
Approach			EB					SB	
Opposing Approach						•	•	•	
Opposing Lance			Λ					Λ	

Approach	EB	SB
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	8.8	15.7
HCM LOS	А	С

Lane	EBLn1	SBLn1	SBLn2	
Vol Left, %	0%	100%	0%	
Vol Thru, %	100%	0%	0%	
Vol Right, %	0%	0%	100%	
Sign Control	Stop	Stop	Stop	
Traffic Vol by Lane	66	431	62	
LT Vol	0	431	0	
Through Vol	66	0	0	
RT Vol	0	0	62	
Lane Flow Rate	69	449	65	
Geometry Grp	2	7	7	
Degree of Util (X)	0.1	0.643	0.071	
Departure Headway (Hd)	5.231	5.155	3.954	
Convergence, Y/N	Yes	Yes	Yes	
Cap	690	696	894	
Service Time	3.231	2.933	1.73	
HCM Lane V/C Ratio	0.1	0.645	0.073	
HCM Control Delay	8.8	16.9	7	
HCM Lane LOS	А	С	Α	
HCM 95th-tile Q	0.3	4.7	0.2	

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Intersection									
Intersection Delay, s/veh	20.2								
Intersection LOS	С								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	67	0	0	0	0	517	63
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	70	0	0	0	0	539	66
Number of Lanes	0	0	1	0	0	0	0	1	1

Approach	EB	SB
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	9.1	21.5
HCM LOS	Α	С

Lane	EBLn1	SBLn1	SBLn2
Vol Left, %	0%	100%	0%
Vol Thru, %	100%	0%	0%
Vol Right, %	0%	0%	100%
Sign Control	Stop	Stop	Stop
Traffic Vol by Lane	67	517	63
LT Vol	0	517	0
Through Vol	67	0	0
RT Vol	0	0	63
Lane Flow Rate	70	539	66
Geometry Grp	2	7	7
Degree of Util (X)	0.106	0.771	0.072
Departure Headway (Hd)	5.463	5.157	3.956
Convergence, Y/N	Yes	Yes	Yes
Cap	660	695	892
Service Time	3.463	2.944	1.742
HCM Lane V/C Ratio	0.106	0.776	0.074
HCM Control Delay	9.1	23.3	7.1
HCM Lane LOS	А	С	Α
HCM 95th-tile Q	0.4	7.4	0.2

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Intersection									
Intersection Delay, s/veh	13.3								
Intersection LOS	В								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	4	0	0	0	0	372	11
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	4	0	0	0	0	388	11
Number of Lanes	0	0	1	0	0	0	0	1	1

Approach	EB	SB
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	8	13.4
HCM LOS	Α	В

Lane	EBLn1	SBLn1	SBLn2	
Vol Left, %	0%	100%	0%	
Vol Thru, %	100%	0%	0%	
Vol Right, %	0%	0%	100%	
Sign Control	Stop	Stop	Stop	
Traffic Vol by Lane	4	372	11	
LT Vol	0	372	0	
Through Vol	4	0	0	
RT Vol	0	0	11	
Lane Flow Rate	4	388	11	
Geometry Grp	2	7	7	
Degree of Util (X)	0.006	0.543	0.012	
Departure Headway (Hd)	4.999	5.042	3.842	
Convergence, Y/N	Yes	Yes	Yes	
Cap	720	721	936	
Service Time	2.999	2.746	1.546	
HCM Lane V/C Ratio	0.006	0.538	0.012	
HCM Control Delay	8	13.6	6.6	
HCM Lane LOS	А	В	Α	
HCM 95th-tile Q	0	3.3	0	

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Intersection									
Intersection Delay, s/veh	20.2								
Intersection LOS	С								
Movement	EBU	EBL	EBT	WBU	WBT	WBR	SBU	SBL	SBR
Vol, veh/h	0	0	67	0	0	0	0	517	63
Peak Hour Factor	0.92	0.96	0.96	0.92	0.96	0.96	0.92	0.96	0.96
Heavy Vehicles, %	2	2	2	2	2	2	2	2	2
Mvmt Flow	0	0	70	0	0	0	0	539	66
Number of Lanes	0	0	1	0	0	0	0	1	1
Approach			EB					SB	
Opposing Approach									_
Opposing Lanes			0					0	
Conflicting Approach Left			SB						

Арргоаст	LD	JD
Opposing Approach		
Opposing Lanes	0	0
Conflicting Approach Left	SB	
Conflicting Lanes Left	2	0
Conflicting Approach Right		EB
Conflicting Lanes Right	0	1
HCM Control Delay	9.1	21.5
HCM LOS	А	С

Lane	EBLn1	SBLn1	SBLn2		
Vol Left, %	0%	100%	0%		
Vol Thru, %	100%	0%	0%		
Vol Right, %	0%	0%	100%		
Sign Control	Stop	Stop	Stop		
Traffic Vol by Lane	67	517	63		
LT Vol	0	517	0		
Through Vol	67	0	0		
RT Vol	0	0	63		
Lane Flow Rate	70	539	66		
Geometry Grp	2	7	7		
Degree of Util (X)	0.106	0.771	0.072		
Departure Headway (Hd)	5.463	5.157	3.956		
Convergence, Y/N	Yes	Yes	Yes		
Cap	660	695	892		
Service Time	3.463	2.944	1.742		
HCM Lane V/C Ratio	0.106	0.776	0.074		
HCM Control Delay	9.1	23.3	7.1		
HCM Lane LOS	А	С	Α		
HCM 95th-tile Q	0.4	7.4	0.2		

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# **Level of Service Workheet**

(Circular 212 Method)



I/S #:	North-South Street: Rob	ertson Bo	n Boulevard		Year of Count: 20°		2016	Ambient Growth: (%):			1	Conducted by:		: RA		Date: 1/24/20		1/24/2017	,	
24	East-West Street: Exp	osition B	Boulevar	ď		Projec	ction Year:	2018	Peak Hour:		AM	Reviewed by:		R	RA	Project:		RA491		
	No. of Phas				0			0				0				0				0
	oosed Ø'ing: N/S-1, E/W-2 or Both	A/D	0	SB	0 1	NB	0 SB	0	NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
Right 1	Turns: FREE-1, NRTOR-2 or OLA-	3?   NB-		WB	0	EB	0 SB		EB	0	WB	0	EB	0	WB	0	EB	0	WB	0
	ATSAC-1 or ATSAC+ATCS				0	,		0	·			0				0				0
	Override Capac	ity	=>//0=11		1200	57/107		1200	5117115	5 00 UDITU		1200				1200			OT 14// 14/7	1200
	MOVEMENT		EXISTIN	NG CONDIT	Lane	Project	Total		Added	E CONDITION Total	No. of	Lane	Project	Total	No. of	Lane	Added	W/ PROJE	No. of	Lane
	MO VEMENT	Vo	olume	Lanes	Volume	Traffic	Volume	Lane Volume	Volume	Volume	Lanes	Volume	Traffic	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
	↑ Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NORTHBOUND	← Left-Through			0		_			_	_	0		_		0		_		0	
BOI	↑ Through		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
王	Through-Right Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Š	Left-Through-Right			0	ŭ		ŭ	· ·		ŭ	0	ŭ		· ·	0	ŭ		ŭ	0	ŭ
				0							0				0				0	
	↓ Left		247	1	247	0	247	247	120	372	1	372	0	372	1	372	0	372	1	372
9	Left-Through		241	0	241	U	241	241	120	312	0	312	0	312	0	312	U	312	0	312
og	Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
뿔	Through-Right		44	0	0		44	0		44	0 1	•		44	0	0	•	44	0 1	0
SOUTHBOUND			11	0	0	0	11	0	0	11	0	0	0	11	0	0	0	11	0	0
Ñ	Left-Right			0							0				Ö				0	
	1	-									_									
Ω	J Left     ∴ Left-Through		0	0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
5	→ Through		4	1	4	0	4	4	0	4	1	4	0	4	1	4	0	4	1	4
<u>B</u>	→ Through-Right			0							0				0				0	
EASTBOUND	Right  Left-Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
ш	Left-Right			0							0				0				0	
	*	- 1	Ī																	
۵			0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
WESTBOUND	√ Leπ-Inrough  ← Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
<u>8</u>	Through-Right		_	0		_	-			-	0	_		-	0		_	-	0	
ES	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
>	Left-Through-Right Left-Right			0							0 0				0				0	
	γ —-····g···		Nort	th-South:	247	No	rth-South:	247		Nor	th-South:	372		Nort	th-South:	372		Non	h-South:	372
	CRITICAL VOLUM	ES	Ea	ast-West:	4	E	ast-West:	4		E	ast-West:	4		Ea	ast-West:	4		Ea	st-West:	4
	VOLUME/CARACITY (V/C) RAT	<u></u>		SUM:	251		SUM:	251			SUM:	376			SUM:				SUM:	376
1//0	VOLUME/CAPACITY (V/C) RAT				0.209			0.209				0.313				0.313				0.313
V/C	LESS ATSAC/ATCS ADJUSTME				0.209			0.209				0.313				0.313				0.313
	LEVEL OF SERVICE (LO		. ,	ntersection.	Α			Α				Α				Α				Α

Version: 1i Beta; 8/4/2011

#### PROJECT IMPACT

Change in v/c due to project: 0.000  $\Delta v/c$  after mitigation: 0.000 Significant impacted? NO Fully mitigated? N/A



# **Level of Service Workheet**

(Circular 212 Method)



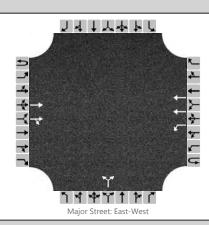
I/S #:	North-South Street:	Robertso	on Boulevar	n Boulevard		Yea	r of Count:	2016	Ambient Growth: (%):			Conducted by:			RA Date:		1/24/2017		,	
24	East-West Street:	Expositi	on Bouleva	rd		Proje	ction Year:	2018		Pe	ak Hour:	PM	Revie	ewed by:	R	!A	Project:		RA491	
	No. o posed Ø'ing: N/S-1, E/W-2 or Turns: FREE-1, NRTOR-2 or		NB 0	SB	0 0 1	NB	0 SB	0 0 1	NB	0	SB	0 0 1	NB	0	SB	0 0 1	NB	0	SB	0 0 1
Right	·		EB 0	WB	0	EB	0 WE		EB	0	WB	0	EB	0	WB	0	EB	0	WB	0
	ATSAC-1 or ATSAC+				0 1200			0 1200				0 1200				0 1200				0 1200
			EXISTI	NG CONDIT			TING PLUS P	ROJECT			ON W/O PR			RE CONDIT				W/ PROJE		
	MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
Ω	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
N	← Left-Through  ↑ Through		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	0	0
層	↑ Through-Right		· ·	0	ŭ		ŭ			Ü	0	Ů		Ü	0	J		Ŭ	0	·
NORTHBOUND	→ Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2	← Left-Through-Right			0							0				0				0	
				0							0				0				0	
	→ Left		431	1	431	0	431	431	77	517	1	517	0	517	1	517	0	517	1	517
SOUTHBOUND	→ Left-Through			0							0				0				0	
) S	Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
₹	→ Through-Right → Right		62	0 1	0	0	62	0	0	63	0 1	0	0	63	1	0	0	63	0 1	0
l o	Left-Through-Right		02	0	ŭ		02	· ·		00	0	Ŭ		00	0	J		00	0	O
S	↓ Left-Right		l	0							0				0				0	
	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
₽	→ Left-Through		U	0	U	0	U	U		U	0	U		U	0	U	"	U	0	U
EASTBOUND	→ Through		66	1	66	0	66	66	0	67	1	67	0	67	1	67	0	67	1	67
TB(	→ Through-Right			0	6	_			_	•	0		_		0			0	0	
AS	Right  Left-Through-Right		0	0 0	0	0	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0
"	→ Left-Right			0							0				0				0	
											-									
Ω			0	0 0	0	0	0	0	0	0	0	0	0	0	0 0	0	0	0	0	0
WESTBOUND	← Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
IBC	← Through-Right			0							0				0				0	
ES.	Right		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
>	Left-Through-Right Left-Right			0 0							0 0				0				0	
	, <u></u>		Nor	th-South:	431	No	rth-South:	431		Nor	th-South:	517		Nor	th-South:	517		Non	th-South:	517
	CRITICAL VO	OLUMES	E	ast-West:	66	Į į	East-West:	66		E	ast-West:	67		E	ast-West:	67		Ea	ast-West:	67
-	VOLUME (OADAOITY (1/2	) DATIO		SUM:	497		SUM:	497			SUM:	584			SUM:	584	-		SUM:	584
	VOLUME/CAPACITY (V/C	•			0.414			0.414				0.487				0.487				0.487
V/0	C LESS ATSAC/ATCS ADJUS				0.414			0.414				0.487				0.487				0.487
	LEVEL OF SERVIC				Α			Α				Α				Α				Α
	RE	MARKS:	Unsignalized i	intersection.																

Version: 1i Beta; 8/4/2011

#### PROJECT IMPACT

Change in v/c due to project: 0.000  $\Delta v/c$  after mitigation: 0.000 Fully mitigated? N/A Significant impacted? NO

	HCS 2010 Two-Way Stop Control Summary Report												
General Information		Site Information											
Analyst	Raju Associates	Intersection	Wesley & Washington										
Agency/Co.		Jurisdiction	Culver City										
Date Performed	3/29/2016	East/West Street	Washington Bl										
Analysis Year	2016	North/South Street	Wesley St										
Time Analyzed	AM Peak Hour	Peak Hour Factor	0.87										
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25										
Project Description	Existing 2016												



### **Vehicle Volumes and Adjustments**

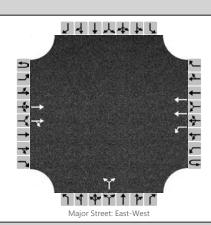
Approach		Eastb	ound		Westbound					North	bound		Southbound				
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R	
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12	
Number of Lanes	0	0	2	0	0	1	2	0		0	0	0		0	0	0	
Configuration			Т	TR		L	Т				LR						
Volume (veh/h)			709	20		11	1555			2		5					
Percent Heavy Vehicles						3				3		3					
Proportion Time Blocked																	
Right Turn Channelized		N	lo			N	lo			N	0			N	lo		
Median Type								Undivided									

# Delay, Queue Length, and Level of Service

Median Storage

Flow Rate (veh/h)						13				8			
Capacity						786				217			
v/c Ratio						0.02				0.04			
95% Queue Length						0.1				0.1			
Control Delay (s/veh)						9.7				22.3			
Level of Service (LOS)						Α				С			
Approach Delay (s/veh)						0	.1		22	1.3			
Approach LOS								(	2				

HCS 2010 Two-Way Stop Control Summary Report											
General Information		Site Information									
Analyst	Raju Associates	Intersection	Wesley & Washington								
Agency/Co.		Jurisdiction	Culver City								
Date Performed	3/29/2016	East/West Street	Washington Bl								
Analysis Year	2016	North/South Street	Wesley St								
Time Analyzed	PM Peak Hour	Peak Hour Factor	0.93								
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25								
Project Description	Existing (2016)										



### **Vehicle Volumes and Adjustments**

Approach		Eastb	ound	Westbound					Northbound				Southbound					
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R		
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12		
Number of Lanes	0	0	2	0	0	1	2	0		0	0	0		0	0	0		
Configuration			Т	TR		L	Т				LR							
Volume (veh/h)			1359	3		5	1013			7		10						
Percent Heavy Vehicles						3				3		3						
Proportion Time Blocked																		
Right Turn Channelized		N	lo			Ν	lo			N	0			N	lo			
Median Type	Undivided																	

M. P. C.

Median Storage

# Delay, Queue Length, and Level of Service

Flow Rate (veh/h)			5				19			
Capacity			452				99			
v/c Ratio			0.01				0.19			
95% Queue Length			0.0				0.7			
Control Delay (s/veh)			13.0				49.7			
Level of Service (LOS)			В				E			
Approach Delay (s/veh)			0	.1		49	.7			
Approach LOS						E				

**INT # 25** 

North/South Street: WESLEY STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

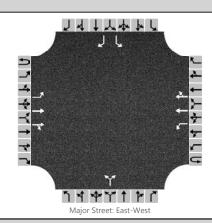
Thru Lane:	1200 vph	N-S Split Phase :	N
Left-Turn Lane:	1200 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000
	TH	0.00	0	0	0.000 *	N-S(2):	0.006 *
	LT	0.00	0	0	0.000	E-W(1):	0.313
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.648 *
	TH	2.00	1,555	2,400	0.648 *		
	LT	1.00	11	1,200	0.009	V/C:	0.654
Northbound	RT	0.71	5	857	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	0.000
	LT	0.29	2	343	0.006 *		
Eastbound	RT	0.00	20	0	0.000	ICU:	0.754
	TH	2.00	709	2,400	0.304		
	LT	0.00	0	0	0.000 *	LOS:	С
Deal Bestell	DM DEAK!	IOLID					
Peak Period:	PM PEAK H		Volume	Consoity	V/C	ICU ANA	LVCIC
Approach Southbound	RT	Lanes		Capacity	٧/٥	ICU ANA	
				n n	0 000	NI C/1).	
Southbound		0.00	0	0	0.000	N-S(1):	0.007
Southbound	TH	0.00	0	0	0.000 *	N-S(2):	0.007 0.014 *
	TH LT	0.00 0.00	0	0	0.000 * 0.000	N-S(2): E-W(1):	0.007 0.014 * 0.572 *
Westbound	TH LT RT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 * 0.000 0.000	N-S(2):	0.007 0.014 *
	TH LT RT TH	0.00 0.00 0.00 2.00	0 0 0 1,013	0 0 0 0 2,400	0.000 * 0.000 0.000 0.422	N-S(2): E-W(1): E-W(2):	0.007 0.014 * 0.572 * 0.422
Westbound	TH LT RT TH LT	0.00 0.00 0.00 2.00 1.00	0 0 0 1,013 5	0 0 0 2,400 1,200	0.000 * 0.000 0.000 0.422 0.004 *	N-S(2): E-W(1): E-W(2): V/C:	0.007 0.014 * 0.572 * 0.422 0.586
	TH LT RT TH LT	0.00 0.00 0.00 2.00 1.00 0.59	0 0 0 1,013 5	0 0 0 2,400 1,200 706	0.000 * 0.000 0.000 0.422 0.004 * 0.007	N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.007 0.014 * 0.572 * 0.422 0.586 0.100
Westbound	TH LT RT TH LT RT TH	0.00 0.00 0.00 2.00 1.00 0.59 0.00	0 0 0 1,013 5 10 0	0 0 0 2,400 1,200 706 0	0.000 * 0.000 0.000 0.422 0.004 * 0.007 0.000	N-S(2): E-W(1): E-W(2): V/C:	0.007 0.014 * 0.572 * 0.422 0.586
Westbound  Northbound	TH LT RT TH LT RT TH LT	0.00 0.00 2.00 1.00 0.59 0.00 0.41	0 0 0 1,013 5 10 0 7	0 0 0 2,400 1,200 706 0 494	0.000 * 0.000 0.000 0.422 0.004 * 0.007 0.000 0.014 *	N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.007 0.014 * 0.572 * 0.422 0.586 0.100 0.000
Westbound	TH LT RT TH LT RT TH LT	0.00 0.00 2.00 1.00 0.59 0.00 0.41	0 0 0 1,013 5 10 0 7	0 0 0 2,400 1,200 706 0 494	0.000 * 0.000 0.000 0.422 0.004 * 0.007 0.000 0.014 * 0.000	N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.007 0.014 * 0.572 * 0.422 0.586 0.100
Westbound  Northbound	TH LT RT TH LT RT TH LT	0.00 0.00 2.00 1.00 0.59 0.00 0.41	0 0 0 1,013 5 10 0 7	0 0 0 2,400 1,200 706 0 494	0.000 * 0.000 0.000 0.422 0.004 * 0.007 0.000 0.014 *	N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.007 0.014 * 0.572 * 0.422 0.586 0.100 0.000

Unsignalized intersection.

^{* =} Critical Movement

	HCS 2010 Two-Way Stop Control Summary Report											
General Information		Site Information										
Analyst	Raju Associates	Intersection	Wesley & Washington									
Agency/Co.		Jurisdiction	Culver City									
Date Performed	4/29/2016	East/West Street	Washington Bl									
Analysis Year	2016	North/South Street	Wesley St									
Time Analyzed	AM Peak Hour	Peak Hour Factor	0.87									
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25									
Project Description	Existing + Project											



### **Vehicle Volumes and Adjustments**

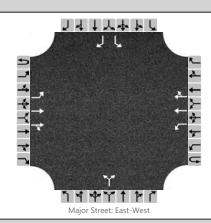
Approach		Eastbound				Westbound		Northbound				Southbound				
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	1	2	0	0	1	2	0		0	0	0		1	0	1
Configuration		L	Т	TR		L	Т	TR			LR			L		R
Volume (veh/h)		0	712	20		11	1570	0		2		5		0		0
Percent Heavy Vehicles		3				3				3		3		3		3
Proportion Time Blocked																
Right Turn Channelized		Ν	lo			Ν	10			N	О			Ν	lo	
Median Type								Undi	vided							

# **Delay, Queue Length, and Level of Service**

Median Storage

Flow Rate (veh/h)			13				8			
Capacity	333		784				214		23	279
v/c Ratio			0.02				0.04			
95% Queue Length			0.1				0.1			
Control Delay (s/veh)	15.8		9.7				22.5		162.6	17.9
Level of Service (LOS)	С		А				С		F	С
Approach Delay (s/veh)			0.	.1		22	2.5			
Approach LOS						(	2			

HCS 2010 Two-Way Stop Control Summary Report											
General Information		Site Information									
Analyst	Raju Associates	Intersection	Wesley & Washington								
Agency/Co.		Jurisdiction	Culver City								
Date Performed	4/29/2016	East/West Street	Washington BI								
Analysis Year	2016	North/South Street	Wesley St								
Time Analyzed	PM Peak Hour	Peak Hour Factor	0.93								
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25								
Project Description	Existing + Project										



### **Vehicle Volumes and Adjustments**

Approach		Eastbound Westbound						Northbound				Southbound					
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R	
Priority	10	1	2	3	4U	4	5	6		7	8	9		10	11	12	
Number of Lanes	0	1	2	0	0	1	2	0		0	0	0		1	0	1	
Configuration		L	Т	TR		L	Т	TR			LR			L		R	
Volume (veh/h)		0	1375	3		5	1019	0		7		10		0		0	
Percent Heavy Vehicles		3				3				3		3		3		3	
Proportion Time Blocked																	
Right Turn Channelized		N	lo			Ν	lo			N	О			N	lo		
Median Type	Undivided																

# Delay, Queue Length, and Level of Service

Median Storage

Flow Rate (veh/h)			5				19			
Capacity	627		446				96		46	478
v/c Ratio			0.01				0.20			
95% Queue Length			0.0				0.7			
Control Delay (s/veh)	10.7		13.2				51.4		83.5	12.5
Level of Service (LOS)	В		В				F		F	В
Approach Delay (s/veh)			0	.1		51	4			
Approach LOS						ı	=			

**INT # 25** 

North/South Street: WESLEY STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

Thru Lane:	1200 vph	N-S Split Phase :	N
Left-Turn Lane:	1200 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR										
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS					
Southbound	RT	0.00	0	0	0.000	N-S(1):	0.000					
	TH	0.00	0	0	0.000 *	N-S(2):	0.006 *					
	LT	0.00	0	0	0.000	E-W(1):	0.314					
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.654 *					
	TH	2.00	1,570	2,400	0.654 *							
	LT	1.00	11	1,200	0.009	V/C:	0.660					
Northbound	RT	0.71	5	857	0.000	Lost Time:	0.100					
	TH	0.00	0	0	0.000	ATSAC:	0.000					
	LT	0.29	2	343	0.006 *							
Eastbound	RT	0.00	20	0	0.000	ICU:	0.760					
	TH	2.00	712	2,400	0.305							
	LT	0.00	0	0	0.000 *	LOS:	С					
Dook Dowlad	DM DEAK I	IOLID										
Peak Period:	PM PEAK H		Volumo	Capacity	V/C	I ICH ANA	ı vele					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA						
	Movement RT	Lanes 0.00	0	0	0.000	N-S(1):	0.007					
Approach	Movement RT TH	0.00 0.00	0 0	0	0.000 0.000 *	N-S(1): N-S(2):	0.007 0.014 *					
Approach Southbound	Movement RT TH LT	0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000	N-S(1): N-S(2): E-W(1):	0.007 0.014 * 0.578 *					
Approach	Movement RT TH LT RT	0.00 0.00 0.00 0.00	0 0 0	0 0 0	0.000 0.000 * 0.000 0.000	N-S(1): N-S(2):	0.007 0.014 *					
Approach Southbound	Movement RT TH LT RT TH	0.00 0.00 0.00 0.00 0.00 2.00	0 0 0 0 1,019	0 0 0 0 0 2,400	0.000 0.000 * 0.000 0.000 0.425	N-S(1): N-S(2): E-W(1): E-W(2):	0.007 0.014 * 0.578 * 0.425					
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00	0 0 0 0 1,019 5	0 0 0 0 2,400 1,200	0.000 0.000 * 0.000 0.000 0.425 0.004 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.007 0.014 * 0.578 * 0.425					
Approach Southbound	Movement RT TH LT RT TH	0.00 0.00 0.00 0.00 0.00 2.00	0 0 0 0 1,019	0 0 0 0 0 2,400	0.000 0.000 * 0.000 0.000 0.425	N-S(1): N-S(2): E-W(1): E-W(2):	0.007 0.014 * 0.578 * 0.425					
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.59	0 0 0 0 1,019 5	0 0 0 0 2,400 1,200 706	0.000 0.000 * 0.000 0.000 0.425 0.004 * 0.007 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.007 0.014 * 0.578 * 0.425 0.592 0.100					
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.59 0.00	0 0 0 1,019 5 10	0 0 0 0 2,400 1,200 706 0	0.000 0.000 * 0.000 0.000 0.425 0.004 * 0.007	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.007 0.014 * 0.578 * 0.425 0.592 0.100					
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT TH LT TH	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.59 0.00 0.41	0 0 0 1,019 5 10 0	0 0 0 0 2,400 1,200 706 0 494	0.000 0.000 * 0.000 0.000 0.425 0.004 * 0.007 0.000 0.014 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.007 0.014 * 0.578 * 0.425 0.592 0.100 0.000					
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT RT TH LT RT TH LT RT TH LT RT	Lanes 0.00 0.00 0.00 0.00 2.00 1.00 0.59 0.00 0.41 0.00	0 0 0 1,019 5 10 0 7	0 0 0 0 2,400 1,200 706 0 494	0.000 0.000 * 0.000 0.000 0.425 0.004 * 0.007 0.000 0.014 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.007 0.014 * 0.578 * 0.425 0.592 0.100 0.000					

Unsignalized intersection.

^{* =} Critical Movement

**INT # 25** 

North/South Street: WESLEY STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	N
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period: AM PEAK HOUR											
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS				
Southbound	RT	1.00	0	1,600	0.000	N-S(1):	0.034 *				
	TH	0.00	0	0	0.000	N-S(2):	0.000				
	LT	1.00	0	1,600	0.000 *	E-W(1):	0.289				
Westbound	RT	0.00	34	0	0.000	E-W(2):	0.594 *				
	TH	2.00	1,689	3,200	0.538 *						
	LT	1.00	33	1,600	0.021	V/C:	0.628				
Northbound	RT	0.33	18	524	0.000	Lost Time:	0.100				
	TH	0.00	0	0	0.000	ATSAC:	-0.070				
	LT	0.67	37	1,076	0.034 *						
Eastbound	RT	0.00	47	0	0.000	ICU:	0.658				
	TH	2.00	811	3,200	0.268						
	LT	1.00	89	1,600	0.056 *	LOS:	В				
Peak Period:	PM PEAK H			_							
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA					
Southbound	RT	1.00	71	1,600	0.044 *	N-S(1):	0.102 *				
	TH	0.00	0	0	0.000	N-S(2):	0.000				
	LT	1.00	21	1,600	0.013	E-W(1):	0.533 *				
Westbound	RT	0.00	0	0	0.000	E-W(2):	0.350				
	TH	2.00	1,121	3,200	0.350						
	LT	1.00	50	1,600	0.031 *	V/C:	0.635				
Northbound	RT	0.39	36	619	0.000	Lost Time:	0.100				
	TH	0.00	0	0	0.000	ATSAC:	-0.070				
	LT	0.61	57	981	0.058 *						
Eastbound		0.00	45	0	0.000	ICU:	0.665				
Lasibouria	RT	0.00	43	U	0.000	100.	0.000				
Lasibound	TH	2.00	1,560	3,200	0.502 *	100.	0.000				

Traffic signals in Culver City have advanced traffic signal synchronization equivalent to ATSAC.

^{* =} Critical Movement

**INT # 25** 

North/South Street: WESLEY STREET

East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

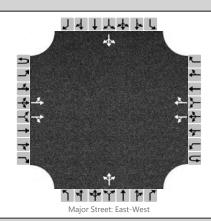
Thru Lane:	1600 vph	N-S Split Phase :	Υ
Left-Turn Lane:	1600 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK I	HOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	1.00	0	1,600	0.000	N-S(1):	0.034 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
	LT	1.00	0	1,600	0.000 *	E-W(1):	0.290
Westbound	RT	0.00	34	0	0.000	E-W(2):	0.599 *
	TH	2.00	1,704	3,200	0.543 *		
	LT	1.00	33	1,600	0.021	V/C:	0.633
Northbound	RT	0.33	18	524	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
	LT	0.67	37	1,076	0.034 *		
Eastbound	RT	0.00	47	0	0.000	ICU:	0.663
	TH	2.00	814	3,200	0.269		
	LT	1.00	89	1,600	0.056 *	LOS:	В
		10115					
Peak Period:	PM PEAK H		\/ali vaa	O a m a aith i	V/C	IOLI ANIA	1.1/010
Approach	Movement	Lanes	Volume	Capacity	_	ICU ANA	
Southbound	RT	1.00	71	1,600	0.044 *	N-S(1):	0.102 *
	TH	0.00	0	0	0.000	N-S(2):	0.000
Ma ath a cad	LT	1.00	21 0	1,600 0	0.013	E-W(1):	0.538 *
Westbound	RT	0.00		ľ	0.000	E-W(2):	0.352
	TH	2.00	1,127	3,200	0.352	\//O	0.040
N. (1.1	LT	1.00	50	1,600	0.031 *	V/C:	0.640
Northbound	RT	0.39	36	619	0.000	Lost Time:	0.100
	TH	0.00	0	0	0.000	ATSAC:	-0.070
		0.61	57	981	0.058 *		
	LT			_			
Eastbound	RT	0.00	45	0	0.000	ICU:	0.670
Eastbound	<u> </u>			0 3,200 1,600	0.000 0.507 * 0.000	ICU: LOS:	0.670 B

Traffic signals in Culver City have advanced traffic signal synchronization equivalent to ATSAC.

^{* =} Critical Movement

	HCS 2010 Two-Way Stop Control Summary Report										
General Information		Site Information									
Analyst	Raju Associates	Intersection	Cattaraugus & Washington								
Agency/Co.		Jurisdiction	Culver City								
Date Performed	3/29/2016	East/West Street	Washington Bl								
Analysis Year	2016	North/South Street	Cattaraugus Ave								
Time Analyzed	AM Peak Hour	Peak Hour Factor	0.95								
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25								
Project Description	Existing 2016										



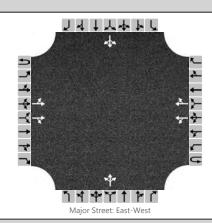
### **Vehicle Volumes and Adjustments**

Approach	Eastbound			Westbound				Northbound				Southbound				
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	10	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		42	713	11		14	1357	360		3	9	8		52	2	68
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized	No				No				No				No			
Median Type	Left Only															
Median Storage		1														

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	420			729					20			129	
Capacity	333			839					47			137	
v/c Ratio	1.26			0.87					0.43			0.94	
95% Queue Length	0.5			0.1					1.5			6.5	
Control Delay (s/veh)	17.5			9.4					130.7			124.5	
Level of Service (LOS)	С			А					F			F	
Approach Delay (s/veh)	2	.6				130.7			124.5				
Approach LOS								F			ı	F	

HCS 2010 Two-Way Stop Control Summary Report									
General Information		Site Information							
Analyst	Raju Associates	Intersection	Cattaraugus & Washington						
Agency/Co.		Jurisdiction	Culver City						
Date Performed	3/29/2016	East/West Street	Washington Bl						
Analysis Year	2016	North/South Street	Cattaraugus Ave						
Time Analyzed	PM Peak Hour	Peak Hour Factor	0.98						
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25						
Project Description	Existing 2016								



### **Vehicle Volumes and Adjustments**

Approach	Eastbound				Westbound				Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	10	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		38	1205	23		7	683	53		5	0	4		94	2	54
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized	No				No				No				No			
Median Type	Left Only															
Median Storage	1															

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)		654				356					9			153	
Capacity		848				546					167			243	
v/c Ratio		0.77				0.65					0.05			0.63	
95% Queue Length		0.1				0.0					0.2			3.8	
Control Delay (s/veh)		9.5				11.7					27.8			41.9	
Level of Service (LOS)		А				В					D			E	
Approach Delay (s/veh)		0	.9		0.2			27.8			41.9				
Approach LOS										)					

**INT # 26** 

North/South Street: CATTARAUGUS AVENUE East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) CONDITIONS

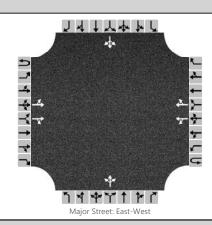
Thru Lane:	1200 vph	N-S Split Phase :	N
Left-Turn Lane:	1200 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	68	0	0.000	N-S(1):	0.060
	TH	1.00	2	1,200	0.102 *	N-S(2):	0.105 *
	LT	0.00	52	1,200	0.043	E-W(1):	0.331
Westbound	RT	0.00	360	0	0.000	E-W(2):	0.756 *
	TH	2.00	1,357	2,400	0.721 *		
	LT	0.00	14	1,200	0.012	V/C:	0.861
Northbound	RT	0.00	8	0	0.000	Lost Time:	0.100
	TH	1.00	9	1,200	0.017	ATSAC:	0.000
	LT	0.00	3	1,200	0.003 *		
Eastbound	RT	0.00	11	0	0.000	ICU:	0.961
	TH	2.00	713	2,400	0.319		
	LT	0.00	42	1,200	0.035 *	LOS:	E
Dook Doriods	DM DEAK I	IOLID					
Peak Period: Approach	PM PEAK F	Lanes	Volume	Capacity	V/C	ICU ANA	I VCIC
Southbound	RT	0.00	54	Оараспу	0.000	N-S(1):	0.086
Southbound	TH	1.00	2	1,200	0.000 0.125 *	N-S(1). N-S(2):	0.000
	LT	0.00	94	1,200	0.125	E-W(1):	0.129
Westbound	RT	0.00	53	0	0.000	E-W(1):	0.342
vvestbound	TH	2.00	683	2,400	0.310	L-VV(Z).	0.542
	LT	0.00	7	1,200	0.006 *	V/C:	0.663
Northbound	RT	0.00	4	0	0.000	Lost Time:	0.100
INOLLIBOULIU	TH	1.00	0	1,200	0.008	ATSAC:	0.000
	LT	0.00	5	1,200	0.008	A10A0.	0.000
Eastbound	RT	0.00	23	0	0.000	ICU:	0.763
Lastbouria	TH	2.00	1,205	2,400	0.528 *	100.	0.700
	LT	0.00	38	1,200	0.032	LOS:	С

Unsignalized intersection.

^{* =} Critical Movement

	HCS 2010 Two-Way Stop C	ontrol Summary Re	eport
General Information		Site Information	
Analyst	Raju Associates	Intersection	Cattaraugus & Washington
Agency/Co.		Jurisdiction	Culver City
Date Performed	4/29/2016	East/West Street	Washington Bl
Analysis Year	2016	North/South Street	Cattaraugus Ave
Time Analyzed	AM Peak Hour	Peak Hour Factor	0.95
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description	Existing + Project		



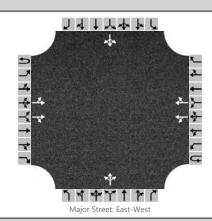
## **Vehicle Volumes and Adjustments**

Approach		Eastb	ound			Westl	oound		Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		42	716	11		14	1372	360		3	9	8		52	2	68
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized		N	lo			Ν	lo			Ν	lo			Ν	lo	
Median Type		·						Left	Only							
Median Storage	1															

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	421			737			20			129	
Capacity	328			837			43			129	
v/c Ratio	1.28			0.88			0.46			1.00	
95% Queue Length	0.5			0.1			1.6			6.9	
Control Delay (s/veh)	17.7			9.4			145.9			143.8	
Level of Service (LOS)	С			А			F			F	
Approach Delay (s/veh)	2	.7				14	5.9		14	3.8	
Approach LOS						ı	=		ı	=	

	HCS 2010 Two-Way Stop C	ontrol Summary Re	eport
General Information		Site Information	
Analyst	Raju Associates	Intersection	Cattaraugus & Washington
Agency/Co.		Jurisdiction	Culver City
Date Performed	4/29/2016	East/West Street	Washington Bl
Analysis Year	2016	North/South Street	Cattaraugus Ave
Time Analyzed	PM Peak Hour	Peak Hour Factor	0.98
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description	Existing + Project		



### **Vehicle Volumes and Adjustments**

Approach		Eastb	ound			Westl	oound		Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	10	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		38	1221	23		7	689	53		5	0	4		94	2	54
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized		Ν	lo			Ν	lo			Ν	lo			Ν	lo	
Median Type								Left	Only							
Median Storage									1							

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	662			359				9			153	
Capacity	843			538				163			239	
v/c Ratio	0.78			0.67				0.06			0.64	
95% Queue Length	0.1			0.0				0.2			3.9	
Control Delay (s/veh)	9.5			11.8				28.4			43.4	
Level of Service (LOS)	А			В				D			E	
Approach Delay (s/veh)	1	.0		0.	.2		28	.4		43	3.4	
Approach LOS							С	)				

**INT # 26** 

North/South Street: CATTARAUGUS AVENUE East/West Street: WASHINGTON BOULEVARD

Scenario: EXISTING (2016) PLUS PROJECT CONDITIONS

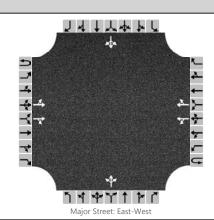
Thru Lane:	1200 vph	N-S Split Phase :	N
Left-Turn Lane:	1200 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	68	0	0.000	N-S(1):	0.060
	TH	1.00	2	1,200	0.102 *	N-S(2):	0.105 *
	LT	0.00	52	1,200	0.043	E-W(1):	0.332
Westbound	RT	0.00	360	0	0.000	E-W(2):	0.763 *
	TH	2.00	1,372	2,400	0.728 *		
	LT	0.00	14	1,200	0.012	V/C:	0.868
Northbound	RT	0.00	8	0	0.000	Lost Time:	0.100
	TH	1.00	9	1,200	0.017	ATSAC:	0.000
	LT	0.00	3	1,200	0.003 *		
Eastbound	RT	0.00	11	0	0.000	ICU:	0.968
	TH	2.00	716	2,400	0.320		
	LT	0.00	42	1,200	0.035 *	LOS:	E
Peak Period:	PM PEAK H						
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	
	Movement RT	Lanes 0.00	54	0	0.000	N-S(1):	0.086
Approach	Movement RT TH	Lanes 0.00 1.00	54 2	0 1,200	0.000 0.125 *	N-S(1): N-S(2):	0.086 0.129 *
Approach Southbound	Movement RT TH LT	Lanes 0.00 1.00 0.00	54 2 94	0 1,200 1,200	0.000 0.125 * 0.078	N-S(1): N-S(2): E-W(1):	0.086 0.129 * 0.540 *
Approach	Movement RT TH LT RT	Lanes 0.00 1.00 0.00	54 2 94 53	0 1,200 1,200 0	0.000 0.125 * 0.078 0.000	N-S(1): N-S(2):	0.086 0.129 *
Approach Southbound	Movement RT TH LT RT RT TH	Lanes 0.00 1.00 0.00 0.00 2.00	54 2 94 53 689	0 1,200 1,200 0 2,400	0.000 0.125 * 0.078 0.000 0.312	N-S(1): N-S(2): E-W(1): E-W(2):	0.086 0.129 * 0.540 * 0.344
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH	Lanes 0.00 1.00 0.00 0.00 2.00 0.00	54 2 94 53 689 7	0 1,200 1,200 0 2,400 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 *	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.086 0.129 * 0.540 * 0.344 0.669
Approach Southbound	Movement RT TH LT RT TH LT TH LT TH LT RT	Lanes 0.00 1.00 0.00 0.00 2.00	54 2 94 53 689	0 1,200 1,200 0 2,400 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 * 0.000	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.086 0.129 * 0.540 * 0.344 0.669 0.100
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT TH LT RT TH	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00 1	54 2 94 53 689 7 4	0 1,200 1,200 0 2,400 1,200 0 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 * 0.000 0.008	N-S(1): N-S(2): E-W(1): E-W(2): V/C:	0.086 0.129 * 0.540 * 0.344 0.669
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT TH	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00 0.00	54 2 94 53 689 7 4 0	0 1,200 1,200 0 2,400 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 * 0.000 0.008 0.004 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.086 0.129 * 0.540 * 0.344 0.669 0.100 0.000
Approach Southbound Westbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT RT	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00 1	54 2 94 53 689 7 4	0 1,200 1,200 0 2,400 1,200 0 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 * 0.000 0.008	N-S(1): N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.086 0.129 * 0.540 * 0.344 0.669 0.100
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT TH	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00 0.00	54 2 94 53 689 7 4 0	0 1,200 1,200 0 2,400 1,200 0 1,200 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 * 0.000 0.008 0.004 *	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.086 0.129 * 0.540 * 0.344 0.669 0.100 0.000
Approach Southbound Westbound Northbound	Movement RT TH LT RT TH LT TH LT TH LT RT TH LT RT TH LT RT	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00 0.00 0	54 2 94 53 689 7 4 0 5	0 1,200 1,200 0 2,400 1,200 0 1,200 1,200	0.000 0.125 * 0.078 0.000 0.312 0.006 * 0.000 0.008 0.004 * 0.000	N-S(1):     N-S(2):     E-W(1):     E-W(2):     V/C:     Lost Time:     ATSAC:	0.086 0.129 * 0.540 * 0.344 0.669 0.100 0.000

Unsignalized intersection.

^{* =} Critical Movement

	HCS 2010 Two-Way Stop C	ontrol Summary Re	eport
General Information		Site Information	
Analyst	Raju Associates	Intersection	Cattaraugus & Washington
Agency/Co.		Jurisdiction	Culver City
Date Performed	1/24/2017	East/West Street	Washington Bl
Analysis Year	2018	North/South Street	Cattaraugus Ave
Time Analyzed	AM Peak Hour	Peak Hour Factor	0.95
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description	Cumulative Base		



Vehicle Volumes and Adjustments

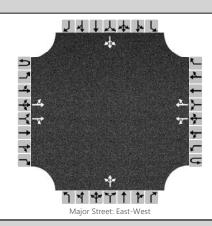
Approach		Eastb	ound			Westl	oound		Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		71	799	11		14	1530	367		3	9	8		53	2	82
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized		Ν	lo			Ν	lo			N	О			Ν	lo	
Median Type		L						Left	Only							
Median Storage									1							

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	496			821			20		144	
Capacity	280			776			15			
v/c Ratio	1.77			1.06			1.35			
95% Queue Length	1.1			0.1			3.1			
Control Delay (s/veh)	22.5			9.7			719.3			
Level of Service (LOS)	С			А			F			
Approach Delay (s/veh)	6	.2				71	9.3			
Approach LOS						ı	=			

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HCS 2010 Two-Way Stop Control Summary Report											
General Information		Site Information									
Analyst	Raju Associates	Intersection	Cattaraugus & Washington								
Agency/Co.		Jurisdiction	Culver City								
Date Performed	1/24/2017	East/West Street	Washington Bl								
Analysis Year	2018	North/South Street	Cattaraugus Ave								
Time Analyzed	PM Peak Hour	Peak Hour Factor	0.98								
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25								
Project Description	Cumulative Base										



Approach	Eastbound V						Westbound				Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R		
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12		
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0		
Configuration		LT		TR		LT		TR			LTR				LTR			
Volume (veh/h)		88	1401	23		7	811	54		5	0	4		96	2	68		
Percent Heavy Vehicles		3				3				3	3	3		3	3	3		
Proportion Time Blocked																		
Right Turn Channelized		Ν	lo			Ν	lo			Ν	lo		No					
Median Type	Let							Left	Left Only									
Median Storage	1																	

### Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	805			421				9			169	
Capacity	756			457				57			108	
v/c Ratio	1.07			0.92				0.16			1.56	
95% Queue Length	0.4			0.0				0.5			12.6	
Control Delay (s/veh)	10.4			13.0				79.8			362.8	
Level of Service (LOS)	В			В				F			F	
Approach Delay (s/veh)		3.3		0	.3		79	9.8		36	2.8	
Approach LOS								F		ſ	F	

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**INT # 26** 

North/South Street: CATTARAUGUS AVENUE East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) BASE CONDITIONS

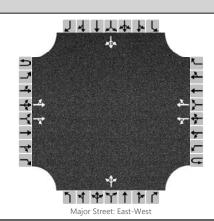
Thru Lane:	1200 vph	N-S Split Phase :	N
Left-Turn Lane:	1200 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

AMBEAKI	IOLID					
		Valuma	Conceity	VIC	ICLLANIA	I VOIC
		_	•		, ,	0.061
			,	_		0.117 *
			,		` '	0.379
			•		E-W(2):	0.855 *
		1,530	2,400	0.796 *		
	0.00	14	1,200	0.012	V/C:	0.972
RT	0.00	8	0	0.000	Lost Time:	0.100
TH	1.00	9	1,200	0.017	ATSAC:	0.000
LT	0.00	3	1,200	0.003 *		
RT	0.00	11	0	0.000	ICU:	1.072
TH	2.00	799	2,400	0.367		
LT	0.00	71	1,200	0.059 *	LOS:	F
	IOUR					
	Lanes					
l RT	0.00	68	0	0.000	NI 0 (4)	
	0.00	00	•		N-S(1):	0.088
TH	1.00	2	1,200	0.000	N-S(1): N-S(2):	0.088 0.142 *
			•		` ,	
TH	1.00	2	1,200	0.138 *	N-S(2):	0.142 *
TH LT	1.00 0.00	2 96	1,200 1,200	0.138 * 0.080	N-S(2): E-W(1):	0.142 * 0.636 *
TH LT RT	1.00 0.00 0.00	2 96 54	1,200 1,200 0	0.138 * 0.080 0.000	N-S(2): E-W(1):	0.142 * 0.636 *
TH LT RT TH	1.00 0.00 0.00 2.00	2 96 54 811	1,200 1,200 0 2,400	0.138 * 0.080 0.000 0.363	N-S(2): E-W(1): E-W(2):	0.142 * 0.636 * 0.436
TH LT RT TH LT	1.00 0.00 0.00 2.00 0.00	2 96 54 811 7	1,200 1,200 0 2,400 1,200	0.138 * 0.080 0.000 0.363 0.006 *	N-S(2): E-W(1): E-W(2): V/C:	0.142 * 0.636 * 0.436 0.778
TH LT RT TH LT	1.00 0.00 0.00 2.00 0.00 0.00	2 96 54 811 7 4	1,200 1,200 0 2,400 1,200	0.138 * 0.080 0.000 0.363 0.006 * 0.000	N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.142 * 0.636 * 0.436 0.778 0.100
TH LT RT TH LT RT TH	1.00 0.00 0.00 2.00 0.00 0.00 1.00	2 96 54 811 7 4	1,200 1,200 0 2,400 1,200 0 1,200	0.138 * 0.080 0.000 0.363 0.006 * 0.000 0.008	N-S(2): E-W(1): E-W(2): V/C: Lost Time:	0.142 * 0.636 * 0.436 0.778 0.100
TH LT RT TH LT RT TH LT	1.00 0.00 0.00 2.00 0.00 0.00 1.00 0.00	2 96 54 811 7 4 0	1,200 1,200 0 2,400 1,200 0 1,200 1,200	0.138 * 0.080 0.000 0.363 0.006 * 0.000 0.008 0.004 *	N-S(2): E-W(1): E-W(2): V/C: Lost Time: ATSAC:	0.142 * 0.636 * 0.436 0.778 0.100 0.000
	Movement RT TH LT RT TH LT RT TH LT RT TH LT TH LT TH LT	RT	Movement         Lanes         Volume           RT         0.00         82           TH         1.00         2           LT         0.00         53           RT         0.00         367           TH         2.00         1,530           LT         0.00         14           RT         0.00         8           TH         1.00         9           LT         0.00         3           RT         0.00         11           TH         2.00         799           LT         0.00         71    PM PEAK HOUR  Movement Lanes Volume	Movement         Lanes         Volume         Capacity           RT         0.00         82         0           TH         1.00         2         1,200           LT         0.00         53         1,200           RT         0.00         367         0           TH         2.00         1,530         2,400           LT         0.00         14         1,200           RT         0.00         8         0           TH         1.00         9         1,200           LT         0.00         3         1,200           RT         0.00         11         0           TH         2.00         799         2,400           LT         0.00         71         1,200    PM PEAK HOUR  Movement Lanes Volume Capacity	Movement         Lanes         Volume         Capacity         V/C           RT         0.00         82         0         0.000           TH         1.00         2         1,200         0.114 *           LT         0.00         53         1,200         0.044           RT         0.00         367         0         0.000           TH         2.00         1,530         2,400         0.796 *           LT         0.00         14         1,200         0.012           RT         0.00         8         0         0.000           TH         1.00         9         1,200         0.017           LT         0.00         3         1,200         0.003 *           RT         0.00         11         0         0.000           TH         2.00         799         2,400         0.367           LT         0.00         71         1,200         0.059 *    PM PEAK HOUR  Movement Lanes Volume Capacity V/C	Movement         Lanes         Volume         Capacity         V/C         ICU ANA           RT         0.00         82         0         0.000         N-S(1):           TH         1.00         2         1,200         0.114 *         N-S(2):           LT         0.00         53         1,200         0.044         E-W(1):           RT         0.00         367         0         0.000         E-W(2):           TH         2.00         1,530         2,400         0.796 *         V/C:           LT         0.00         14         1,200         0.012         V/C:           RT         0.00         8         0         0.000         Lost Time:           TH         1.00         9         1,200         0.017         ATSAC:           LT         0.00         3         1,200         0.003 *         ICU:           TH         2.00         799         2,400         0.367         LOS:           PM PEAK HOUR           Movement         Lanes         Volume         Capacity         V/C         ICU ANA

Unsignalized intersection.

^{* =} Critical Movement

	HCS 2010 Two-Way Stop Control Summary Report												
General Information		Site Information											
Analyst	Raju Associates	Intersection	Cattaraugus & Washington										
Agency/Co.		Jurisdiction	Culver City										
Date Performed	1/24/2017	East/West Street	Washington Bl										
Analysis Year	2018	North/South Street	Cattaraugus Ave										
Time Analyzed	AM Peak Hour	Peak Hour Factor	0.95										
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25										
Project Description	Cumulative + Project												



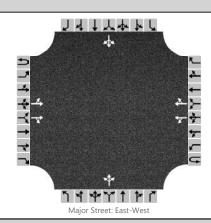
Vehicle Volumes and Adjustments

Approach		Eastb	ound			Westl	oound		Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		71	802	11		14	1545	367		3	9	8		53	2	82
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized		Ν	lo			Ν	lo			N	lo		No			
Median Type								Left	Only							
Median Storage									1							

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	497			828			20		144	
Capacity	276			774			14			
v/c Ratio	1.80			1.07			1.42			
95% Queue Length	1.1			0.1			3.1			
Control Delay (s/veh)	22.8			9.7			770.3			
Level of Service (LOS)	С			А			F			
Approach Delay (s/veh)	6	5.4				77	0.3			
Approach LOS							F			

	HCS 2010 Two-Way Stop Control Summary Report												
General Information		Site Information											
Analyst	Raju Associates	Intersection	Cattaraugus & Washington										
Agency/Co.		Jurisdiction	Culver City										
Date Performed	1/24/2017	East/West Street	Washington Bl										
Analysis Year	2018	North/South Street	Cattaraugus Ave										
Time Analyzed	PM Peak Hour	Peak Hour Factor	0.98										
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25										
Project Description	Cumulative + Project												



### **Vehicle Volumes and Adjustments**

Approach		Eastb	ound			Westl	oound		Northbound				Southbound			
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	0	2	0	0	0	2	0		0	1	0		0	1	0
Configuration		LT		TR		LT		TR			LTR				LTR	
Volume (veh/h)		88	1417	23		7	817	54		5	0	4		96	2	68
Percent Heavy Vehicles		3				3				3	3	3		3	3	3
Proportion Time Blocked																
Right Turn Channelized		Ν	lo			Ν	lo			N	lo		No			
Median Type					Left Only											
Median Storage									1							

## Delay, Queue Length, and Level of Service

Flow Rate (veh/h)	813			424				9			169	
Capacity	752			450				51			99	
v/c Ratio	1.08			0.94				0.18			1.71	
95% Queue Length	0.4			0.0				0.6			13.5	
Control Delay (s/veh)	10.4			13.1				90.0			433.8	
Level of Service (LOS)	В			В				F			F	
Approach Delay (s/veh)	3.4	4		0	.3		90	0.0		433	3.8	
Approach LOS							ı	•		F		

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**INT # 26** 

North/South Street: CATTARAUGUS AVENUE East/West Street: WASHINGTON BOULEVARD

Scenario: CUMULATIVE (2018) PLUS PROJECT CONDITIONS

Thru Lane:	1200 vph	N-S Split Phase :	N
Left-Turn Lane:	1200 vph	E-W Split Phase :	Ν
Dual LT Penalty:	10 %	Lost Time (% of cycle):	10

Peak Period:	AM PEAK H	IOUR					
Approach	Movement	Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
Southbound	RT	0.00	82	0	0.000	N-S(1):	0.061
	TH	1.00	2	1,200	0.114 *	N-S(2):	0.117 *
	LT	0.00	53	1,200	0.044	E-W(1):	0.380
Westbound	RT	0.00	367	0	0.000	E-W(2):	0.862 *
	TH	2.00	1,545	2,400	0.803 *		
	LT	0.00	14	1,200	0.012	V/C:	0.979
Northbound	RT	0.00	8	0	0.000	Lost Time:	0.100
	TH	1.00	9	1,200	0.017	ATSAC:	0.000
	LT	0.00	3	1,200	0.003 *		
Eastbound	RT	0.00	11	0	0.000	ICU:	1.079
	TH	2.00	802	2,400	0.368		
					0.0=0.#		_
	LT	0.00	71	1,200	0.059 *	LOS:	F
Peak Period:	PM PEAK H	IOUR		,			
Approach	PM PEAK H	IOUR Lanes	Volume	Capacity	V/C	ICU ANA	LYSIS
	PM PEAK H Movement RT	Lanes 0.00	Volume 68	Capacity 0	V/C 0.000	ICU ANA N-S(1):	LYSIS 0.088
Approach	PM PEAK H Movement RT TH	Lanes 0.00 1.00	Volume 68 2	Capacity 0 1,200	V/C 0.000 0.138 *	ICU ANA N-S(1): N-S(2):	LYSIS 0.088 0.142 *
Approach Southbound	PM PEAK H  Movement  RT  TH  LT	Lanes 0.00	Volume 68 2 96	Capacity 0 1,200 1,200	V/C 0.000 0.138 * 0.080	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.088 0.142 * 0.643 *
Approach	PM PEAK H Movement RT TH LT RT	Lanes 0.00 1.00 0.00 0.00	Volume 68 2 96 54	Capacity 0 1,200 1,200 0	V/C 0.000 0.138 * 0.080 0.000	ICU ANA N-S(1): N-S(2):	LYSIS 0.088 0.142 *
Approach Southbound	PM PEAK H  Movement  RT  TH  LT	Lanes 0.00 1.00 0.00	Volume 68 2 96	Capacity 0 1,200 1,200	V/C 0.000 0.138 * 0.080	ICU ANA N-S(1): N-S(2): E-W(1):	LYSIS 0.088 0.142 * 0.643 *
Approach Southbound Westbound	PM PEAK H Movement RT TH LT RT	Lanes 0.00 1.00 0.00 0.00	Volume  68 2 96 54 817 7	Capacity 0 1,200 1,200 0	V/C 0.000 0.138 * 0.080 0.000	ICU ANA N-S(1): N-S(2): E-W(1):	0.088 0.142 * 0.643 * 0.439
Approach Southbound	PM PEAK H  Movement  RT  TH  LT  RT  RT  TH	Lanes 0.00 1.00 0.00 0.00 2.00	Volume 68 2 96 54 817	Capacity 0 1,200 1,200 0 2,400	V/C 0.000 0.138 * 0.080 0.000 0.366	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):	0.088 0.142 * 0.643 * 0.439
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT	Lanes 0.00 1.00 0.00 0.00 2.00 0.00	Volume  68 2 96 54 817 7	Capacity 0 1,200 1,200 0 2,400 1,200	V/C 0.000 0.138 * 0.080 0.000 0.366 0.006 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C:	0.088 0.142 * 0.643 * 0.439
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  RT  TH  LT	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00	Volume  68 2 96 54 817 7	Capacity  0 1,200 1,200 0 2,400 1,200 0	V/C 0.000 0.138 * 0.080 0.000 0.366 0.006 * 0.000	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time:	0.088 0.142 * 0.643 * 0.439 0.785 0.100
Approach Southbound Westbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  TH  LT	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00	Volume  68 2 96 54 817 7 4 0	Capacity  0 1,200 1,200 0 2,400 1,200 0 1,200	V/C 0.000 0.138 * 0.080 0.000 0.366 0.006 * 0.000 0.008	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time:	0.088 0.142 * 0.643 * 0.439 0.785 0.100
Approach Southbound Westbound Northbound	PM PEAK H  Movement  RT  TH  LT  RT  TH  LT  RT  TH  LT  TH  LT  RT	Lanes 0.00 1.00 0.00 0.00 2.00 0.00 0.00 1.00 0.00 0	Volume 68 2 96 54 817 7 4 0 5	Capacity  0 1,200 1,200 0 2,400 1,200 0 1,200 1,200 1,200	V/C 0.000 0.138 * 0.080 0.000 0.366 0.006 * 0.000 0.008 0.004 *	ICU ANA N-S(1): N-S(2): E-W(1): E-W(2):  V/C: Lost Time: ATSAC:	0.088 0.142 * 0.643 * 0.439 0.785 0.100 0.000

Unsignalized intersection.

^{* =} Critical Movement

# **APPENDIX E**

**Queuing Analysis** 



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#### **TECHNICAL MEMORANDUM**

**TO:** Ms. Susan Yun, City of Culver City

CC: Mr. Barry Kurtz, City of Culver City

FROM: Srinath Raju, P.E.

Chris Munoz

**SUBJECT:** 8888 Washington Boulevard Project Traffic Study

Queueing Analysis at Project Driveway

**DATE:** February 19, 2017 **REF:** RA491

This memorandum provides a brief description of queueing analysis at the project driveway along Washington Boulevard taking into consideration the automated parking facility and associated infrastructure provided to support the same. The intent of this analysis is to determine the potential, if any, for arriving traffic to queue up within the site and spill over to Washington Boulevard and consequently affect the traffic flow along Washington Boulevard during peak time periods.

#### **Automated Parking Facility Background Information**

A preliminary Parking Operations Plan for the automated parking facility proposed for the Project on-site, has been prepared. Per the parking facility's automated system specifications, the retrieval rate at the proposed facility would range between 65 seconds per vehicle to 150 seconds per vehicle. The retrieval rate is the speed of the system and does not include the time associated with loading, unloading, etc. that would comprise of the overall processing rate.

The processing rate is dependent primarily upon the vertical and horizontal distance a vehicle has to be transported to and from its parking space, whether the space is a tandem space or not, etc. The (non-tandem) spaces closest to the elevator shaft take the least amount of time to process

while those spaces farthest from the elevator shaft take the most amount of time to process. This fact is demonstrated in the Exhibit 1 (also provided in the Parking Operations Plan). Based on the exhibits in the Parking Operations Plan, a processing rate of 90 seconds per vehicle is estimated by the parking operator (CityLift) to be available in the automated parking structure for approximately 50 spaces per level (total of 150 spaces).

#### **Project Driveway Volumes**

The proposed Project's trip generation is provided in Table E-0. From Table E-0, it can be observed that the driveway traffic volumes at the Project Site can be calculated aggregating the inbound traffic generation for each of the three component uses of the proposed Project and then crediting the same for transit trips and internal trip capture. Based on the forecasts developed for the proposed Project, the driveway volumes at the site is estimated to be 102 trips inbound during the morning peak hour.

#### **Queueing Analysis Methodology**

The methodology for queueing analysis involves the following key elements:

- Compile traffic counts conducted at three office sites within the City of Culver City on numerous days including the observed traffic at the driveways to the three sites in 15minute time intervals
- Determine the 15-minute inbound % traffic at each site for all four days based on the observed overall inbound traffic flows during the AM peak hours and identify the maximum 15-minute inbound % traffic among all these data points
- Determine the estimated AM peak hour driveway volumes inbound at the proposed Project site
- Determine the maximum 15-minute traffic volumes at the proposed Project site using the observed maximum 15-minute inbound % from the various office sites in Culver City and the estimated AM peak hour driveway volumes at the proposed Project site
- Calculate the average queue length in the peak 15-minute period during the AM peak hour when inbound traffic would be maximum, based on the processing rate at the proposed automated parking facility

 Compare this average queue length (in number of vehicles) during the peak 15-minute time period to the available storage on site including queue storage and short-term loading spaces provided and determine if the queue length exceeds the queue storage

#### **Queueing Analysis**

A queueing analysis of trips inbound to the Project Site during the morning peak hour when maximum number of inbound vehicular traffic is anticipated, was conducted using the methodology noted above to assess the potential of vehicles queueing in the driveway aisle within the Project Site beyond the access driveway and spilling over on to the external street system (Washington Boulevard).

Table E-1 summarizes the analysis of inbound traffic within the AM peak hours to determine the average 15-minute arrival %, 90th-percentile 15-minute arrival % and the maximum 15-minute arrival %. It can be observed that the average 15-minute arrival % is 32%, 90th percentile 15-minute arrival % is 36.1%, and the maximum 15-minute arrival % is 41%. For the purposes of this queueing analysis, the maximum 15-minute arrival % of 41% has been chosen.

Table E-2 details the maximum queueing analysis at the Project driveway. This table provides the total inbound traffic at the proposed Project driveway during the AM peak hour, the maximum estimated number of proposed Project arrivals in the peak 15-minute interval, service volume processed in the automated parking facility's four elevators, average queue length in the maximum 15-minute period in number of vehicles, available storage on site and whether the queue length would be such that it would extend to Washington Boulevard.

Based on the queueing analysis, it can be observed that during the peak times of the morning peak hour, a maximum total of 42 vehicles would arrive within a peak 15-minute period. Based on the parking operator's estimated processing rate of the system (including all-day valet services) of 90 seconds per vehicle, a total of 40 vehicles within the same time period can be processed by the system with all four operating vehicular elevators. A maximum queue of 2 vehicles would remain on site. The maximum available storage on-site, based on the Site Plan, is 10 vehicles in the queue plus four (4) short-term loading spaces and one (1) ADA parking space. Therefore,

there would not be any queueing vehicles that would extend beyond the site on to the external roadway system (Washington Boulevard) assuming the maximum peaking characteristics of the arriving vehicles in the morning peak hour. Consequently, the traffic flow along Washington Boulevard would not be affected by inbound vehicles extending out of the Project driveway.

Per City of Culver City's request, a queueing analysis with three of the four parking elevators being available during the morning peak conditions was conducted. With the estimated processed rate of the system (with 3 of the 4 elevators available) with all day valet services at 90 seconds per vehicle, a total of 30 vehicles (3600 / 4 (in 15-minutes) / 90 seconds per vehicle * 3 elevators) can be processed by the system within the same peak 15-minute interval. Using a maximum arrival of a total of 42 vehicles within the peak 15-minute period, a maximum queue of 12 vehicles is anticipated. Again, the maximum available storage on-site, based on the Site Plan, is 10 vehicles in the storage lane on site plus four (4) short-term loading spaces and one (1) ADA parking space for a total of 14 to 15 vehicles that can be stored on site. Therefore, there would still not be any queueing vehicles that would extend beyond the site on to the external roadway system (Washington Boulevard) assuming the maximum peaking characteristics of the arriving vehicles in the morning peak hour and 3 of the 4 parking elevators available during that same time period. Consequently, the traffic flow along Washington Boulevard would not be affected by inbound vehicles extending out of the Project driveway even with 3 of the 4 parking elevators available during the peak time period in the AM peak hour.

RAJU Associates, Inc.

#### TABLE E-0 ESTIMATED PROJECT TRIP GENERATION

			Α	M Peak Ho	ur	PM Peak Hour			
	Size	Daily	IN	OUT	TOTAL	IN	OUT	TOTAL	
Proposed Project									
Office Transit *  *Internal Capture (10)	59,325 s.f.	883	111	15	126	25	120	145	
	Trip Use (25%)	(221)	(28)	(4)	(32)	(6)	(30)	(36)	
	0%) Trip Credit	(66)	(8)	(1)	(9)	(2)	(9)	(11)	
Retail 2,878 s.f. Internal Capture (10%) Trip Credit **Pass-By Trip Reduction (25%)		677	11	7	18	27	29	56	
		(68)	(1)	(1)	(2)	(3)	(3)	(6)	
		(152)	(3)	(1)	(4)	(6)	(7)	(13)	
High-Turnover Restaurant	405	19	15	34	19	12	31		
Internal Capture (10	(41)	(2)	(1)	(3)	(2)	(1)	(3)		
**Pass-By Trip Re	(91)	(4)	(4)	(8)	(4)	(3)	(7)		
Existing Uses (to be removed)	Existing Uses (to be removed)								
Auto Repair Shop	200	15	7	22	17	19	36		
Pass-By Trip Re	(20)	(2)	0	(2)	(2)	(2)	(4)		
Project Net Trip Ge	1,146	82	18	100	33	91	124		
Trip Generation Rates [1] Office (ITE Land Use 710) Retail/Shopping Center (ITE Land Use 820) High-Turnover Restaurant (ITE Land Use 932) Automobile Care Center (ITE Land Use 942) Trips per 1,00		[2]	88%	12%	[2]	17%	83%	[2]	
		[3]	62%	38%	[3]	48%	52%	[3]	
		127.15	55%	45%	10.81	60%	40%	9.85	
		20.00 [4]	66%	34%	2.25	48%	52%	[5]	

^{*} Internal capture trips determined after reduction of transit trips.

[2] Trip generation for office was calculated using the following equations:

Daily: Ln(T) = 0.76 Ln(X) + 3.68 Where:

AM Peak Hour: Ln(T) = 0.80 Ln(X) + 1.57 Ln = Natural logarithm

PM Peak Hour: T = 1.12 (X) + 78.45 T = Two-way volume of traffic (total trip-ends) <math>X = Area in 1,000 square feet gross floor area

[3] Trip generation for retail/shopping center was calculated using the following equations:

Where:

Daily: Ln(T) = 0.65 Ln(X) + 5.83 Ln = Natural logarithm

AM Peak Hour: Ln(T) = 0.61 Ln(X) + 2.24 T = Two-way volume of traffic (total trip-ends) PM Peak Hour: Ln(T) = 0.67 Ln(X) + 3.31 X = 1,000 square feet gross leasable area

[4] ITE does not provide a daily trip generation rate for this use. Therefore, the daily trip rate for this use from *Brief Guide of Vehicular Traffic Generation Rates for the San Diego Region*, SANDAG, April 2002 was utilized.

[5] PM trip generation for automobile care center was calculated using the following equation:

Where:

PM Peak Hour: T = 2.41 (X) + 11.79 T = Two-way volume of traffic (total trip-ends)

X = 1,000 square feet occupied gross leasable area

^{**} Pass-by trips determined after reduction of internal capture trip credit.

^[1] Trip generation rates from *Trip Generation Manual*, 9th Edition, ITE 2012, unless otherwise noted.

TABLE E-1
Determination of Peak 15-Minute Percents within AM Peak Hour Traffic

Site		Day 1		Day 2			Day 3			Day 4			
Site		Dwy 1	Dwy 2	Total									
Site 1	AM Peak Vols 15Minute	22	30	52	22	36	58	19	40	59	18	24	42
	AM Peak Vols Hourly	76	105	181	69	99	168	51	93	144	62	85	147
	15-min Peak % of Hourly	-	-	28.7%	-	-	34.5%	-	-	41.0%	-	-	28.6%
Site 2	AM Peak Vols 15Minute	17	-	17	33	-	33	30	-	30	17	-	17
	AM Peak Vols Hourly	50	-	50	103	-	103	99	-	99	58	-	58
	15-min Peak % of Hourly	-	-	34.0%	-	-	32.0%	-	-	30.3%	1	-	29.3%
Site 3	AM Peak Vols 15Minute	29	-	29	13	-	13	16	-	16	26	-	26
	AM Peak Vols Hourly	101	-	101	44	-	44	51	-	51	72	-	72
	15-min Peak % of Hourly	-	-	28.7%	-	-	29.5%	-	-	31.4%	-	-	36.1%

Sites 1, 2 and 3 were office buildings in Culver City where traffic counts at driveways were compiled from counts on 4 days

#### **Determination of 90th Percentile Analysis of Peak Demand Percents** Rank Peak% 28.6% 2 28.7% Average 15-min Peak % 32.0% 3 28.7% 90th Percentile Peak % 36.1% 4 29.3% 5 29.5% Maximum 15-min Peak % 41.0% 30.3% 6 7 31.4% 8 32.0% 9 34.0% 10 34.5% 90th Percentile → 11 36.1% 12 41.0%

# TABLE E-2 MAXIMUM QUEUEING ANALYSIS AT DRIVEWAY

<b>102 trips</b> [calculated using 111+11+19-28-1-2]	[max 15-min % * Driveway Inbound AM Pk Hr Trips] = (0.41 * 102) <b>42</b> vehicles	<b>40</b> vehicles {using (15*60/90)*4}	<b>2</b> vehicles	<b>15</b> vehicles {10 vehicles queue storage plus 5 loading spaces on site}	No
Driveway Traffic of Proposed Project (AM Peak Hour Inbound) =	Maximum number of arrivals in peak 15-minute period =	Service Volume of Automated Parking Facility's 4 Elevators = (at the rate of 90 seconds/vehicle per elevator for 15 minutes)	Average Queue Length (2 - 3 above) in maximum 15-min period	Available storage on site =	Would Queue in maximum 15-minute period extend to Washington Boulevard?
П	7	ю	4	5	9

#### **APPENDIX F**

**Expo-to-Downtown Bicycle Connector** 

## EXPO-TO-DOWNTOWN

**BICYCLE CONNECTOR** 



## CONTEXT

With the opening of the Expo Line, Culver City is experiencing a change in transportation and development patterns near the station area. The City is taking advantage of this opportunity by encouraging transit-oriented development and multimodal transportation options. These strategies will help existing and new residents and commuters move around our community more easily by walking, biking, and transit.







provide a safe, family-friendly connection between the Expo Line, Expo Bike Path, and Downtown **Culver City** 



### PROMOTE MOBILITY

design streets for people of all ages and abilities to walk and bike comfortably



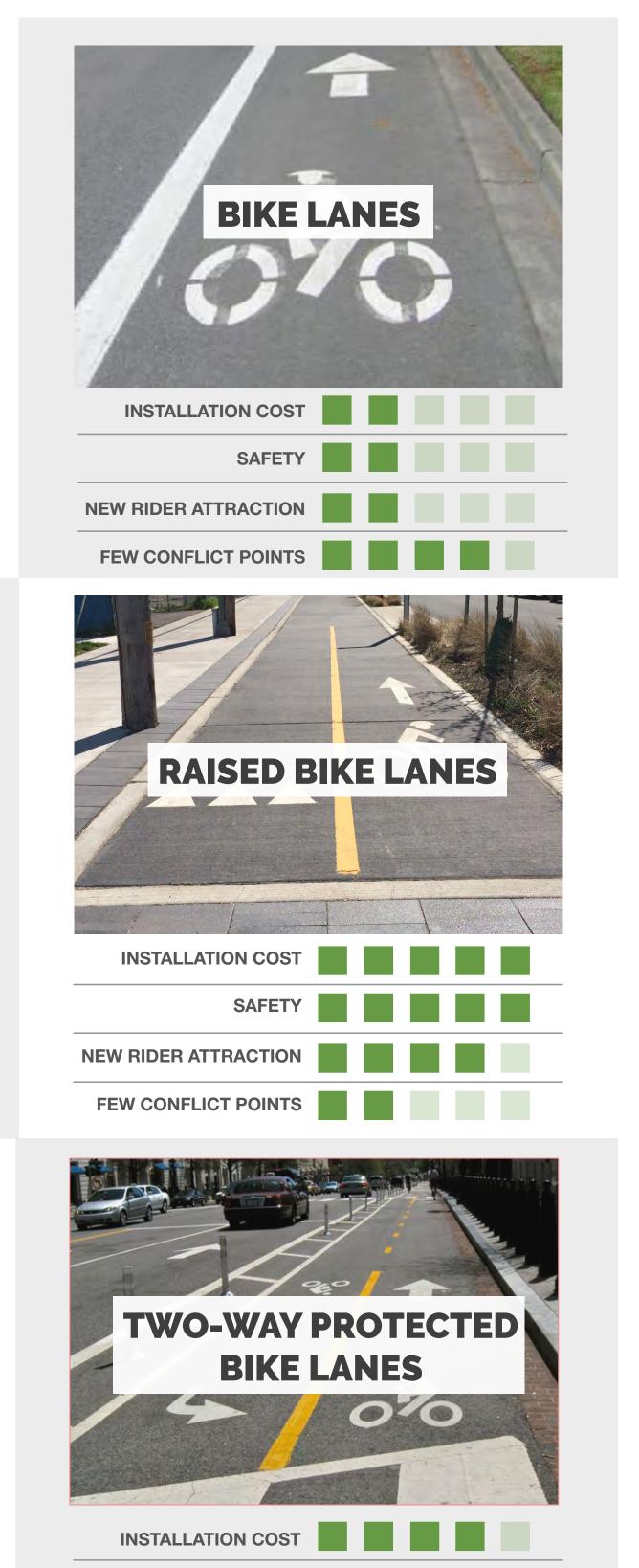


## PROJECT OVERVIEW

The project team was tasked with developing a feasible way to provide a high-quality bikeway between the Expo Line Station and Downtown Culver City. The consultant team considered a range of bikeway types, ranging from sharrows to painted bike lanes to protected bike lanes. To provide a safe and comfortable experience, the project team is recommending a two-way protected bike lane with signalized intersections.

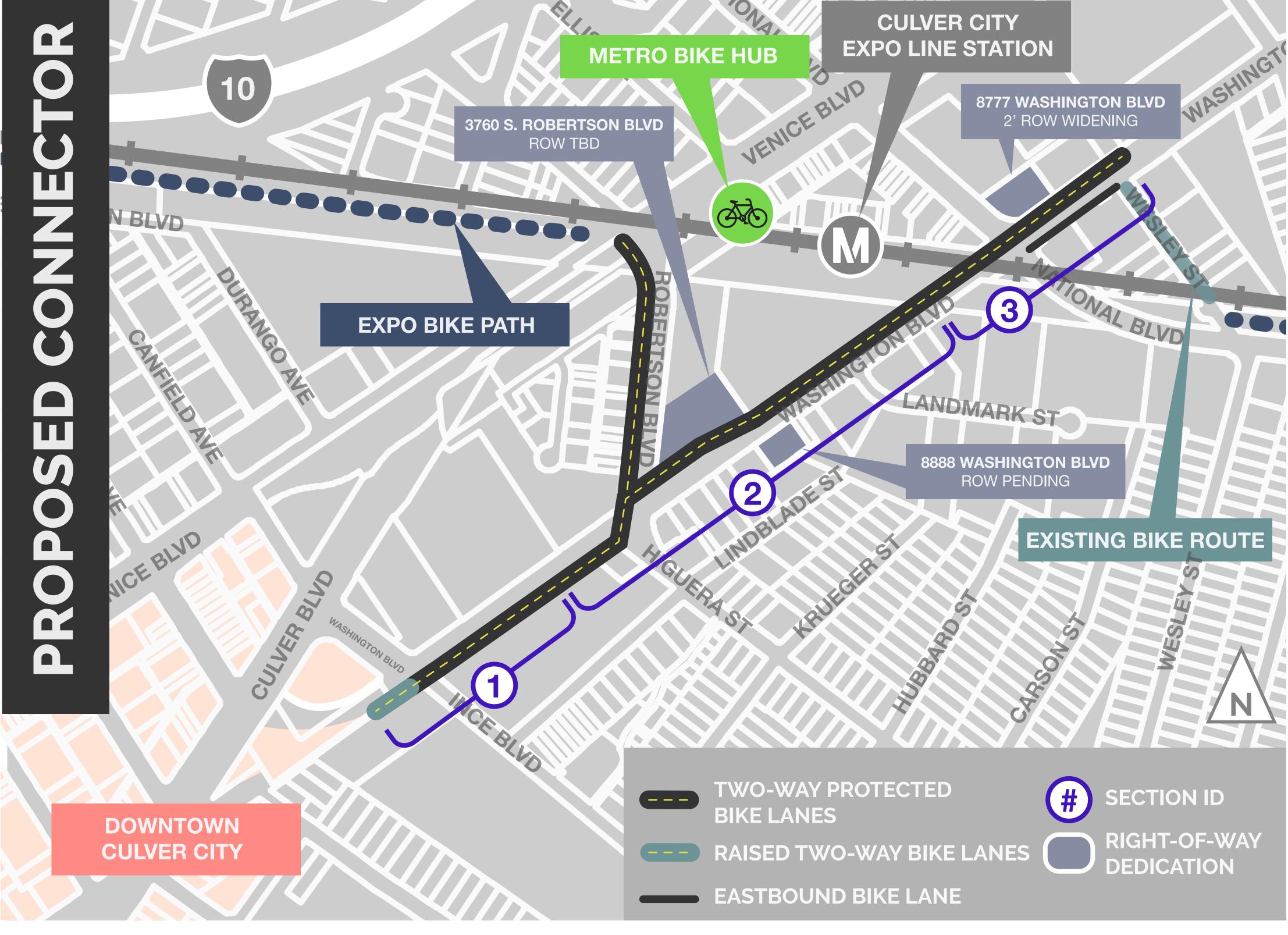
Based on stakeholder input, the City could consider implementing only a portion of the recommended alternative that would achieve some of the project's objectives.





**NEW RIDER ATTRACTION** 

**FEW CONFLICT POINTS** 



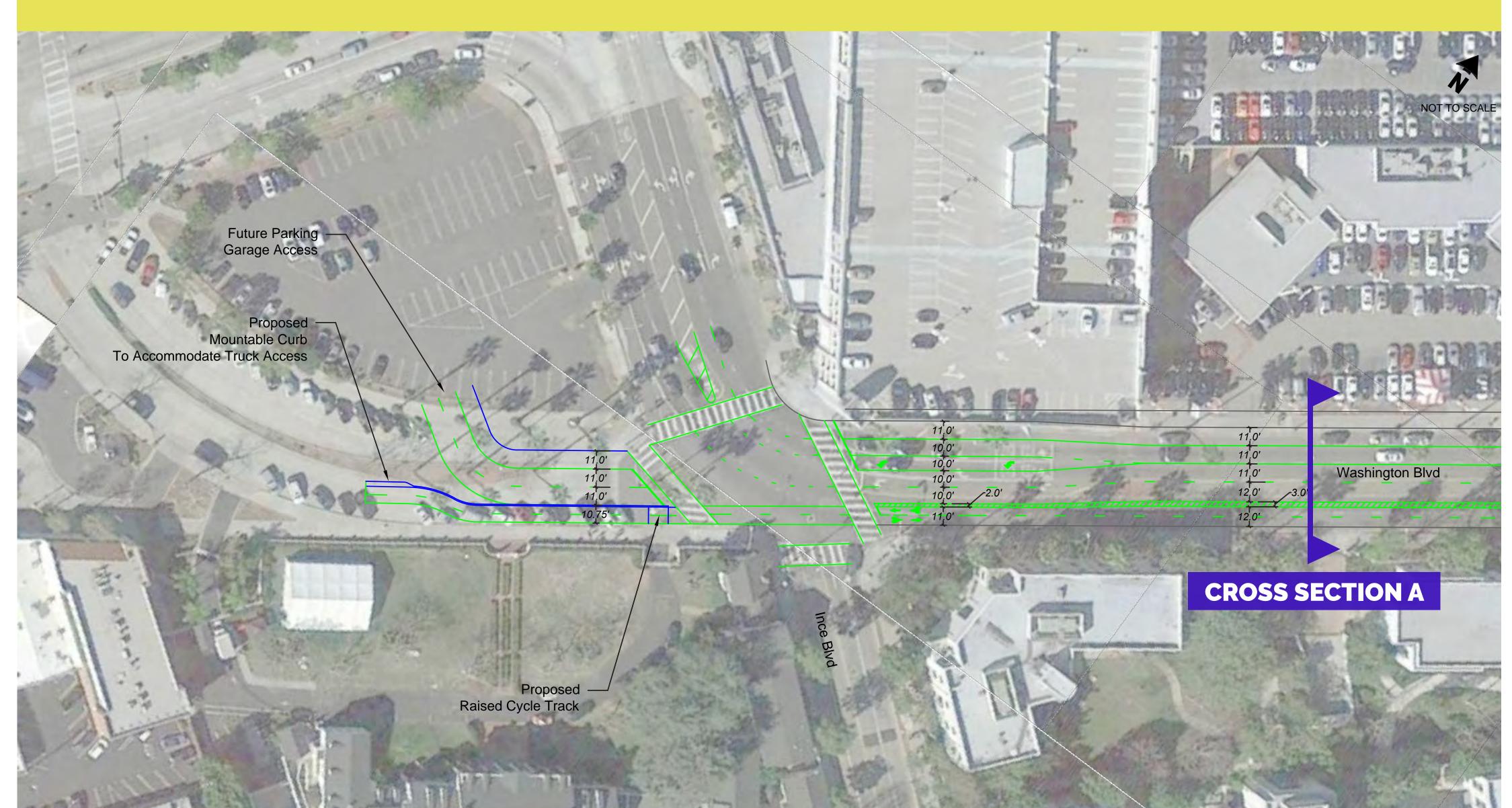
## 1) WASHINGTON/INCE

**FEATURES:** 





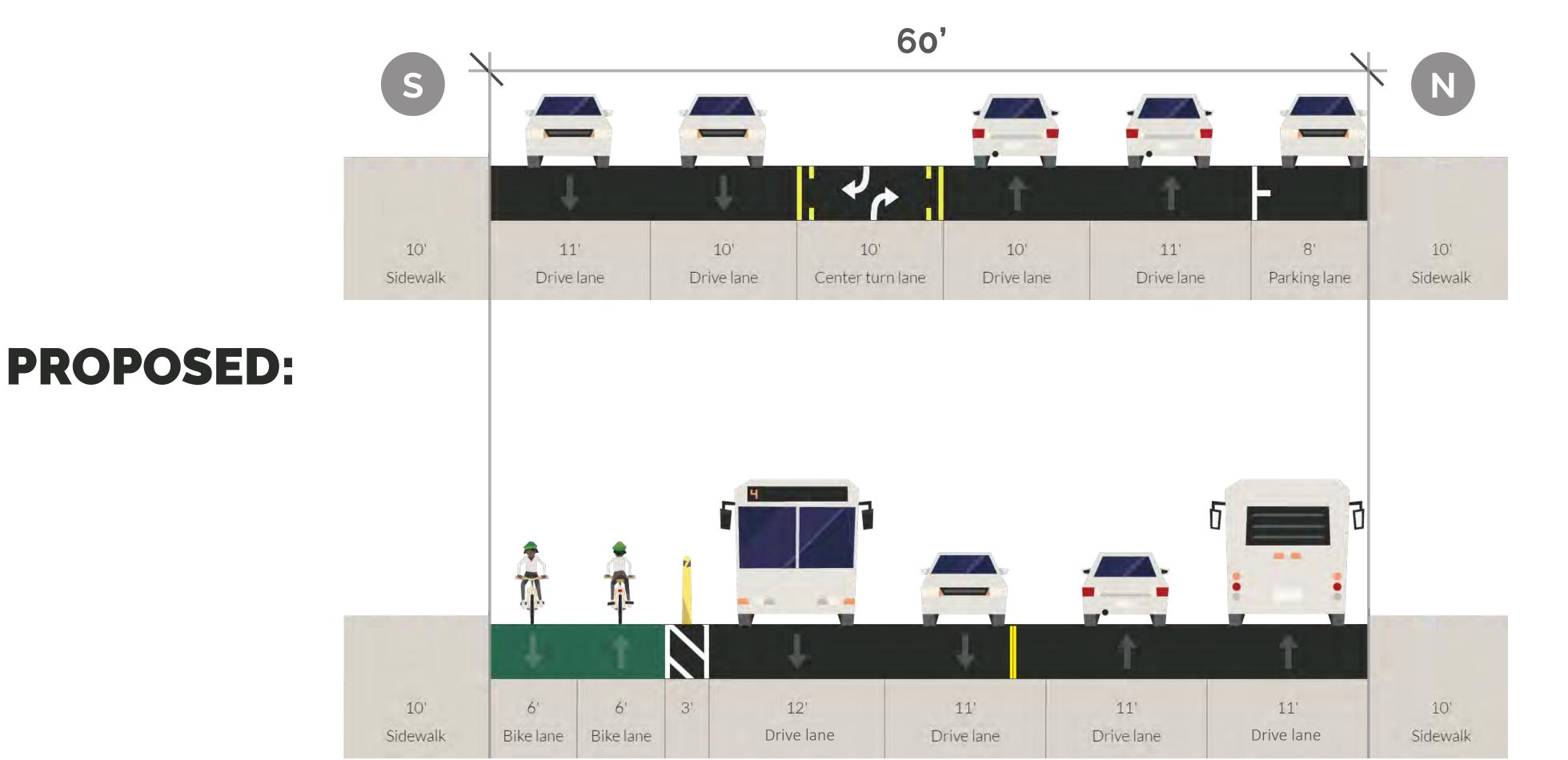




**CROSS SECTION A** 

## WASHINGTON BLVD FROM INCE BLVD TO ROBERTSON BLVD

## **EXISTING:**



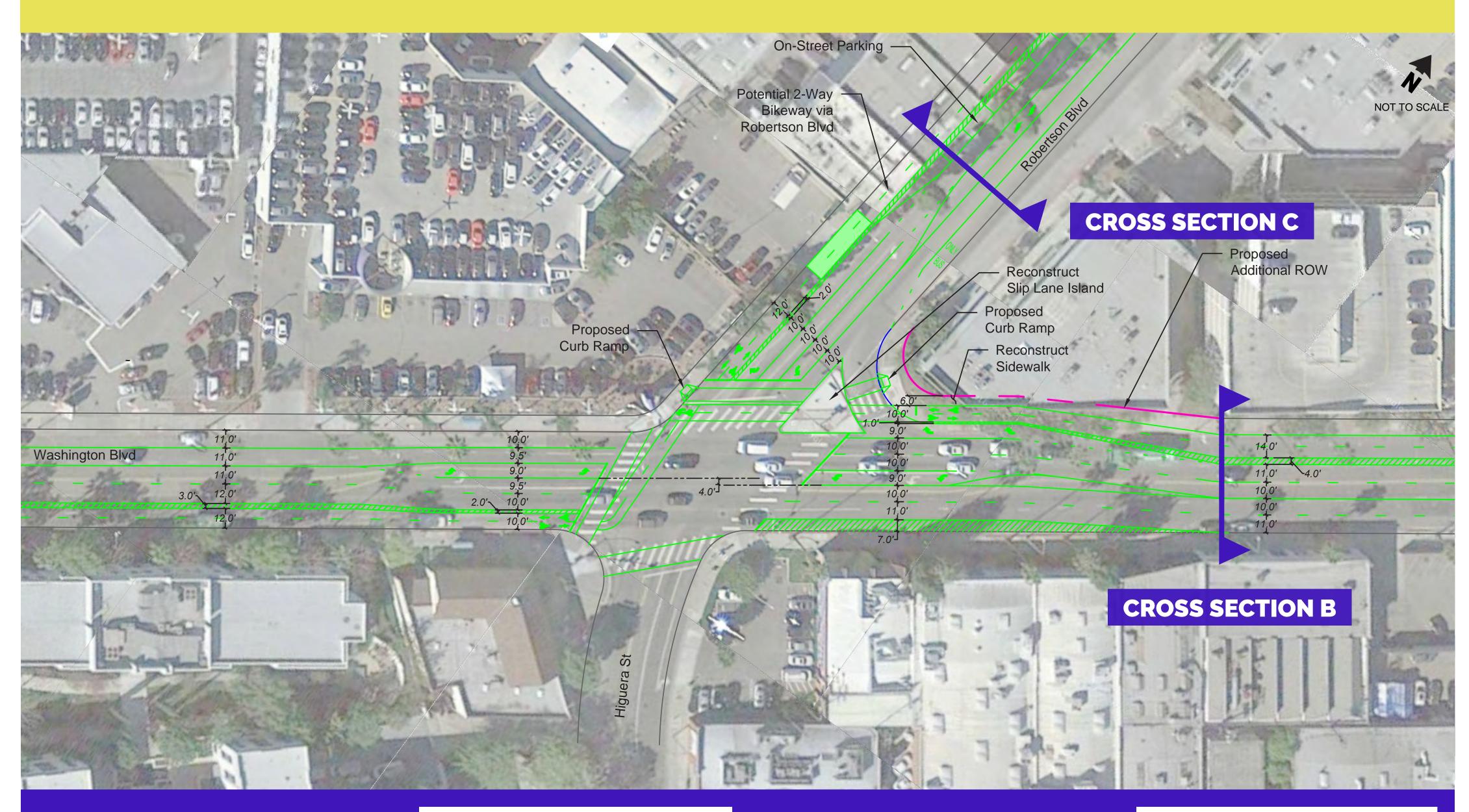
## 2 WASHINGTON/ROBERTSON/HIGUERA

### **FEATURES:**





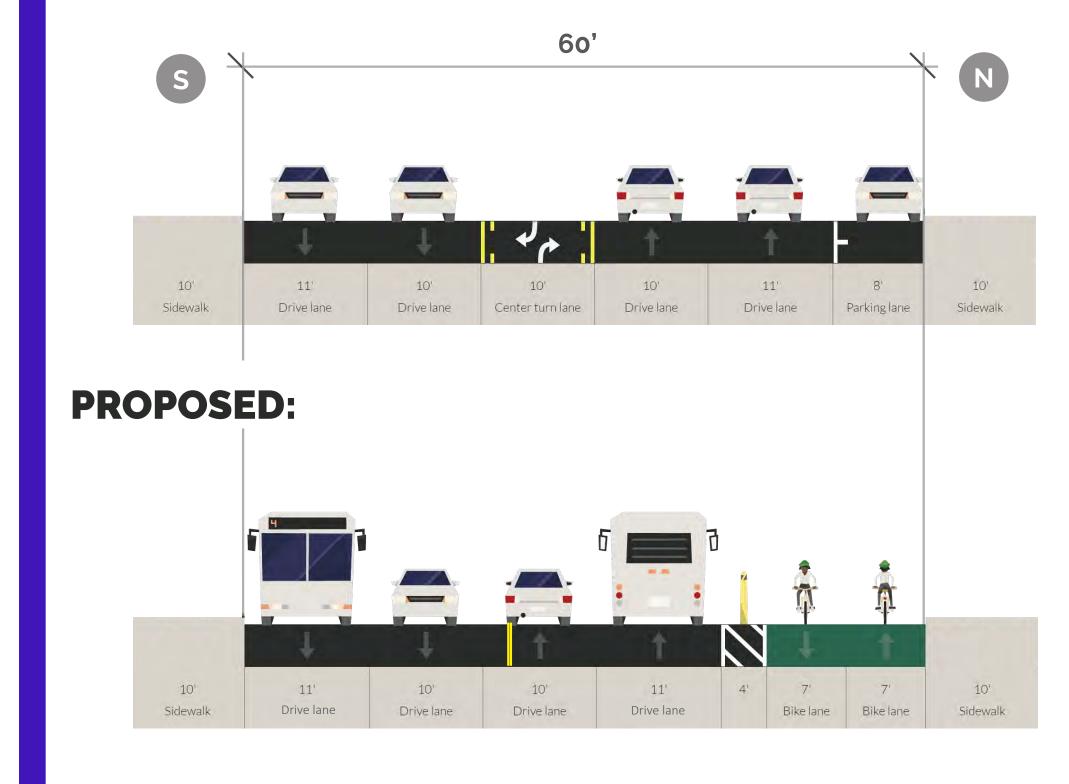




## **CROSS SECTION B**

**WASHINGTON BLVD** FROM ROBERTSON BLVD/HIGUERA ST TO **LANDMARK ST** 

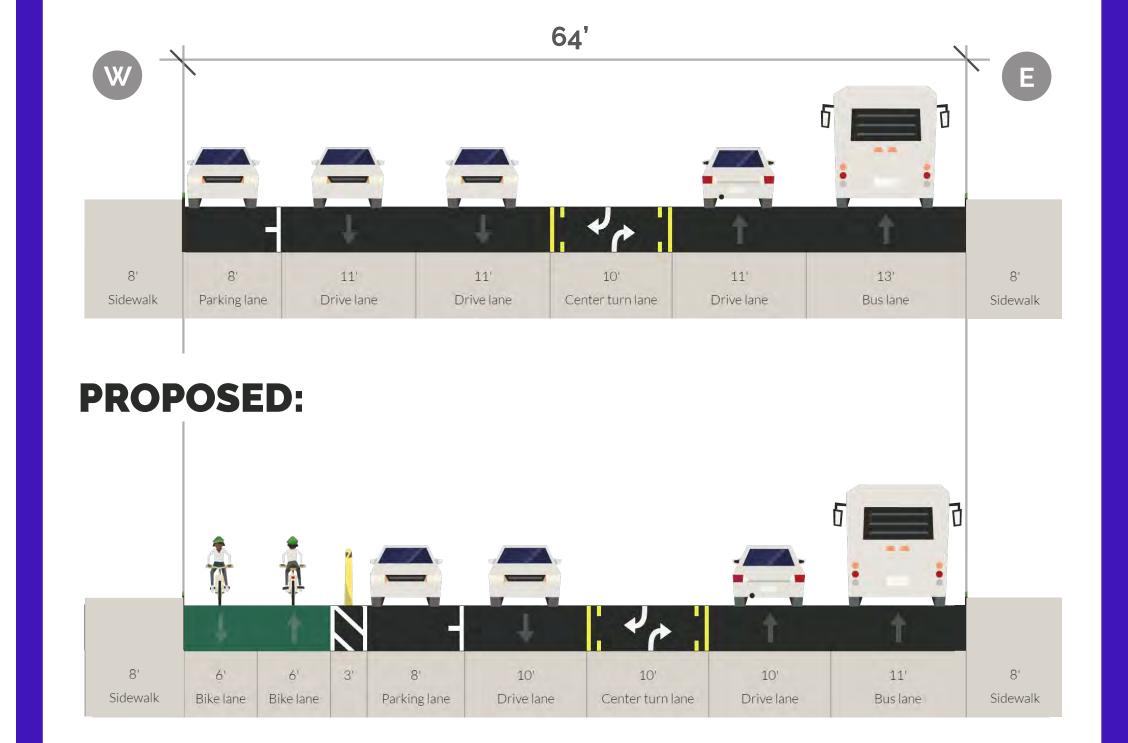
### **EXISTING:**



## CROSS SECTION C

**ROBERTSON BLVD** FROM WASHINGTON BLVD TO VENICE BLVD

### **EXISTING:**



## (3) WASHINGTON/NATIONAL

### **FEATURES:**



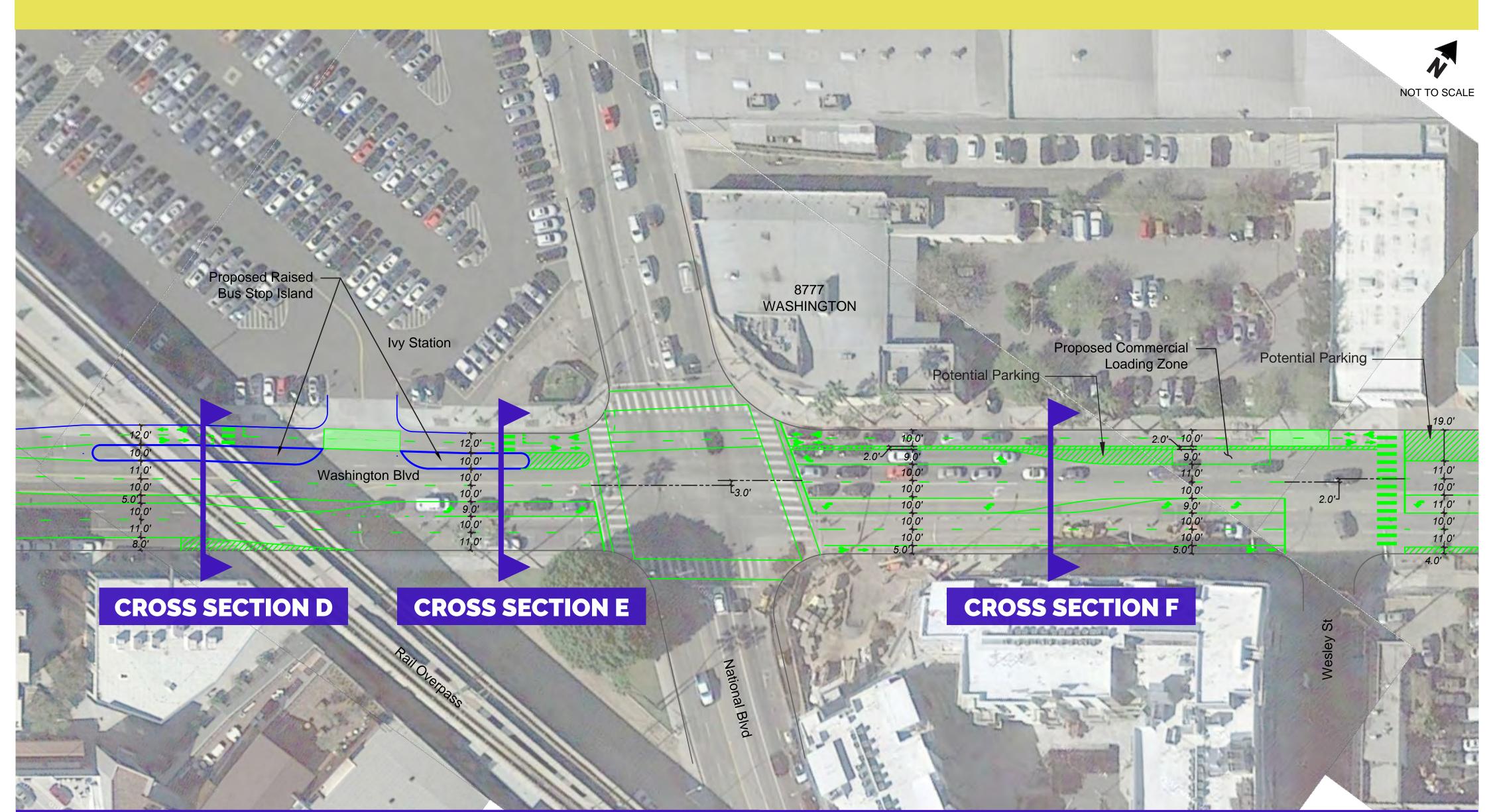








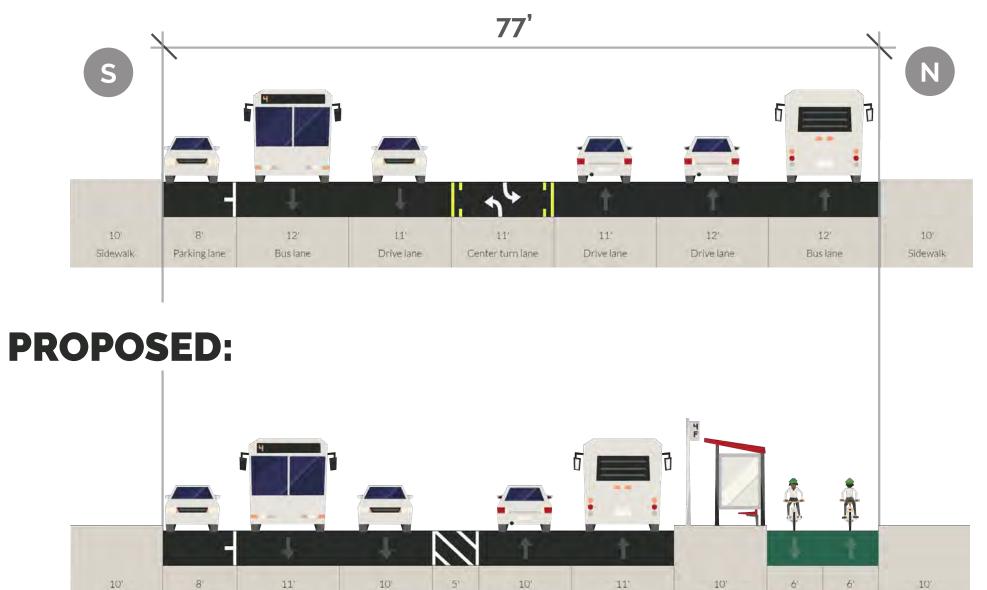
**EAST OF NATIONAL BLVD** 



## CROSS SECTION D

**WASHINGTON BLVD UNDER RAIL OVERPASS** 

### **EXISTING:**



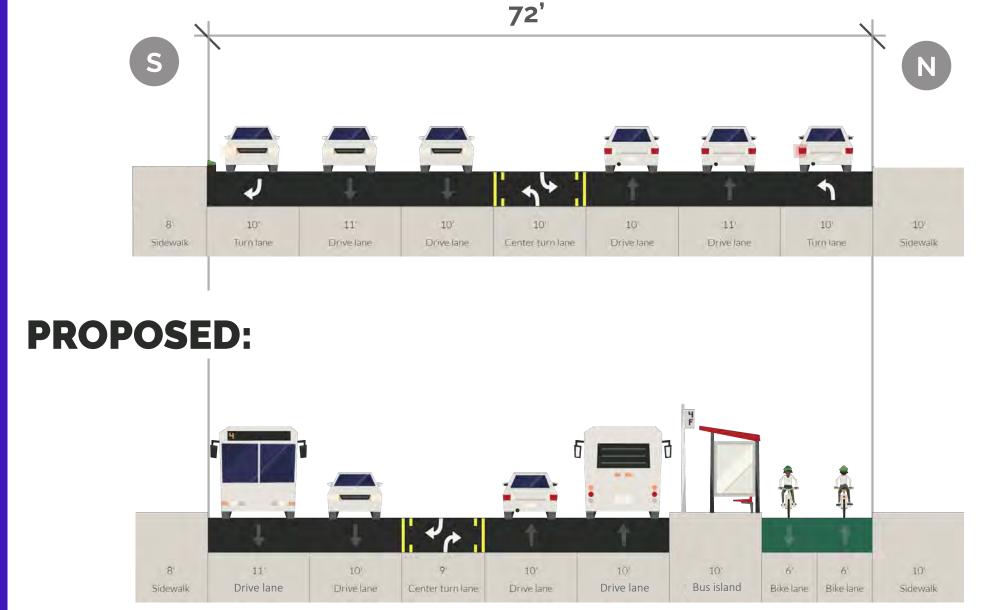
Buffer

Drive lane

## CROSS SECTION E

**WASHINGTON BLVD** FROM RAIL OVERPASS TO NATIONAL BLVD

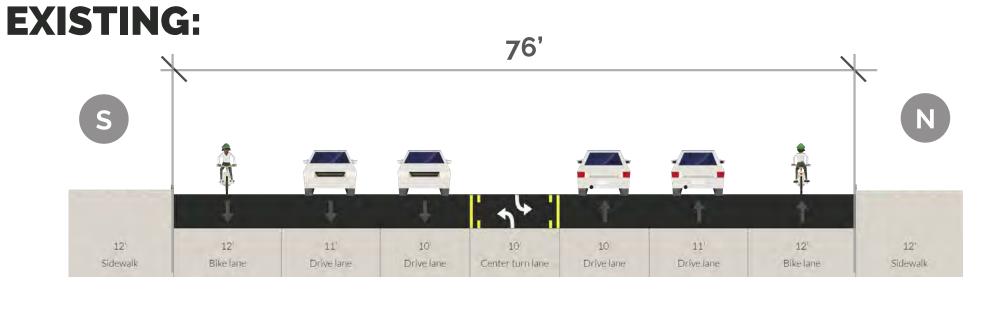
**EXISTING:** 



### **CROSS SECTION F**

Drive lane

**WASHINGTON BLVD FROM NATIONAL BLVD TO WESLEY ST** 



Drive lane

Bus island

Bike lane Bike lane

